

**APPENDIX L. DETERMINATION OF FURNACE AND BOILER ENERGY USE IN  
THE LCC ANALYSIS**

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## APPENDIX L. DETERMINATION OF FURNACE AND BOILER ENERGY USE IN THE LCC ANALYSIS

### L.1 INTRODUCTION

The energy consumption in the LCC analysis is determined using the proposed BSR/ASHRAE SPC 103R “Method of Testing for Annual Fuel Efficiency of Residential Central Furnaces and Boilers”.<sup>1</sup> Department of Energy used this test procedure instead of the current DOE test procedure, because of the anomaly with the DHR parameter as described in Appendix D section D.2.3. This approach requires the calculation of the average annual fuel energy consumption ( $E_F$ ), the average annual electrical energy consumption ( $E_{AE}$ ), and the national average number of burner operating hours ( $BOH$ ) of furnaces and boilers.

The following calculations and summary tables describe the determination of  $E_F$ ,  $E_{AE}$ , and  $BOH$  for gas- and oil-fired furnaces and boilers.

### L.2 CALCULATIONS

#### L.2.1 Determination of Average Annual Fuel Energy Consumption ( $E_F$ )

The average annual fuel consumption is calculated in Appendix C section 2 of the BSR/ASHRAE 103/1993R test procedure:<sup>1</sup>

$$E_F = BOH_{SS} * (Q_{IN} - Q_p) + 8,760 * Q_p, \text{ for single-stage furnaces and boilers,} \quad \text{Eq. 1}$$

$$E_F = (BOH_H * Q_{IN}) + (BOH_R * Q_{IN,R}) + [8,760 - (BOH_H + BOH_R)] * Q_p, \text{ for two-stage furnaces and boilers, and} \quad \text{Eq. 2}$$

$$E_F = (BOH_M * Q_{IN,M}) + (BOH_R * Q_{IN,R}) + [8,760 - (BOH_M + BOH_R)] * Q_p, \text{ for step modulating furnaces and boilers} \quad \text{Eq. 3}$$

where,

- $BOH_{SS}$  = national average number of burner operating hours (see derivation in section L.2.3),
- $BOH_H$  = national average number of burner operating hours at the maximum operating mode for two-stage furnaces and boilers (see derivation in section L.2.3),
- $BOH_R$  = national average number of burner operating hours at the reduced operating mode for two-stage or step modulating furnaces and boilers (see derivation in section L.2.3),
- $BOH_M$  = national average number of burner operating hours at the modulating operating mode for step modulating furnaces and boilers (see derivation in section L.2.3),

- $Q_{IN}$  = steady-state nameplate input rate in Btu/h for single-stage furnaces and boilers or steady-state nameplate maximum input rate in Btu/h for two-stage and step modulating furnaces and boilers,
- $Q_{IN,R}$  = steady-state reduced fuel input rate,
- $Q_{IN,M}$  = steady-state modulating fuel input rate, and
- $Q_P$  = pilot flame fuel input rate in Btu/h.

$Q_{IN}$  is based on the baseline value for each product class. We set  $Q_{IN,R}$  to be 69% of  $Q_{IN}$  for non-condensing two-stage equipment, 67% for condensing two-stage equipment, and 40% for step modulation equipment, where this value represents the average ratio  $Q_{IN}/Q_{IN,R}$  as derived using manufacturer product literature and Gas Appliance Manufacturers Association (GAMA) March 2005 Directory data for all listed two-stage furnace models.<sup>2</sup>

From Appendix C Section 1,<sup>1</sup>  $Q_{IN,M}$  is calculated using  $Q_{OUT,M}$  and  $Effy_{SS,M}$  (as defined in section 11.4.8.10 or 11.5.8.8).<sup>1</sup>  $Q_P$  is zero for all product classes, except for the baseline manufactured-home gas furnace and gas boiler.

