

# Nitrided Metallic Bipolar Plates

**M.P. Brady (project lead)**

**P. F. Tortorelli**

***Oak Ridge National Laboratory***

***Oak Ridge, TN 37831-6115***

***Feb 14, 2007 Kick-Off Meeting***

# Effort Devoted to Scale Up and Demonstration of Thin Stamped Metallic Bipolar Plates

## Timeline

- Start- April, 2006 (estimated)
- Finish- April, 2008 (estimated)

## Budget

- Total project funding
  - \$4530 K (+ \$400 K Match)
- Funding for Year 1
  - \$2480 K
- Funding for Year 2
  - \$2050 K

## Barriers

- A. Durability
- B. Cost
- Targets (2010)
  - resistivity < 10 mohm-cm<sup>2</sup>
  - corrosion < 1 x10<sup>-6</sup> A/cm<sup>2</sup>
  - cost < \$5/kW

## Team Members

- ORNL (Lead)
- Allegheny Ludlum
- Arizona State University
- GenCell Corp
- LANL
- NREL

# Objective: Surface Treatment to Protect Stamped Metallic Bipolar Plates

Overall Goal: ***Demonstrate potential for metallic bipolar plates to meet 5000 h automotive durability goal at cost < \$5/kW***

Year 1 Goals:

**Single-cell fuel cell test performance for 25 cm<sup>2</sup> stamped and nitrided metallic bipolar plates equivalent to that of graphite (~1000 h, cyclic)**

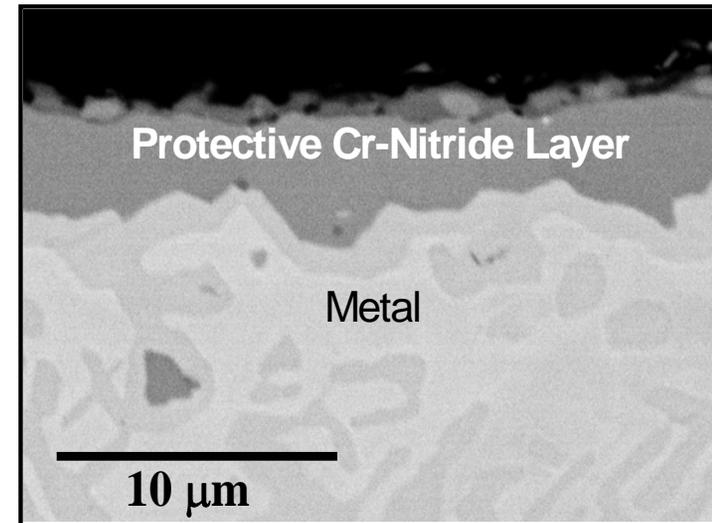
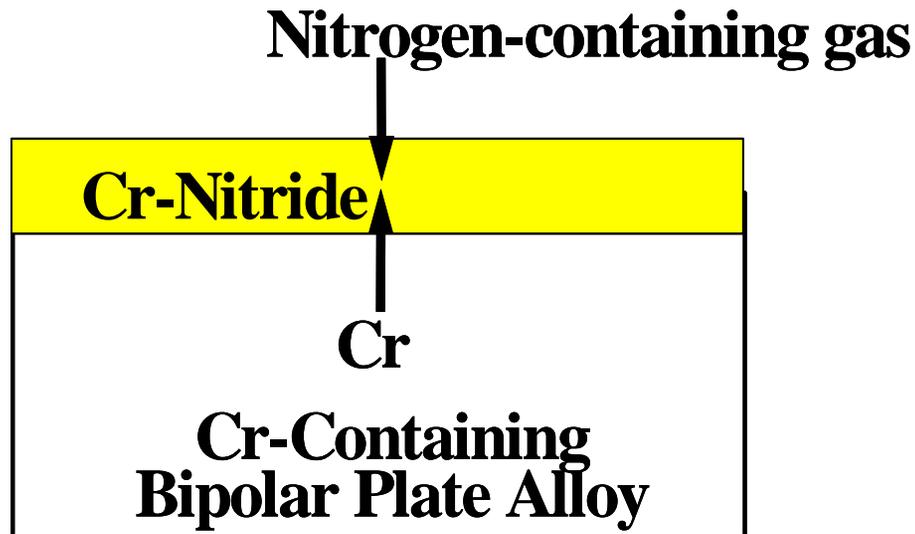
**No significant warping or embrittlement of the stamped plates by the nitriding**

Year 2 Goals:

**10 cell stack test of 250 cm<sup>2</sup> stamped and nitrided metallic bipolar plates under automotive drive-cycle conditions (~2000 h)**

