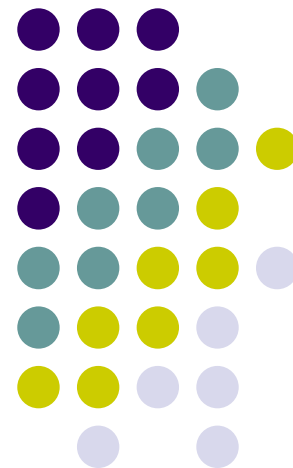


Reactor Cost Analysis

Brian James
Directed Technologies, Inc.
6-7 November 2007

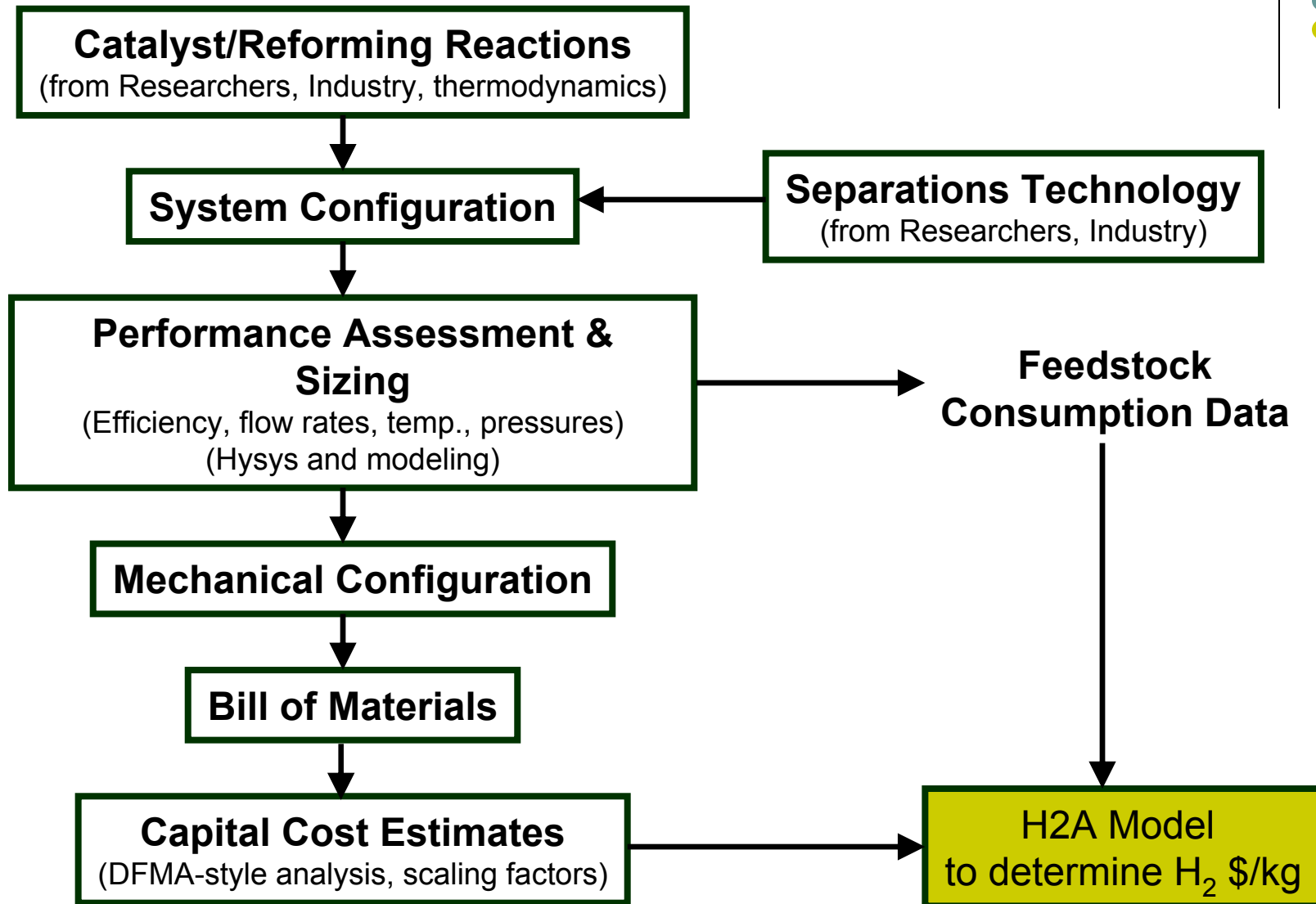
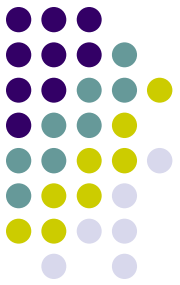