## L.2.2 Determination of Average Annual Electrical Energy Consumption ( $E_{AE}$ )

Using the BSR/ASHRAE SPC 103 test procedure,<sup>1</sup> the average annual auxiliary electrical energy consumption is calculated in Appendix C section 3:

$$E_{AE} = BOH_{SS} (y_P * PE + y_{IG} * PE_{IG} + y * BE), \text{ for single-stage furnaces and boilers, Eq. 4}$$

and

$$E_{AE} = BOH_R (y_{P,R} * PE_R + y_{IG,R} * PE_{IG,R} + y_R * BE_R) + BOH_{H \text{ or } M} (y_P * PE_H + y_{IG} * PE_{IG,H} + y * BE_H)^1, \text{ for two-stage and step modulating furnaces and boilers, Eq. 5}$$

where

- $BOH_{SS}$  = as defined in section L.2.3,
- $BOH_H$  = as defined in section L.2.3,
- $BOH_M$  = as defined in section L.2.3,
- $BOH_R$  = as defined in section L.2.3,
- $y_P$  = ratio of induced or forced draft blower on-time to average burner on-time,
- $y_{P,R}$  = ratio of induced or forced draft blower on-time to average burner on-time, measured at the reduced fuel input rate,
- $PE$  = burner (or draft inducer) electrical power input at full-load steady-state operation in kW,

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<sup>1</sup> The BSR/ASHRAE test procedure does not deal with ignitor energy consumption. The ratio of ignitor on-time to burner on-time and the ignitor power consumption variables come from the DOE test procedure.<sup>3</sup>

$PE_R$	= burner (or draft inducer) electrical power input at full-load steady-state operation in kW, measured at the reduced fuel input rate,
$PE_H$	= burner (or draft inducer) electrical power input at full-load steady-state operation in kW, measured at the maximum fuel input rate,
$y_{IG}$	= ratio of burner interrupted-ignition device on-time to average burner on-time,
$y_{IG,R}$	= ratio of burner interrupted-ignition device on-time to average burner on-time, measured at the reduced fuel input rate,
$PE_{IG}$	= electrical input rate to the interrupted ignition device on the burner,
$PE_{IG,R}$	= electrical input rate to the interrupted ignition device on the burner, measured at the reduced fuel input rate,
$PE_{IG,H}$	= electrical input rate to the interrupted ignition device on the burner, measured at the maximum fuel input rate,
$y$	= ratio of blower or pump on-time to burner on-time,
$y_R$	= ratio of blower or pump on-time to burner on-time, measured at the reduced fuel input rate,
$BE$	= circulating-air fan or water pump electrical energy input rate in kW,
$BE_R$	= circulating-air fan or water pump electrical energy input rate in kW, measured at the reduced fuel input rate, and
$BE_H$	= circulating-air fan or water pump electrical energy input rate in kW, measured at the maximum fuel input rate.

The values  $y_p$  and  $y_{p,R}$  are calculated using  $t_p$  (post-purge time). For this calculation, DOE took  $t_p$  to be 5 seconds for furnaces, which is less than or 30 seconds and is therefore set equal to 0 seconds, according to Appendix C section 1.<sup>1</sup> For gas furnaces,  $t_p$  is equal to 3 minutes. For boilers, DOE calculated the values  $y_{IG}$  and  $y_{IG,R}$  using  $t_{IG}$  (burner interrupted-ignition device on-time). For gas furnaces and boilers,  $t_{IG} = 0.62$  min.<sup>4</sup> For oil boilers,  $t_{IG}$  is equal to 26 minutes for oil equipment without interrupted ignition and 45 seconds with oil equipment with interrupted ignition.<sup>5</sup> DOE calculated the values  $y$  and  $y_{p,R}$  using  $t^+$  (blower or pump on-delay) and  $t^-$  (blower or pump off-delay). For furnaces,  $t^+ = 2$  min and  $t^- = 0.5$  min, and for gas and oil boilers,  $t^+ = 15$  minutes and  $t^- = 0$ , which are values obtained for the generic furnace models (see Chapter 7 Section 7.2.6). For gas furnaces, PE is equal to 75 W for non-condensing furnaces and 90 W for condensing furnaces (see Chapter 7 Section 7.2.6). For oil furnaces and boilers, PE is set to 220 W.<sup>6</sup> For gas boilers, PE is equal to 76 W using typical values from the March 2005 GAMA Directory.<sup>2</sup> For design options which include modulation, we set  $PE_R$  and  $PE_H$  to have the same values as PE, since it is assumed that there is no inducer modulation. For gas furnaces and boilers,  $PE_{IG}$ ,  $PE_{IG,R}$ , and  $PE_{IG,H}$  are set equal to 400 W.<sup>7</sup> For oil furnaces and boilers,  $PE_{IG}$  is equal to 45 watts for oil equipment without interrupted ignition and 25 watts with oil equipment with interrupted ignition.<sup>8</sup> For design options which include modulation, we set  $PE_{IG,R}$  and  $PE_{IG,H}$  to have the same values as  $PE_{IG}$ , since it is assumed that there is no ignition modulation. For furnaces, BE and  $BE_R$  values are calculated using equations in Appendix J for the different design options. For boilers,  $BE_H$  and BE are set equal to 70 W, while  $BE_R$  is set 80% of  $BE_H$  (56 W).<sup>9</sup>