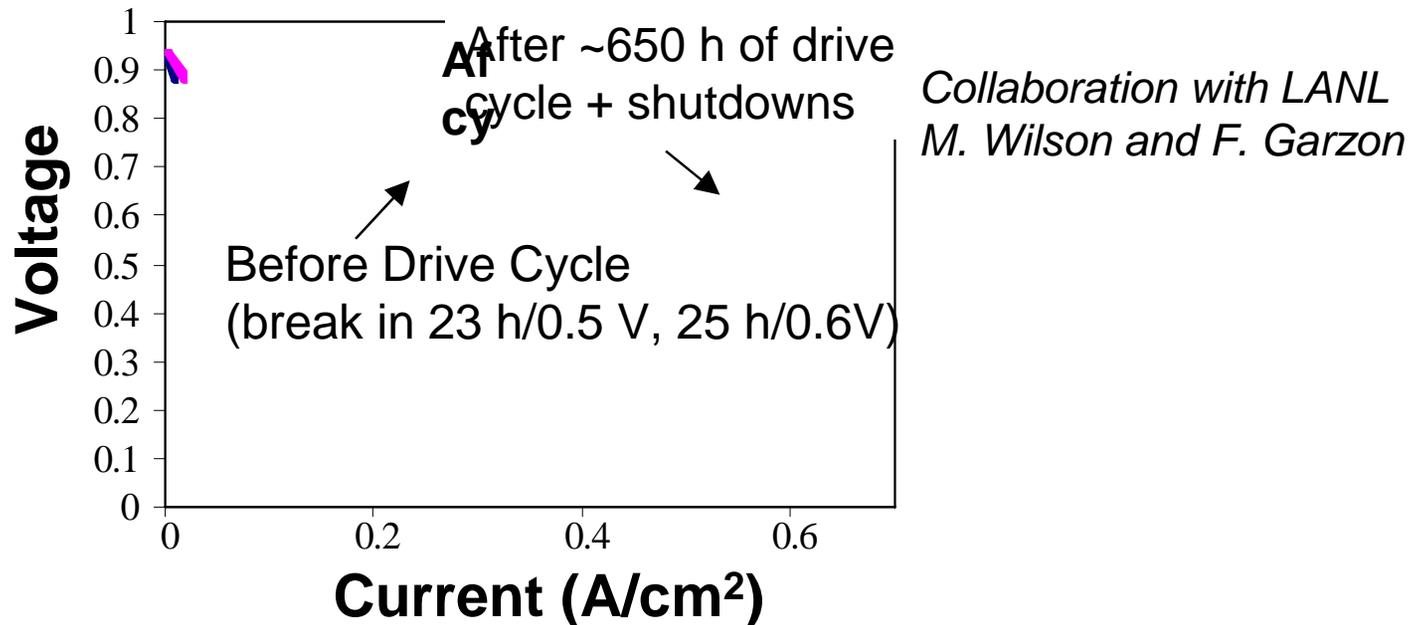
**Potential to manufacture stamped and nitrided metallic bipolar plates at < \$5/kW demonstrated**

# Approach: Thermally Grown Cr-Nitride for Protection



- **Surface conversion, not a deposited coating: High temperature favors reaction of all exposed metal surfaces**
  - No pin-hole defects (other issues to overcome)
  - Amenable to complex geometries (flow field grooves)
- **Stamp then nitride: Industrially established and cheap**