Objective

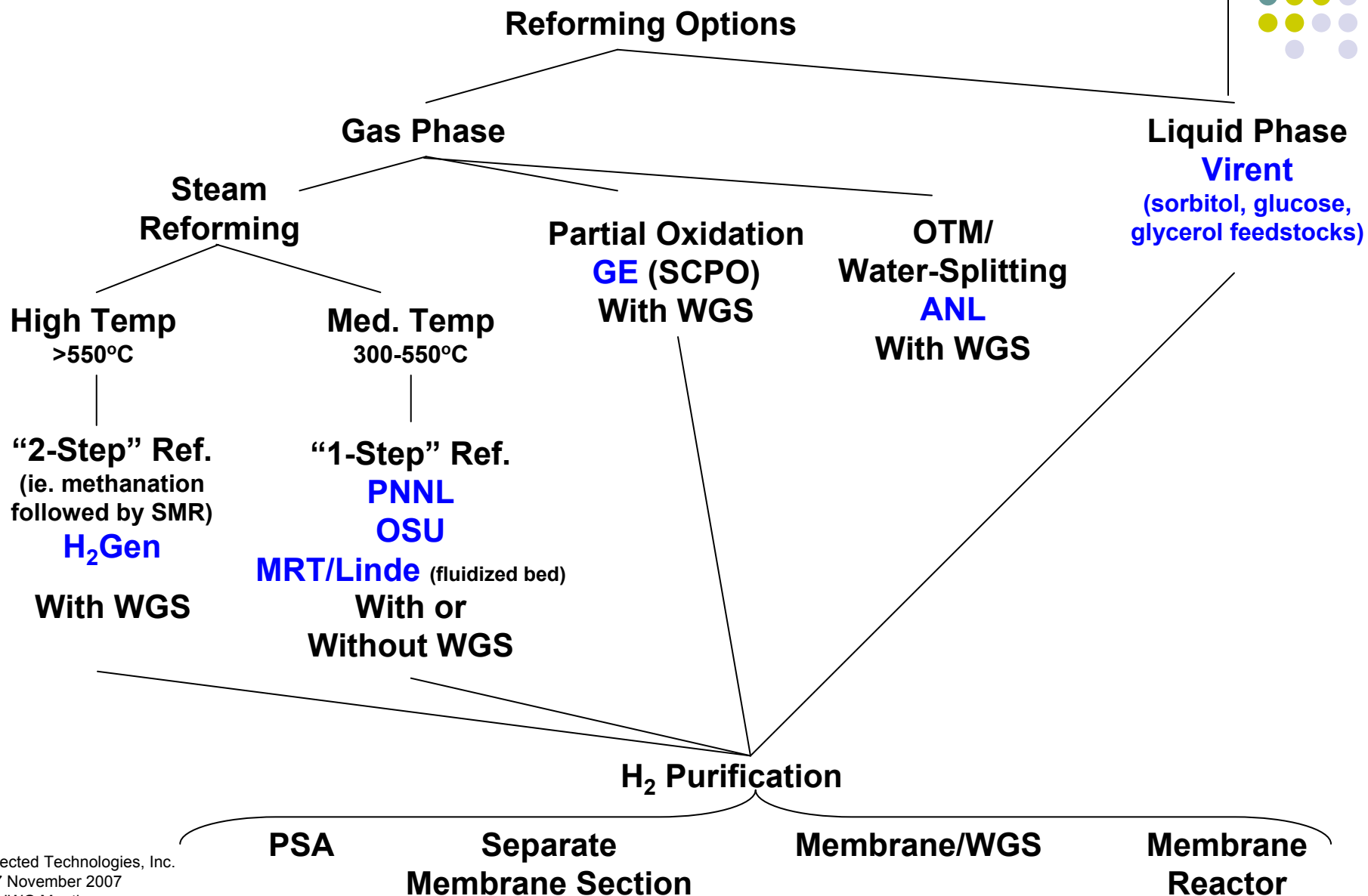


- **Assess cost of H₂ from bio-derived liquids**
 - Looking at forecourt scale systems: 100-1500+kg/day
 - Emphasis on Ethanol
 - Looking at both “conventional” and “advanced” systems
- **Interaction with the Researchers is bi-directional**
 - Researchers help me with catalysts, performance, configurations
 - I can assist Researchers with system studies, configurations, and system performance estimates
- **Output of my work will be:**
 - System/Configuration Definition
 - Performance specification & optimization
 - Capital cost estimation
 - Projected hydrogen \$/kg

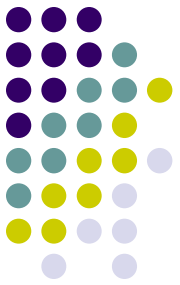
Methodology



Ethanol Reforming Hierarchy



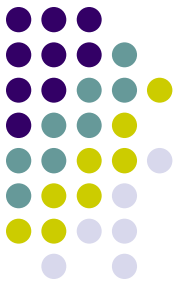
Potential Ethanol SR Reactions



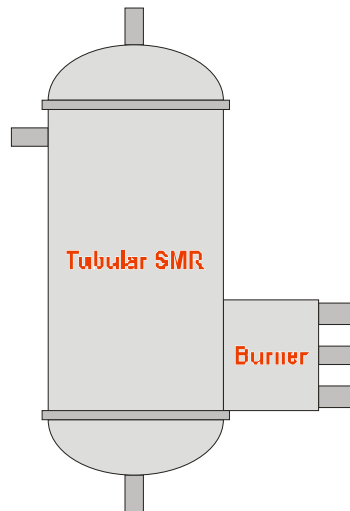
- 1) **C₂H₅OH dehydration to ethylene (C₂H₄) and water**
dehydration $\text{C}_2\text{H}_5\text{OH} \rightarrow \text{C}_2\text{H}_4 + \text{H}_2\text{O}$
polymerization $\text{C}_2\text{H}_4 \rightarrow \text{coke}$
- 2) **C₂H₅OH decomposition/cracking to methane (CH₄)**
decomposition $\text{C}_2\text{H}_5\text{OH} \rightarrow \text{CH}_4 + \text{CO} + \text{H}_2$