### L.2.3 Determination of National Average Number of Burner Operating Hours (BOH<sub>SS</sub>)

From the BSR/ASHRAE SPC103R test procedure,<sup>1</sup> the national average number of burner operating hours for furnaces and boilers is calculated in Appendix C section 1:

$$BOH_{SS} = 2080 * 0.77 * A * (Q_{OUT} / (1 + \alpha)) - 2080 * B, \text{ for single-stage furnaces and boilers,} \quad \text{Eq. 6}$$

$$BOH_H = X_H * (2080) * (0.77) * A_H * (Q_{OUT} / (1 + \alpha)) - 2080 * B_H, \text{ for two-stage furnaces and boilers at the maximum operating mode,} \quad \text{Eq. 7}$$

$$BOH_R = X_R * (2080) * (0.77) * A_R * (Q_{OUT} / (1 + \alpha)) - 2080 * B_R, \text{ for two-stage and step modulating furnaces and boilers operating at the reduced operating mode,} \quad \text{Eq. 8}$$

and

$$BOH_M = X_H * (2080) * (0.77) * A_M * (Q_{OUT} / (1 + \alpha)) - 2080 * B_M, \text{ for step modulating furnaces and boilers operating at the modulating operating mode,} \quad \text{Eq. 9}$$

where

- 2080 = national average heating load hours,  
 0.77 = adjustment factor to adjust the calculated design heating requirements and heating load hours to the actual heating load experienced by the heating system,  
 $A = 100,000 / [341300(y_p * PE + y_{IG,R} * PE_{IG,R} + y * BE) + (Q_{IN} - Q_p) * Effy_{HS}]^a$ ,  
 $A_H = 100,000 / [341300(y_p * PE_H + y_{IG,R} * PE_{IG,R} + y * BE_H) + (Q_{IN} - Q_p) * Effy_{U,H}]^a$ ,  
 $A_R = 100,000 / [341300(y_{p,R} * PE_R + y_{IG,R} * PE_{IG,R} + y_R * BE_R) + (Q_{IN,R} - Q_p) * Effy_{U,R}]^a$ ,  
 $A_M = 100,000 / [341300(y_p * PE_H + y_{IG,R} * PE_{IG,R} + y * BE_H) + (Q_{IN,M} - Q_p) * Effy_{U,M}]^a$ ,  
 $B = 2 * (Q_p) * (Effy_{HS}) * (A) / 100,000$ ,  
 $B_H = 2 * (Q_p) * (Effy_{U,H}) * (A_H) / 100,000$ ,  
 $B_R = 2 * (Q_p) * (Effy_{U,R}) * (A_R) / 100,000$ ,  
 $B_M = 2 * (Q_p) * (Effy_{U,M}) * (A_M) / 100,000$ ,  
 $Q_{OUT}$  = maximum fuel input rate heating capacity,  
 $\alpha$  = oversize factor,  
 $X_H$  = fraction of heating load at maximum fuel input rate operating mode,  
 $X_R$  = fraction of heating load at reduced fuel input rate operating mode (1- $X_H$ ),  
 $Q_{IN}$  = as defined in section L.2.1 of this appendix,  
 $Q_{IN,R}$  = as defined in section L.2.1 of this appendix,  
 $Q_{IN,M}$  = as defined in section L.2.1 of this appendix,  
 $Q_p$  = as defined in section L.2.1 of this appendix,