# Good Single-Cell Drive-Cycle Durability Test Results for Model Nitrided Ni-50Cr Plates



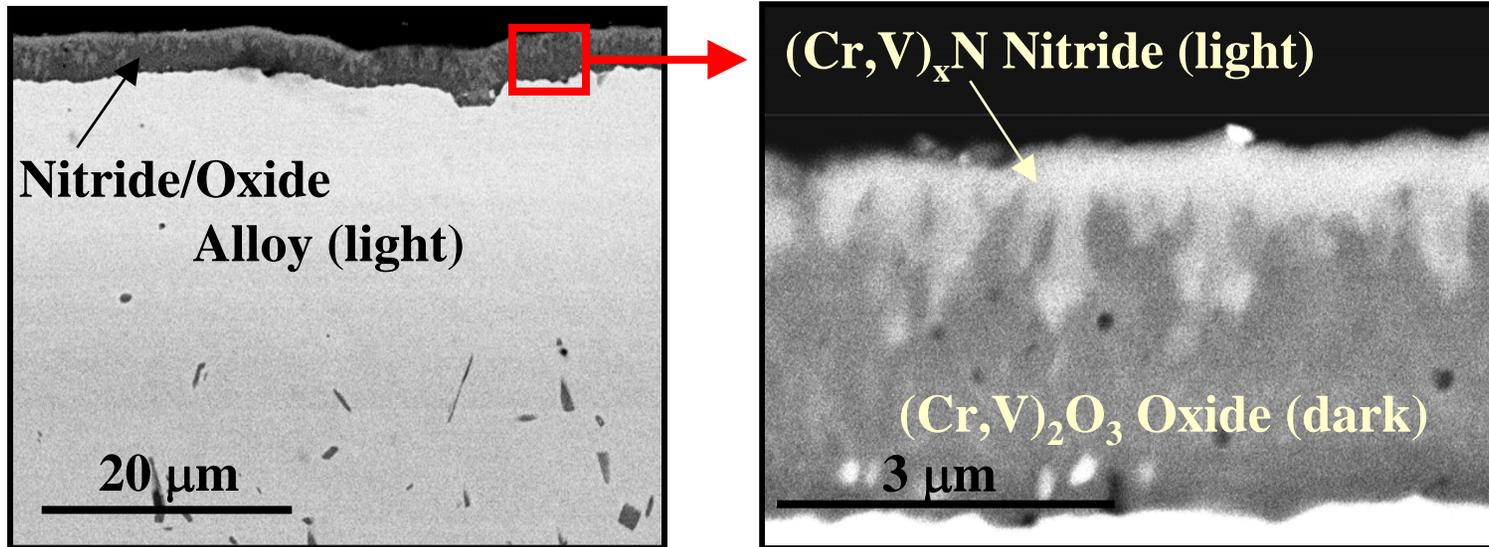
- **1160 h of drive-cycle testing** (after initial 500 h/0.7V/80°C test screening)
  - 0.94V/1 min; 0.60V/30 min; 0.70V/20 min; 0.50V/20 min
  - additional 24 full shutdowns superimposed
- No performance degradation/No attack of the Cr-nitride
  - trace level ( $2 \times 10^{-6}$  g/cm<sup>2</sup>) of Ni detected in MEA, suspect local CrNiN spots

# Need Fe-Base Alloys to Meet \$5/kW Bipolar Plate Cost Goals

- **Dense Cr-nitride surface formation demonstrated on a model Fe-base alloy, Fe-27Cr-6V wt.%**
  - pre-oxidation key to protective surface nitride formation
  - V segregation into Cr-oxide makes it more readily nitrided
- **Alloy Challenges**
  - Lower Cr and V levels to reduce alloy cost
  - Co-optimize preoxidation/nitridation to segregate Cr, V to surface
  - Down select to ferritic (cheaper) or austenitic (more formable) alloy base

# Dense, Continuous Nitride Surface Obtained

SEM Cross-Sections of Preoxidized and Nitrided Fe-27Cr-6V



- Low contact/through-thickness electrical resistance
- Low corrosion current densities under simulated anodic and cathodic conditions

# Stamped Fe-Cr-V Alloys Can Meet \$5/kW Transportation Cost Goals

## **GenCell Corp Cost Estimates for Stamped Bipolar Plates (Nitriding Costs Not Included)**

Foil Thick. (in)	Density kg/kW	Bipolar Plate Cost (\$/kW)		
		<u>\$3/lb Alloy</u>	<u>\$5/lb Alloy</u>	<u>\$7/lb Alloy</u>
0.002	0.26	\$2.31	\$3.47	\$4.58
0.004	0.38	\$3.15	\$4.26	\$6.57
0.008	0.64	\$4.86	\$7.69	\$10.51

High Cr ferritic alloys \$3-7/lb: **viable nitriding costs**

- E-BRITE® (Fe-26Cr-1Mo wt.%): \$5-7/lb commercial price for foil
- Alloy 444 (Fe-18Cr-2Mo wt.%): \$3-5/lb commercial price for foil
- Above alloys comparable to Fe-Cr-V alloys as Mo and V costs similar

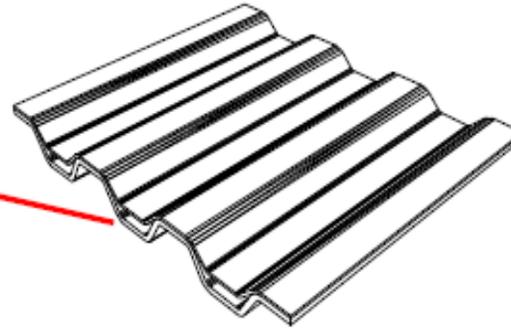
Assumptions: 360 cm<sup>2</sup> active area plate (494 cm<sup>2</sup> total area), 2 mil secondary foil for cooling (nested stacking), parallel flow field 0.025" depth, 2010 MEA target power density