steam reforming $\text{CH}_4 + 2\text{H}_2\text{O} \rightarrow 4\text{H}_2 + \text{CO}_2$
- 3) **C₂H₅OH dehydrogenation to acetaldehyde (C₂H₄O)**
dehydrogenation $\text{C}_2\text{H}_5\text{OH} \rightarrow \text{C}_2\text{H}_4\text{O} + \text{H}_2$
decarbonylation $\text{C}_2\text{H}_4\text{O} \rightarrow \text{CH}_4 + \text{CO}$
steam reforming $\text{CH}_4 + \text{H}_2\text{O} \rightarrow 3\text{H}_2 + 2\text{CO}$
- 4) **C₂H₅OH decomposition into acetone (CH₃COCH₃)**
decomposition $2 \text{C}_2\text{H}_5\text{OH} \rightarrow \text{CH}_3\text{COCH}_3 + \text{CO} + 3\text{H}_2$
steam reforming $\text{CH}_3\text{COCH}_3 + 2\text{H}_2\text{O} \rightarrow 5\text{H}_2 + 3\text{CO}$
- 5) **Steam reforming of C₂H₅OH to syngas (CO + H₂)**
steam reforming $\text{C}_2\text{H}_5\text{OH} + \text{H}_2\text{O} \rightarrow 2\text{CO} + 4\text{H}_2$
- 6) **Water gas shift**
- 7) **Methanation**
- 8) **Coking from CH₄ (methane)**
coking $\text{CH}_4 \rightarrow 2\text{H}_2 + \text{C}$
- 9) **Coking from boudouard reaction**
coking $\text{CO}_2 \rightarrow \text{O}_2 + \text{C}$
- 10) **Dissociative adsorption of water to form acetic acid (CH₃COOH)**
water adsorption $\text{C}_2\text{H}_5\text{OH} + \text{H}_2\text{O} \rightarrow \text{CH}_3\text{COOH} + 2\text{H}_2$