<sup>a</sup> The BSR/ASHRAE test procedure does not deal with ignitor energy consumption. The ratio of ignitor on-time to burner on-time and the ignitor power consumption variables come from the DOE test procedure.<sup>3</sup>

- $y_P$  = as defined in section L.2.2 of this appendix,  
 $y_{P,R}$  = as defined in section L.2.2 of this appendix,  
 $PE$  = as defined in section L.2.2 of this appendix,  
 $PE_R$  = as defined in section L.2.2 of this appendix,  
 $PE_H$  = as defined in section L.2.2 of this appendix,  
 $y_{IG}$  = as defined in section L.2.2 of this appendix,  
 $y_{IG,R}$  = as defined in section L.2.2 of this appendix,  
 $PE_{IG}$  = as defined in section L.2.2 of this appendix,  
 $PE_{IG,R}$  = as defined in section L.2.2 of this appendix,  
 $PE_{IG,H}$  = as defined in section L.2.2 of this appendix,  
 $y$  = as defined in section L.2.2 of this appendix,  
 $y_R$  = as defined in section L.2.2 of this appendix,  
 $BE$  = as defined in section L.2.2 of this appendix,  
 $BE_R$  = as defined in section L.2.2 of this appendix,  
 $BE_H$  = as defined in section L.2.2 of this appendix,  
 $Effy_{HS}$  = ratio of the average length of the heating season in hours to the average heating load hours,  
 $Effy_{U,H}$  = average part load efficiency at the maximum fuel input rate,  
 $Effy_{U,R}$  = average part load efficiency at the reduced fuel input rate, and  
 $Effy_{U,M}$  = average part load efficiency at the modulating fuel input rate.

Equations 6 through 9 are modified to account for the fact that we know the house heating load (HHL) for each RECS household (see Chapter 7 section 7.6). First we set HHL equal to the factors in equations 6 through 9 used to approximate HHL:

$$HHL = 2080 * 0.77 * (Q_{OUT} / (1 + \alpha)) \quad \text{Eq. 10}$$

Therefore  $\alpha$  is set equal to:

$$\alpha = Q_{OUT} * (2080) * (0.77) / (HHL) - 1 \quad \text{Eq. 11}$$

instead of being equal to the constant value 0.7 as defined in the BSR/ASHRAE SPC103 test procedure.<sup>1</sup>

The modified equations used in the LCC spreadsheet are as follows (Note that the maximum value for BOH is set to 8760):

$$BOH_{SS} = A * HHL - 2080 * B, \text{ for single-stage furnaces and boilers,} \quad \text{Eq. 12}$$

$$BOH_H = X_H * A_H * HHL - 2080 * B_H, \text{ for two-stage furnaces and boilers at the maximum operating mode,} \quad \text{Eq. 13}$$

$$BOH_R = X_R * A_R * HHL - 2080 * B_R, \text{ for two-stage and step modulating furnaces and boilers operating at the reduced operating mode,} \quad \text{Eq. 14}$$

and

$BOH_M = X_H * A_M * HHL - 2080 * B_M$ , for step modulating furnaces and boilers operating at the modulating operating mode, **Eq. 15**