# Teaming and Primary Responsibilities

- **Oak Ridge National Lab:**  
Alloy design, nitridation optimization, characterization
- **National Renewable Energy Lab:**  
Corrosion/contact resistance evaluation
- **Allegheny Ludlum:**  
Alloy foil manufacture
- **GenCell Corp:**  
Design and stamp bipolar plate flow field features
- **Arizona State University:**  
Single-cell testing (assisted by Gencell, ORNL)
- **Los Alamos National Lab:**  
Stack testing and performance assessment, characterization

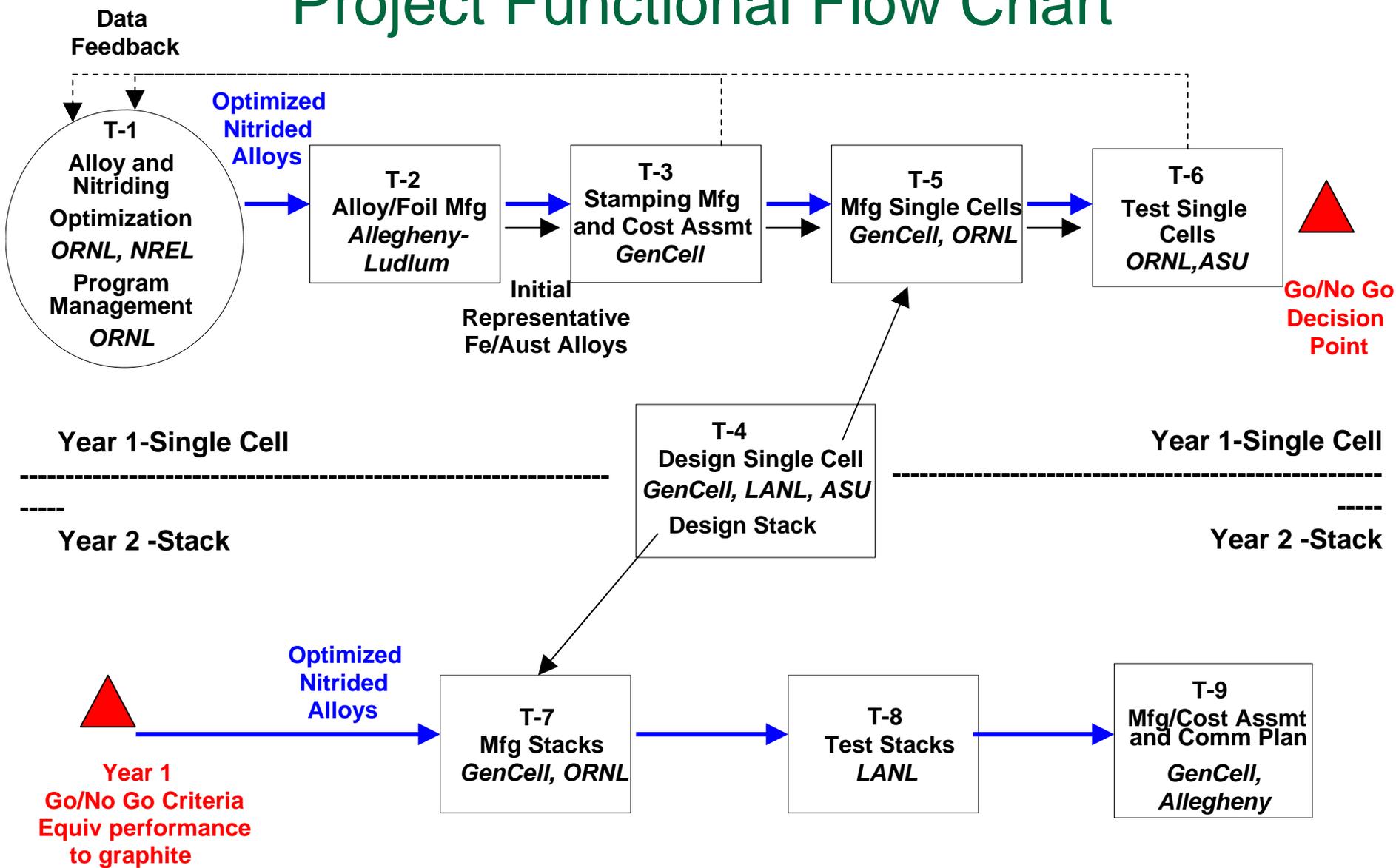
# GenCell Corp Stamped Bipolar Plate Approach

- Internal Chamber (patented)
- "Heat exchanger in each cell"
  - Thin wall, high surface area
  - From same tooling using nested sheet metal



Above shown for molten carbonate fuel cell bipolar plates, approach currently being extended to PEM and SOFC