**Neat EtOH
or E85/E95?**

Reactor Configurations



Tubular Reactor



Annular Heat Exchange Reactor (HER)

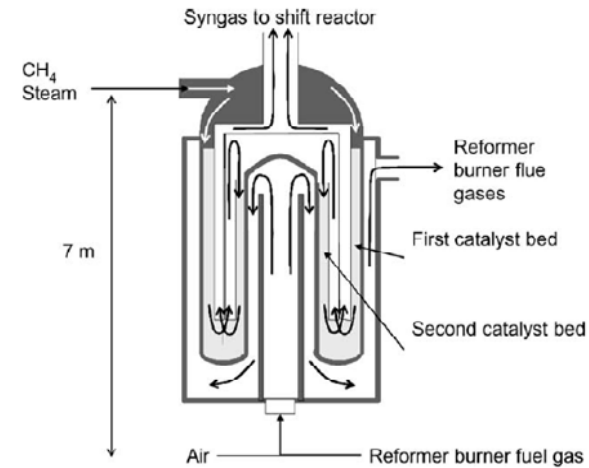
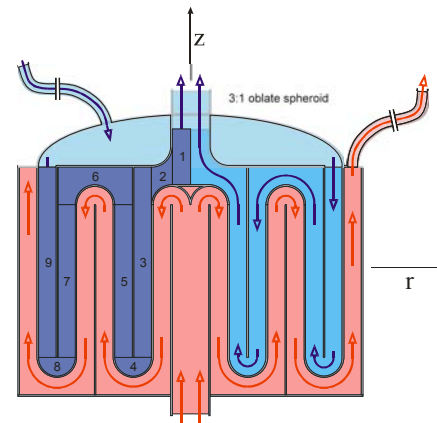


Figure 18: Heat exchange reformer (HER) with annular concentric catalyst bed (170).
[170] Topsoe HTCR Compact Hydrogen Units. Haldor Topsoe A/S. www.haldortopsoe.com (accessed Dec. 2004).



DOE Technical Targets for Dense Metallic Membranes



Flux Rate:	2006 Status	2010 Target	2015 Target
	>200 scfh/ft²	250 scfh/ft²	300 scfh/ft²

Based on:

- 20 psi partial pressure difference
- 15 psig permeate minimum total pressure (preferably >50 psig) (assumed to be pure H₂)
- 400°C

Sievert's Law

$$D = A \cdot \mathcal{P} \cdot (P_{\text{H}_2 \text{ Reformate}}^{0.5} - P_{\text{H}_2 \text{ Permeate}}^{0.5}) \quad \text{where permeability } \mathcal{P} = \frac{a}{t} \cdot \exp\left(\frac{-b}{RT}\right)$$

where

D is the hydrogen permeation rate in **scfh**

$\mathcal{P}$ is the permeability, in **scfh/ft²/atm^{0.5}**

A is the membrane effective surface area in **ft²**

P_{H_2} is the hydrogen partial pressure (reformate or permeate streams) in **atm**