To calculate factors  $A, A_H, A_R, A_M, B, B_H, B_R$ , and  $B_M$ , DOE calculated  $y_P, y_{P,R}, PE, PE_R, PE_H, y_{IG}, y_{IG,R}, PE_{IG}, PE_{IG,R}, PE_{IG,H}, y, y_R, BE, BE_R, BE_H, PE, y_{IG}, PE_{IG}, y, BE, Q_{IN}$ , and  $Q_P y_P$ , as described in section L.2.2 of this appendix. For factor  $B$ , if  $Q_P = 0$ , then  $B = 0$ , which is true for all cases except for the baseline manufactured-home gas furnace and the baseline gas boiler. We calculated  $Effy_{HS}$ , heating seasonal efficiency, as defined in sections 11.2.11, 11.3.11.3, 11.4.11.3, and 11.5.11.3.<sup>1</sup> For  $Q_P = 0$ ,  $Effy_{HS}$  is equal to the annual fuel utilization efficiency (AFUE). For  $Q_P > 0$ ,  $Effy_{HS}$  is calculated using  $Effy_{SS}$  (as defined in section 11.2.8.1<sup>1</sup>).  $Effy_{SS}$  is calculated using  $Q_{OUT}$  (as defined below),  $K$  (factor that adjusts the jacket losses, where  $K = 1.7$  for non-weatherized furnaces, 3.3 for weatherized furnaces, and 1 for boilers as described in section 11.2.8.1<sup>1</sup>), and  $L_j$  (jacket loss, where  $L_j = 1$  is the default value as described in section 11.2.8.1<sup>1</sup>)

$Q_{OUT}$  for all product classes is calculated using the following equations based on GAMA Directory 2005 data for Non-Weatherized Gas Furnaces<sup>2</sup>:

$$Q_{OUT} = Q_{IN} (0.7247 * AFUE + 0.22346), \text{ for non-condensing equipment, and} \quad \text{Eq. 16}$$

$$Q_{OUT} = Q_{IN} (0.8127 * AFUE + 0.17557), \text{ for condensing equipment.} \quad \text{Eq. 17}$$

DOE calculated  $X_H$  by using  $T_C$  (balance-point temperature as defined in section 11.4.8.4<sup>1</sup>),  $\alpha$  (the oversize factor, as calculated in Equation 11),  $Q_{OUT}$ , and  $Q_{OUT,R}$  (reduced fuel input rate heating capacity).  $Q_{OUT,R}$  is set equal to 69%  $Q_{OUT}$  for non-condensing equipment and 67%  $Q_{OUT}$  for condensing equipment, as derived using manufacturer product literature and Gas Appliance Manufacturers Association (GAMA) March 2005 Directory data for all listed two-stage furnace models.<sup>2</sup>  $X_R$  is set equal to  $1 - X_H$ . For similar reasons as provided in Appendix D, section D.3.2,  $Effy_{U,H} = Effy_{U,R}$  and therefore using the equation in section 11.5.11.3<sup>1</sup> is equal to  $Effy_{SS}$ .  $Effy_{U,M}$  is calculated using the equation in section 11.4.9.2.3.<sup>1</sup>

### L.3 SUMMARY TABLES

Tables L.4.1 through L.4.6 in this appendix contain data about the furnaces and boilers.

**Table L.3.1 Non-Weartherized Gas Furnaces**

Description	Effy <sub>HS</sub>	t <sub>p</sub>	PE	t <sub>IG</sub>	P <sub>IG</sub>	t <sup>+</sup>	t <sup>•</sup>
78% AFUE - Baseline	78%	5 sec	75	37 sec	400	120 sec	30 sec
80% AFUE - Increased HX Area	80%	5 sec	75	37 sec	400	120 sec	30 sec
80% AFUE - Modulation (2-Stage)	80%	5 sec	75	37 sec	400	120 sec	30 sec
81% AFUE - Increased HX Area	81%	5 sec	75	37 sec	400	120 sec	30 sec
81% AFUE - Modulation (2-Stage)	81%	5 sec	75	37 sec	400	120 sec	30 sec
90% AFUE	90%	5 sec	90	37 sec	400	120 sec	30 sec
92% AFUE - Increased HX Area	92%	5 sec	90	37 sec	400	120 sec	30 sec
92% AFUE - Modulation (2-Stage)	92%	5 sec	90	37 sec	400	120 sec	30 sec
92% AFUE - Modulation (Continuous)	92%	5 sec	90	37 sec	400	120 sec	30 sec
96% AFUE - Modulation (Continuous)	96%	5 sec	90	37 sec	400	120 sec	30 sec