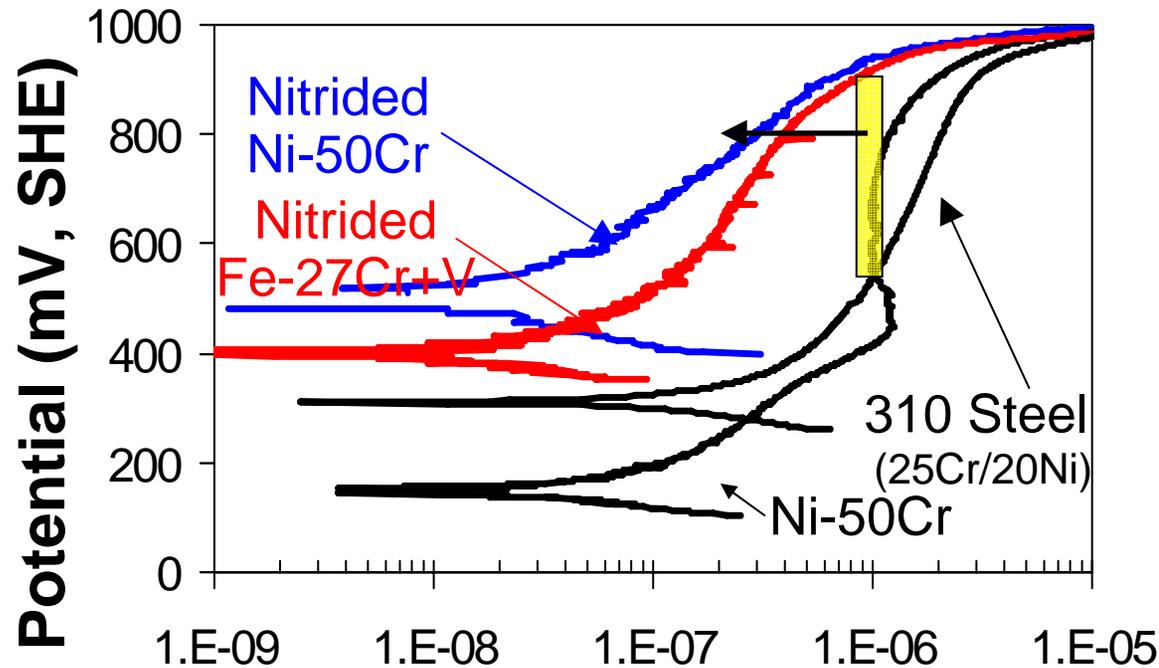
# Project Functional Flow Chart



Extra Slides for Q and A

# Vanadium Additions to Fe-27Cr Result in Protective Cr-Nitride Surface

**Polarization in Aerated pH 3 Sulfuric Acid at 80°C**

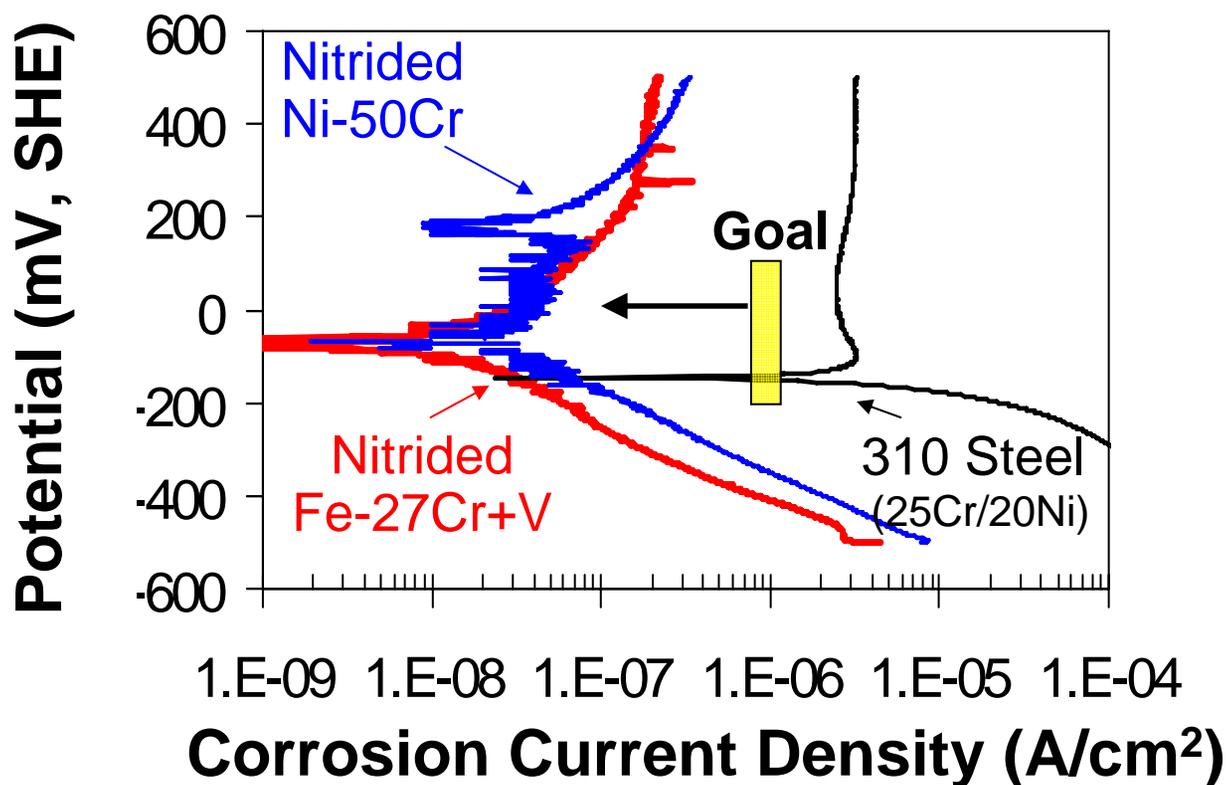