t is the thickness of the membrane in **ft**

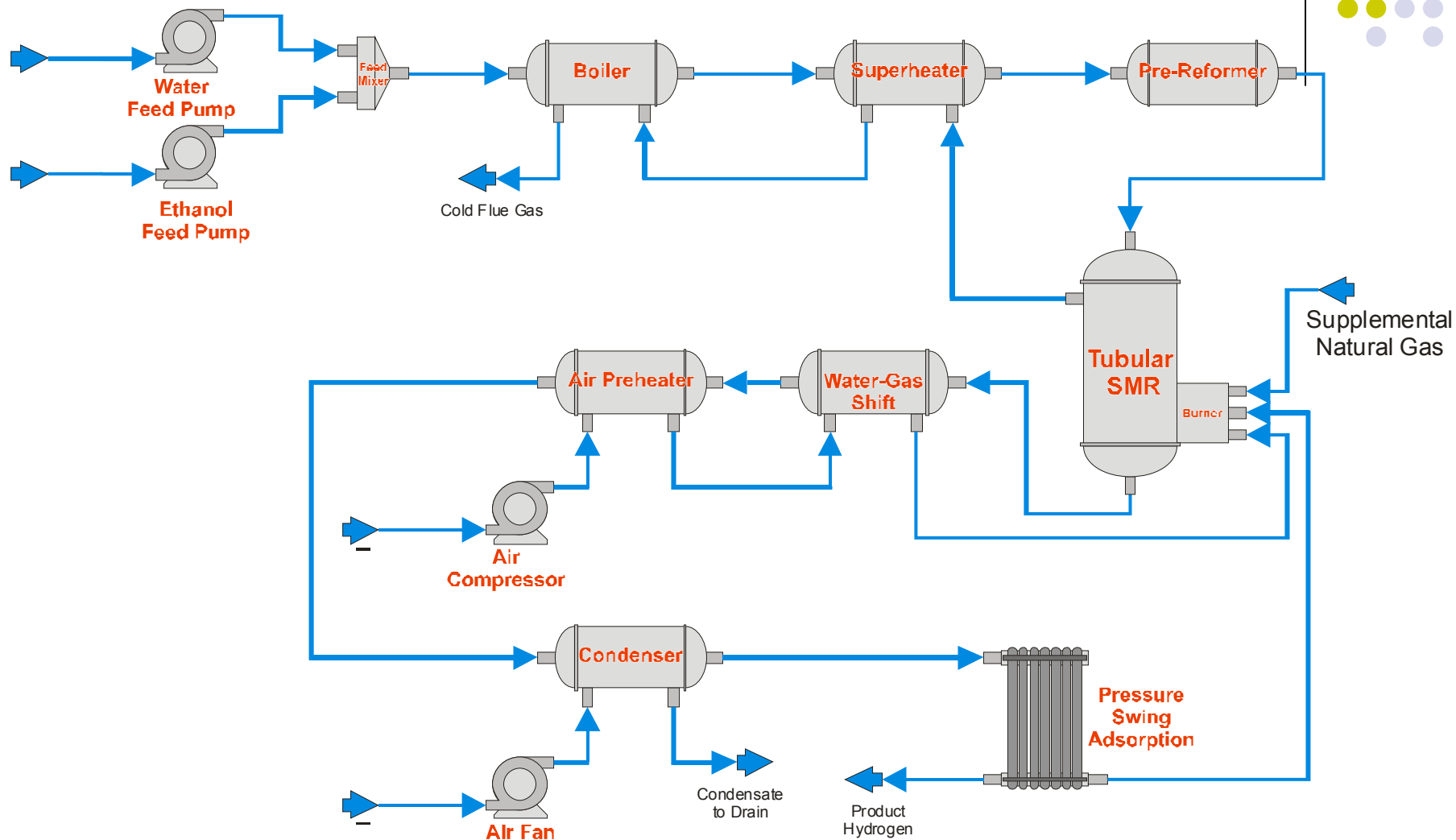
T is the membrane temperature in **°R**

R is the ideal gas constant in **ft³-atm/°R/lb-mol**

a, b are the empirical constants dependent on the material of the membrane

Therefore implied Permeability Technical Targets are:

Permeability:	2006 Status	2010 Target	2015 Target
	>454 scfh/ft²/atm^{0.5}	567 scfh/ft²/atm^{0.5}	>680 scfh/ft²/atm^{0.5}



Configurations Planned for Modeling



Baseline Configuration:

1. **Baseline Ethanol System: High temp. SR with pre-reformer & PSA**

Advanced Configurations:

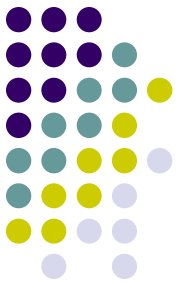
Baseline System:

2. - with membrane separation unit
3. - with combined WGS/membrane

Medium Temperature System:

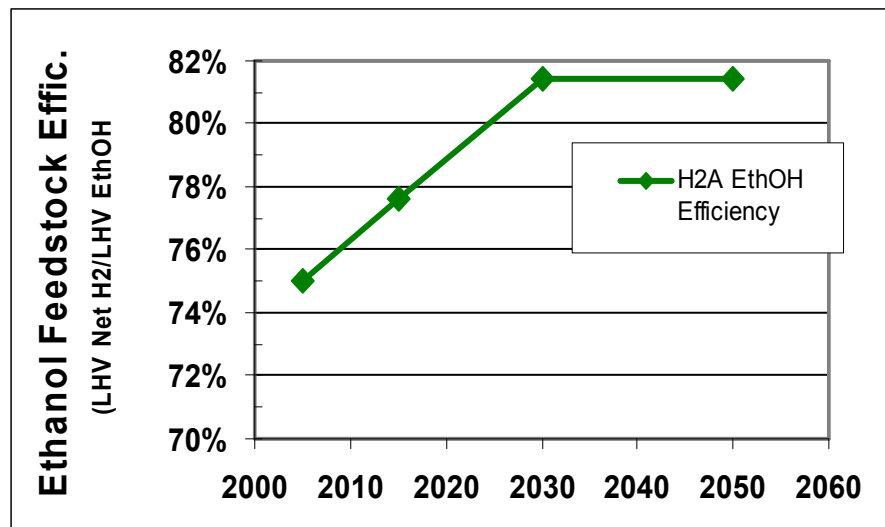
4. - with PSA
5. - with membrane separation unit
6. - with combined WGS/membrane
7. - with membrane reactor