**Table L.3.2 Weartherized Gas Furnaces**

Description	Effy <sub>HS</sub>	t <sub>p</sub>	PE	t <sub>IG</sub>	P <sub>IG</sub>	t <sup>+</sup>	t <sup>•</sup>
78% AFUE - Baseline	78%	5 sec	75	37 sec	400	120 sec	30 sec
80% AFUE - Increased HX Area	80%	5 sec	75	37 sec	400	120 sec	30 sec
81% AFUE - Increased HX Area	81%	5 sec	75	37 sec	400	120 sec	30 sec
82% AFUE - Increased HX Area	82%	5 sec	75	37 sec	400	120 sec	30 sec
83% AFUE - Increased HX Area	83%	5 sec	75	37 sec	400	120 sec	30 sec

**Table L.3.3 Mobile Home Gas Furnaces**

Description	Effy <sub>HS</sub>	t <sub>p</sub>	PE	t <sub>IG</sub>	P <sub>IG</sub>	t <sup>+</sup>	t <sup>•</sup>
75% AFUE - Baseline	79%	5 sec	75	37 sec	0	120 sec	30 sec
80% AFUE - Increased HX Area	80%	5 sec	75	37 sec	400	120 sec	30 sec
80% AFUE - Modulation (2-Stage)	80%	5 sec	75	37 sec	400	120 sec	30 sec
81% AFUE - Increased HX Area	81%	5 sec	75	37 sec	400	120 sec	30 sec
81% AFUE - Modulation (2-Stage)	81%	5 sec	75	37 sec	400	120 sec	30 sec
82% AFUE - Increased HX Area	82%	5 sec	75	37 sec	400	120 sec	30 sec
82% AFUE - Modulation (2-Stage)	82%	5 sec	75	37 sec	400	120 sec	30 sec
90% AFUE - Condensing	90%	5 sec	90	37 sec	400	120 sec	30 sec

**Table L.3.4 Oil-Fired Furnaces**

Description	Effy <sub>HS</sub>	t <sub>p</sub>	PE	t <sub>IG</sub>	P <sub>IG</sub>	t <sup>+</sup>	t <sup>-</sup>
78% AFUE - Baseline	78%	5 sec	220	26 min	45	120 sec	30 sec
80% AFUE - Increased HX Area	80%	5 sec	220	26 min	45	120 sec	30 sec
81% AFUE - Increased HX Area	81%	5 sec	220	26 min	45	120 sec	30 sec
81% AFUE - Interrupted Ignition	81%	5 sec	220	45 sec	25	120 sec	30 sec
81% AFUE - Modulation (2-Stage)	81%	5 sec	220	45 sec	25	120 sec	30 sec
82% AFUE - Increased HX Area	82%	5 sec	220	26 min	45	120 sec	30 sec
82% AFUE - Interrupted Ignition	82%	5 sec	220	45 sec	25	120 sec	30 sec
82% AFUE - Modulation (2-Stage)	82%	5 sec	220	45 sec	25	120 sec	30 sec
83% AFUE - Increased HX Area	83%	5 sec	220	26 min	45	120 sec	30 sec
83% AFUE - Interrupted Ignition	83%	5 sec	220	45 sec	25	120 sec	30 sec
83% AFUE - Modulation (2-Stage)	83%	5 sec	220	45 sec	25	120 sec	30 sec
84% AFUE - Increased HX Area	84%	5 sec	220	26 min	45	120 sec	30 sec
84% AFUE - Interrupted Ignition	84%	5 sec	220	45 sec	25	120 sec	30 sec
84% AFUE - Modulation (2-Stage)	84%	5 sec	220	45 sec	25	120 sec	30 sec
85% AFUE - Increased HX Area	85%	5 sec	220	26 min	45	120 sec	30 sec
85% AFUE - Interrupted Ignition	85%	5 sec	220	45 sec	25	120 sec	30 sec
85% AFUE - Modulation (2-Stage)	85%	5 sec	220	45 sec	25	120 sec	30 sec