**Corrosion Current Density (A/cm<sup>2</sup>)**

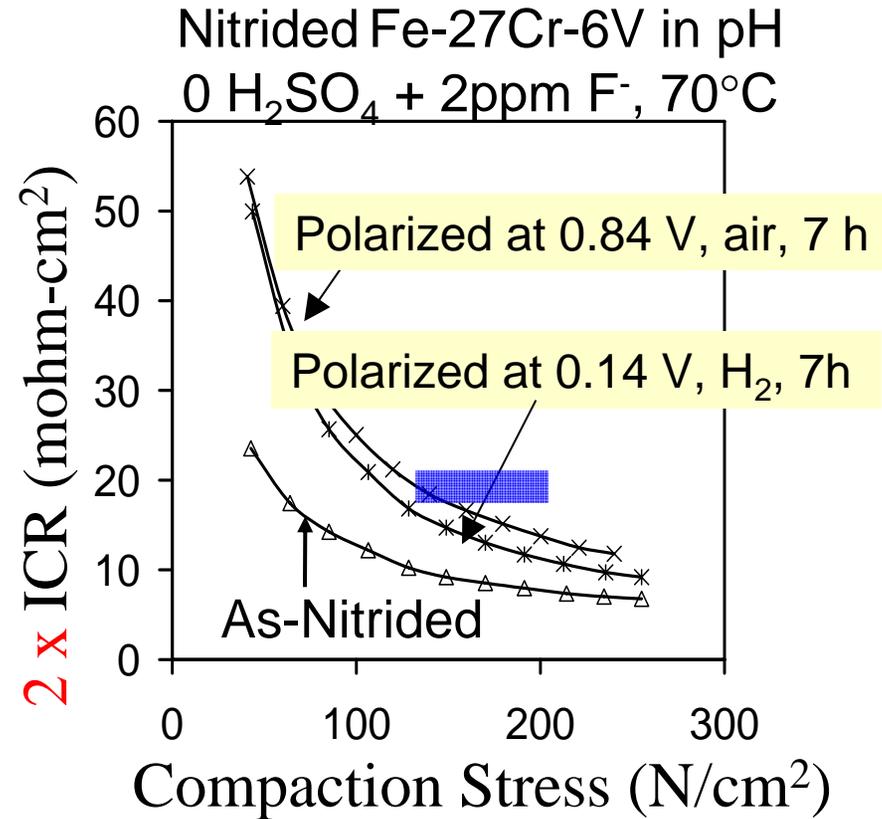
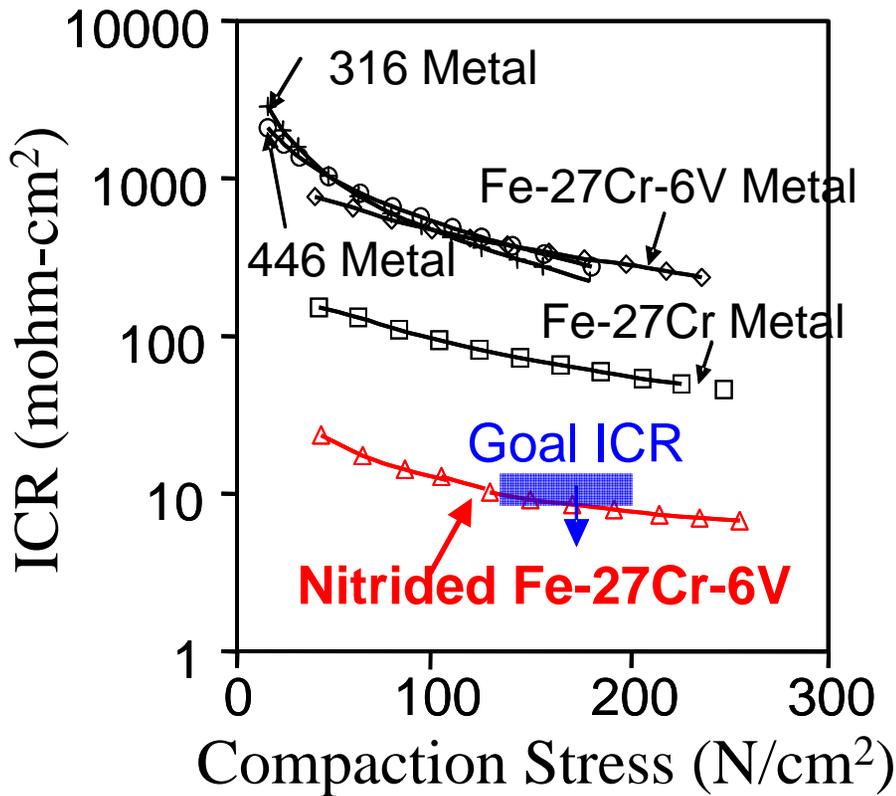
Corrosion resistance comparable to nitrided Ni-50Cr observed for nitrided Fe-27Cr-2V and Fe-27Cr-6V (850-900°C, < 24 h, N<sub>2</sub>-4H<sub>2</sub>)