8. **Aqueous Reformer System**



Back-up Slides describing previous H2A Ethanol Analysis

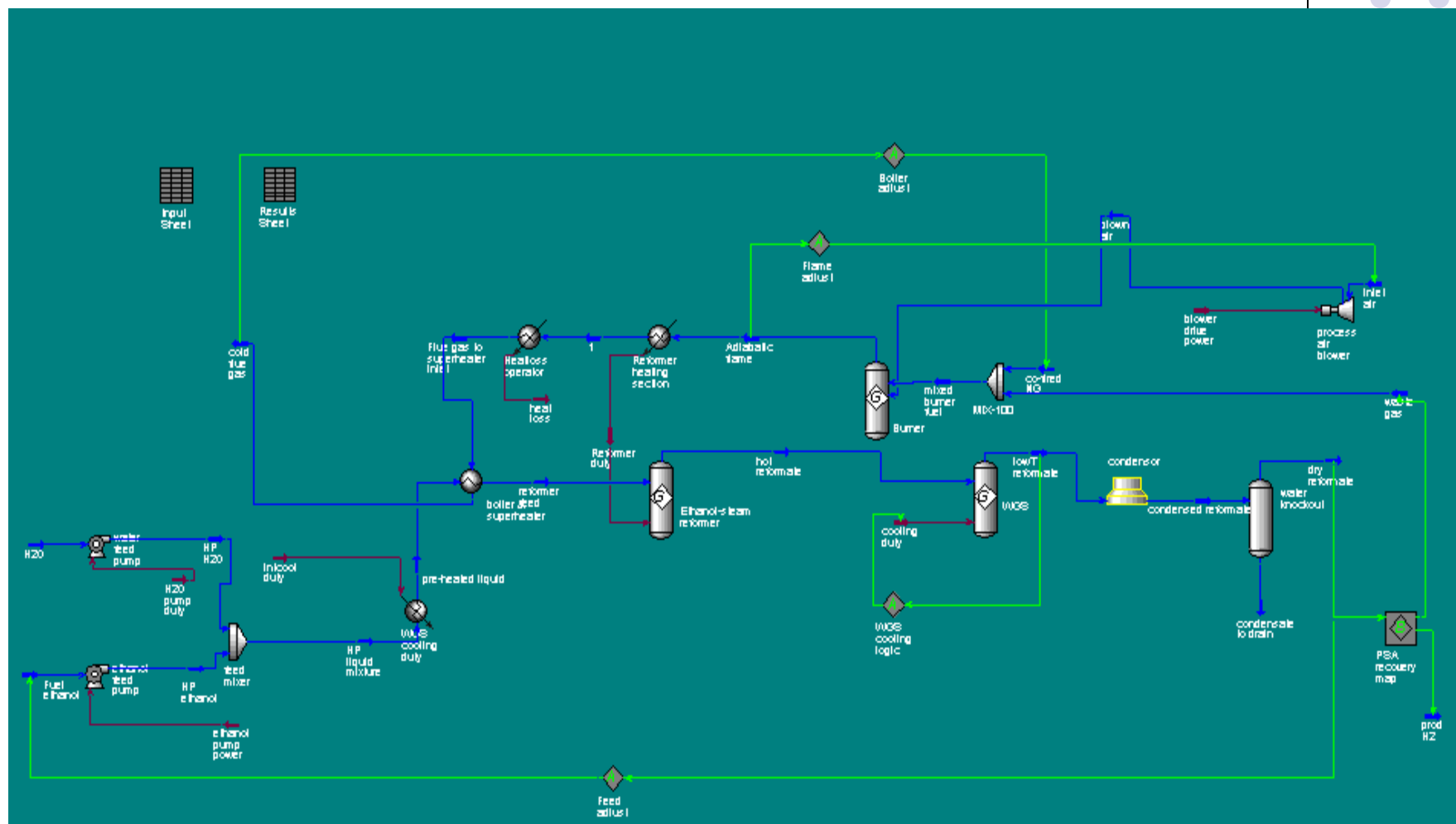
Previous H2A: System Ethanol Feedstock Efficiency (LHV)



Ethanol System Efficiency

	Current/2005	Advanced/2015	Long Term/2030
	Baseline	Baseline	Baseline
Ethanol Efficiency (LHV GJH ₂ /GJEthOH)	75.0%	77.6%	81.4%
NG Ratio (LHV GJNG/GJH ₂)	9.4%	10.0%	10.5%
Overall Energy Efficiency (LHV GJH ₂ /GJFeedstock)	70.1%	72.0%	75.0%

Previous H2A: Hysys Model of Ethanol System



Previous H2A: Other Key 1.5tpd Forecourt Ethanol Assumptions (for Current system)



Financial

- 10% real after-tax discount rate
- 70% plant utilization
- 20 year system lifetime
- 20 year analysis period
- All values in 2005\$

Other Capital Costs (Current)

- H₂ Compressor: \$4500/(kg/hr), 1500kg/day, 20% installation factor
- H₂ Storage: steel tanks at \$818/kgH₂, 1193 kg H₂ stored
- H₂ Dispensers: dual hose disp., \$22,400 each, 3 needed
- H₂ Safety Equip.: \$18,600
- Site prep, Eng. Design, Contingency: \$415k

Other Costs (Current)

- Labor: 1232 hours/yr (18h/day, 50% to fueling, 3/8 to H₂ fueling)
- Rent: \$0.5/ft², 7199ft² for H₂ operations
- Maintenance: 5%/3%/1% per yr of prod./compr./stor., \$800/yr/dispenser
- Prod. Equip. Refurbishment; 15% of initial cost every 5 yrs, complete replacement in 10yrs
Dispenser Lifetime: 10 yrs
- Ethanol Price: \$1.07/gal

Miscellaneous (Current)

- Combination Gasoline/H₂ Dispensing station (3 of 8 dispensers for H₂)

Pump Cost of H₂ from H2A Model (Forecourt EthOH)



	Levelized H ₂ Price
Current	\$4.40/kg
Advanced	\$3.84/kg
Longer-Term	\$3.60/kg