**Table L.3.5 Hot-Water Gas Boilers**

Description	Effy <sub>HS</sub>	t <sub>p</sub>	PE	t <sub>IG</sub>	P <sub>IG</sub>	t <sup>+</sup>	t <sup>-</sup>
80% AFUE - Baseline	82%	180 sec	76	37 sec	0	15 min	0 sec
81% AFUE - Improved Heat Transfer Coef.	81%	180 sec	76	37 sec	400	15 min	0 sec
81% AFUE - Modulation (2-Stage)	81%	180 sec	76	37 sec	400	15 min	0 sec
82% AFUE - Improved Heat Transfer Coef.	82%	180 sec	76	37 sec	400	15 min	0 sec
82% AFUE - Modulation (2-Stage)	82%	180 sec	76	37 sec	400	15 min	0 sec
83% AFUE - Improved Heat Transfer Coef.	83%	180 sec	76	37 sec	400	15 min	0 sec
83% AFUE - Modulation (2-Stage)	83%	180 sec	76	37 sec	400	15 min	0 sec
84% AFUE - Improved Heat Transfer Coef.	84%	180 sec	76	37 sec	400	15 min	0 sec
84% AFUE - Modulation (2-Stage)	84%	180 sec	76	37 sec	400	15 min	0 sec
85% AFUE - Improved Heat Transfer Coef.	85%	180 sec	76	37 sec	400	15 min	0 sec
85% AFUE - Modulation (2-Stage)	85%	180 sec	76	37 sec	400	15 min	0 sec
86% AFUE	86%	180 sec	76	37 sec	400	15 min	0 sec
91% AFUE	91%	180 sec	76	37 sec	400	15 min	0 sec
99% AFUE	99%	180 sec	76	37 sec	400	15 min	0 sec

**Table L.3.6 Hot-Water Oil Boilers**

<b>Description</b>	<b>Effy<sub>HS</sub></b>	<b>t<sub>p</sub></b>	<b>PE</b>	<b>t<sub>IG</sub></b>	<b>P<sub>IG</sub></b>	<b>t<sup>+</sup></b>	<b>t<sup>-</sup></b>
80% AFUE - Baseline	80%	180 sec	220	26 min	45	15 min	0 sec
81% AFUE - Improved Heat Transfer Coef.	81%	180 sec	220	26 min	45	15 min	0 sec
81% AFUE - Interrupted Ignition	81%	180 sec	220	45 sec	25	15 min	0 sec
82% AFUE - Improved Heat Transfer Coef.	82%	180 sec	220	26 min	45	15 min	0 sec
82% AFUE - Interrupted Ignition	82%	180 sec	220	45 sec	25	15 min	0 sec
82% AFUE - Modulation (2-Stage)	82%	180 sec	220	45 sec	25	15 min	0 sec
83% AFUE - Improved Heat Transfer Coef.	83%	180 sec	220	26 min	45	15 min	0 sec
83% AFUE - Interrupted Ignition	83%	180 sec	220	45 sec	25	15 min	0 sec
83% AFUE - Modulation (2-Stage)	83%	180 sec	220	45 sec	25	15 min	0 sec
84% AFUE - Improved Heat Transfer Coef.	84%	180 sec	220	26 min	45	15 min	0 sec
84% AFUE - Interrupted Ignition	84%	180 sec	220	45 sec	25	15 min	0 sec
84% AFUE - Modulation (2-Stage)	84%	180 sec	220	45 sec	25	15 min	0 sec
85% AFUE - Improved Heat Transfer Coef.	85%	180 sec	220	26 min	45	15 min	0 sec
85% AFUE - Interrupted Ignition	85%	180 sec	220	45 sec	25	15 min	0 sec
85% AFUE - Modulation (2-Stage)	85%	180 sec	220	45 sec	25	15 min	0 sec
86% AFUE - Improved Heat Transfer Coef.	86%	180 sec	220	26 min	45	15 min	0 sec
86% AFUE - Interrupted Ignition	86%	180 sec	220	45 sec	25	15 min	0 sec
86% AFUE - Modulation (2-Stage)	86%	180 sec	220	45 sec	25	15 min	0 sec
90% AFUE	90%	180 sec	220	45 sec	25	15 min	0 sec
95% AFUE	95%	180 sec	220	45 sec	25	15 min	0 sec

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