# Good Corrosion Resistance Also Observed Under Simulated Anode Conditions

Polarization in Ar-4H<sub>2</sub> Purged pH 3 Sulfuric Acid at 80°C



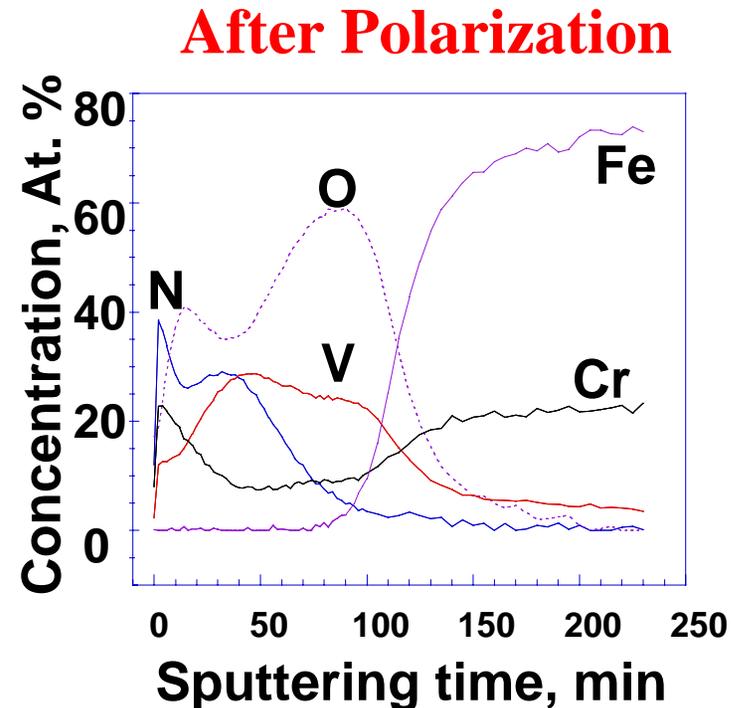
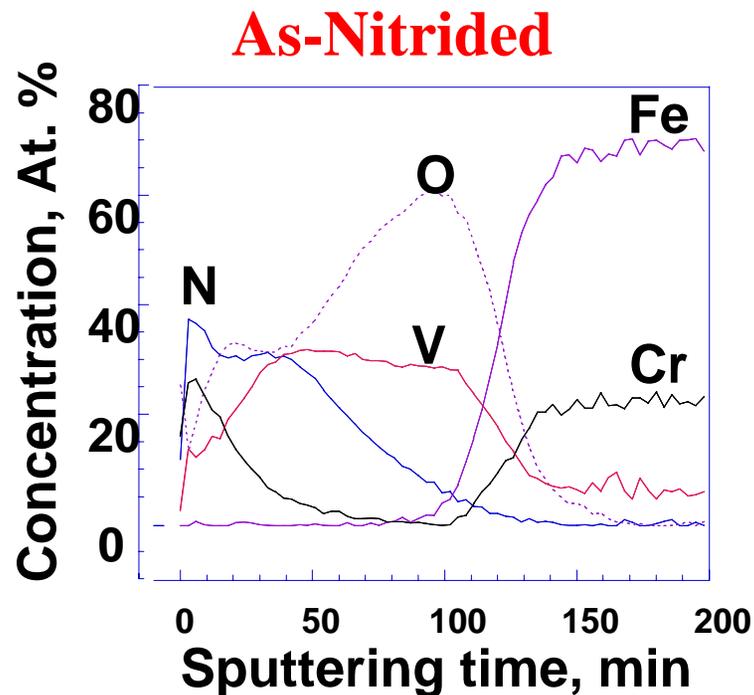
# Nitrided Fe-27Cr+V Meets and Maintains Contact Resistance Goal



- Nitridation significantly reduces interfacial contact resistance (ICR)
- Slight increase in ICR on polarization-still meets goal
- Untreated stainless steels don't meet ICR goals

# Little Effect of Polarization on Surface Chemistry of Nitrided Fe-27Cr-6V

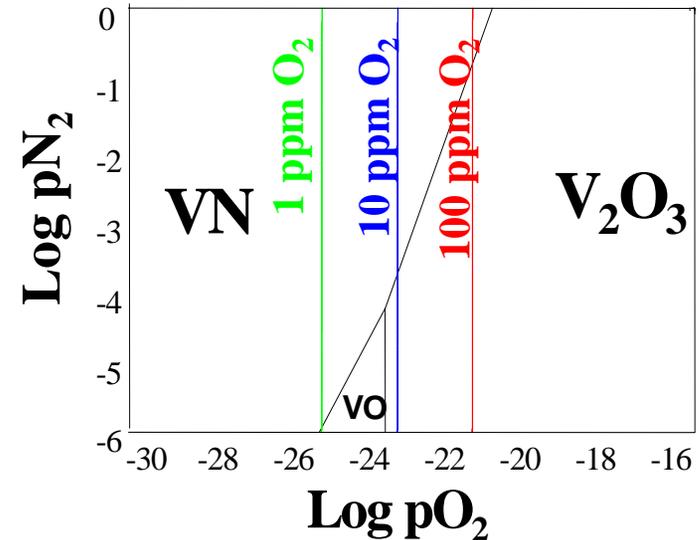
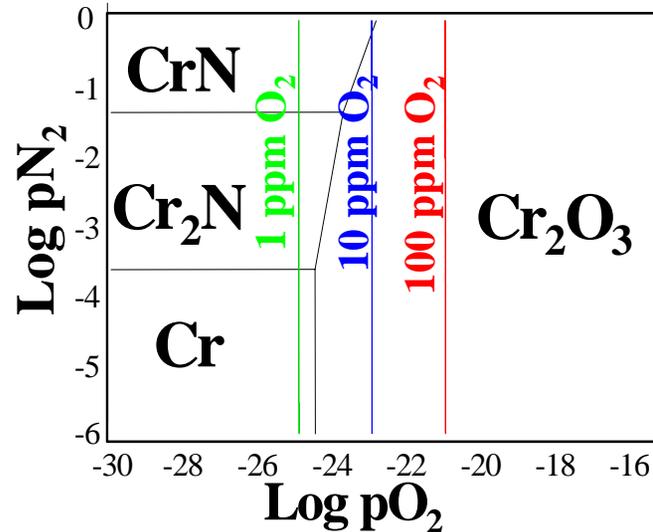
## Auger Electron Spectroscopy of Nitrided Fe-27Cr-6V



- Polarized 7 h at 0.84 V SHE in pH 0  $\text{H}_2\text{SO}_4$  + 2 ppm  $\text{F}^-$  air purged at 70 °C (similar results under  $\text{H}_2$ -purged anodic conditions)
- No Fe detected in nitrided surface, **oxygen present** in surface

# V Additions Destabilize Oxide Relative to Nitride Compared to Cr

## 900°C Predominance Diagrams



- Order of magnitude greater O<sub>2</sub> impurity stability for VN relative to CrN at 900°C in N<sub>2</sub>-4H<sub>2</sub> (100 vs 10 ppm O<sub>2</sub>)
- V works because Cr<sub>2</sub>O<sub>3</sub>-V<sub>2</sub>O<sub>3</sub>; Cr<sub>2</sub>N-V<sub>2</sub>N; CrN-VN all mutually soluble
- V<sub>2</sub>O<sub>3</sub> and Cr-doped V<sub>2</sub>O<sub>3</sub> also conductive – combined with intermixed morphology and N<sub>2</sub>-doping yields good ICR values