
From Climate Data to Accelerated Test Conditions

Michael Köhl

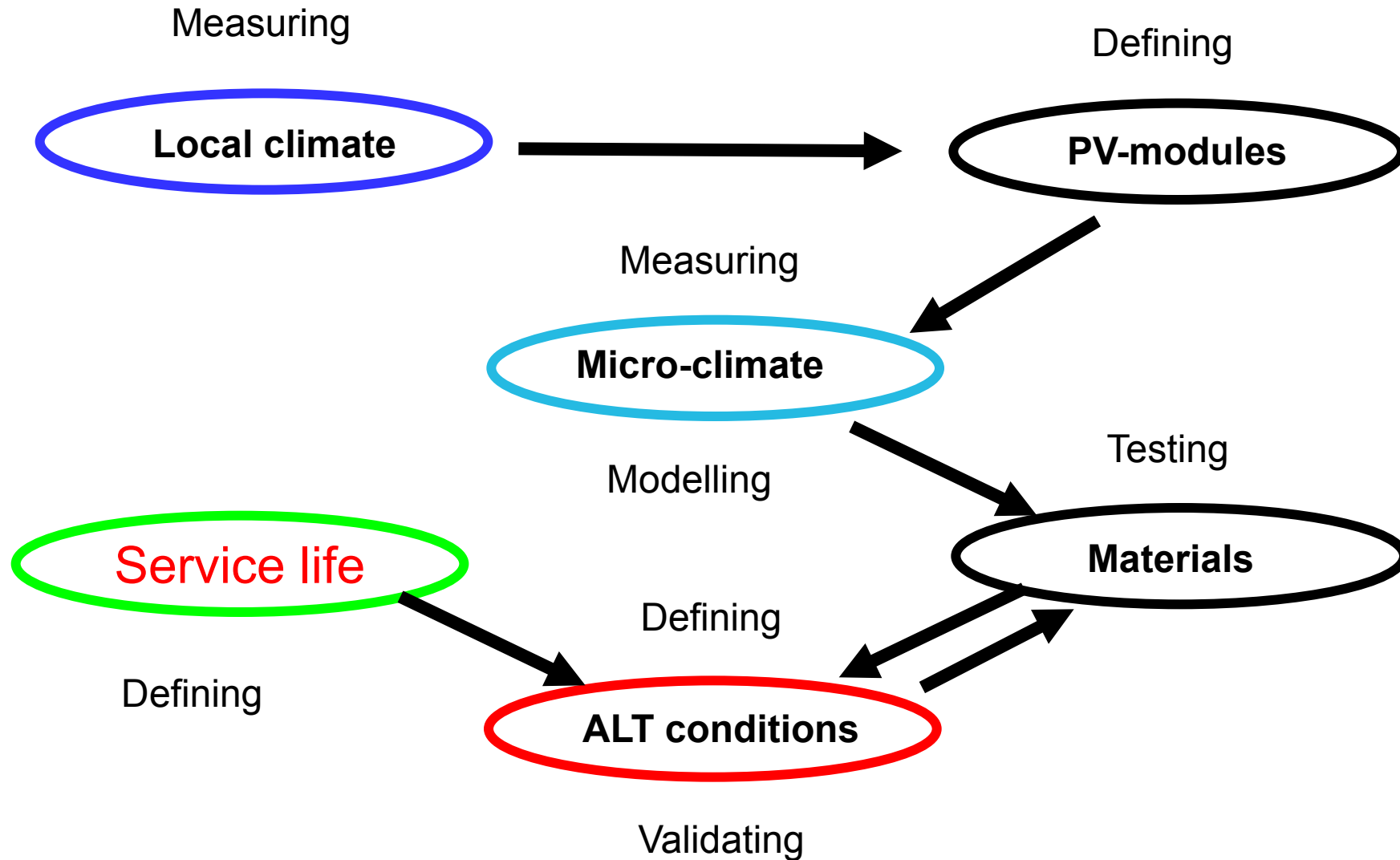
Fraunhofer Institute for Solar Energy Systems

Freiburg, Germany

Presented at the PVMRW, Golden, February 2011

General methodology

Modeling the ALT conditions based on realistic loads



Simple deterministic model for aging processes: Time-transformation functions

Changes of property **P** after the testing time Δt_i

$$\Delta P = \sum_{j=1}^m \{$$

Temperature

$$+ A \Delta t_i \exp[-E_A / RT_i]$$

Moisture

$$+ B \Delta t_i f(\text{rh})_i \exp[-E_B / RT_i]$$

UV-Radiation

$$+ C \Delta t_i I_i^n \exp[-E_C / RT_i]$$

T cycles

$$+ D \Delta t_i f(\Delta T)_i \exp[-E_D / RT_i]$$

Potential I D

$$+ E \Delta t_i f(P)_i f_p(\text{rh})_i \exp[-E_E / RT_i]$$

Salt

$$+ F \Delta t_i f(S)_i f_p(\text{rh})_i \exp[-E_F / RT_i]$$

.....

$$+ \dots X \Delta t_i I_i^n f(X)_i \exp[-E_X / RT_i] \dots \}$$

Other degradation factors or synergistic effects



**Sample dependent degradation
process parameters**

Module temperature T

Micro-climatic stress factor

Time-interval Δt_i

Simple deterministic model for aging processes: Time-transformation functions

Changes of property P after the testing time Δt_i

Degradation factor $\Delta P = \sum_{j=1}^m \{$

Temperature $+ A \Delta t_i \exp[-E_A / RT_i]$

Moisture $+ B \Delta t_i f(\text{rh})_i \exp[-E_B / RT_i]$

UV-Radiation $+ C \Delta t_i I_i^n \exp[-E_C / RT_i]$

T cycles $+ D \Delta t_i f(\Delta T)_i \exp[-E_D / RT_i]$

Potential I D $+ E \Delta t_i f(P)_i f_p(\text{rh})_i \exp[-E_E / RT_i]$

Salt $+ F \Delta t_i f(S)_i f_p(\text{rh})_i \exp[-E_F / RT_i]$

..... $+ \dots X \Delta t_i I_i^n f(X)_i \exp[-E_X / RT_i] \dots \}$



**Sample dependent degradation
process parameters**

Starting point: Outdoor exposure testing

Sites with extreme stresses

City or reference:
Freiburg Germany



Desert
Sede Boqer
Israel

Alpes
Zugspitze
Germany

Tropical
Serpang
Indonesia

Maritimes
Pozo Izquierdo
Gran Canaria

Monitoring degradation factors for modelling degradation

Measurement of module performance over time for validation of ALT

End point: Outdoor exposure anywhere

Sites with climatic conditions known for one year at least

Examples (irradiation, wind, temperature, humidity data from 2007):

	Average temperature	Irradiation	UV dose
Goodwin Creek (warm and humid)	16,6 °C	1631 kWh/m²a	83,20 kWh/m² a
Desert Rock (Hot and dry)	19,0 °C	2095 kWh/m²a	106,87 kWh/m² a

Temperature

Difficulties:

1. Micro – climate (module temperature depends on module and climate)
2. Transient behaviour (changing temperature continuously, but delayed)
3. Accelerator for all degradation processes

Pay attention to thresholds changing degradation processes:

„ You never got a chicken by boiling an egg“

Outdoor testing

Temperature monitoring

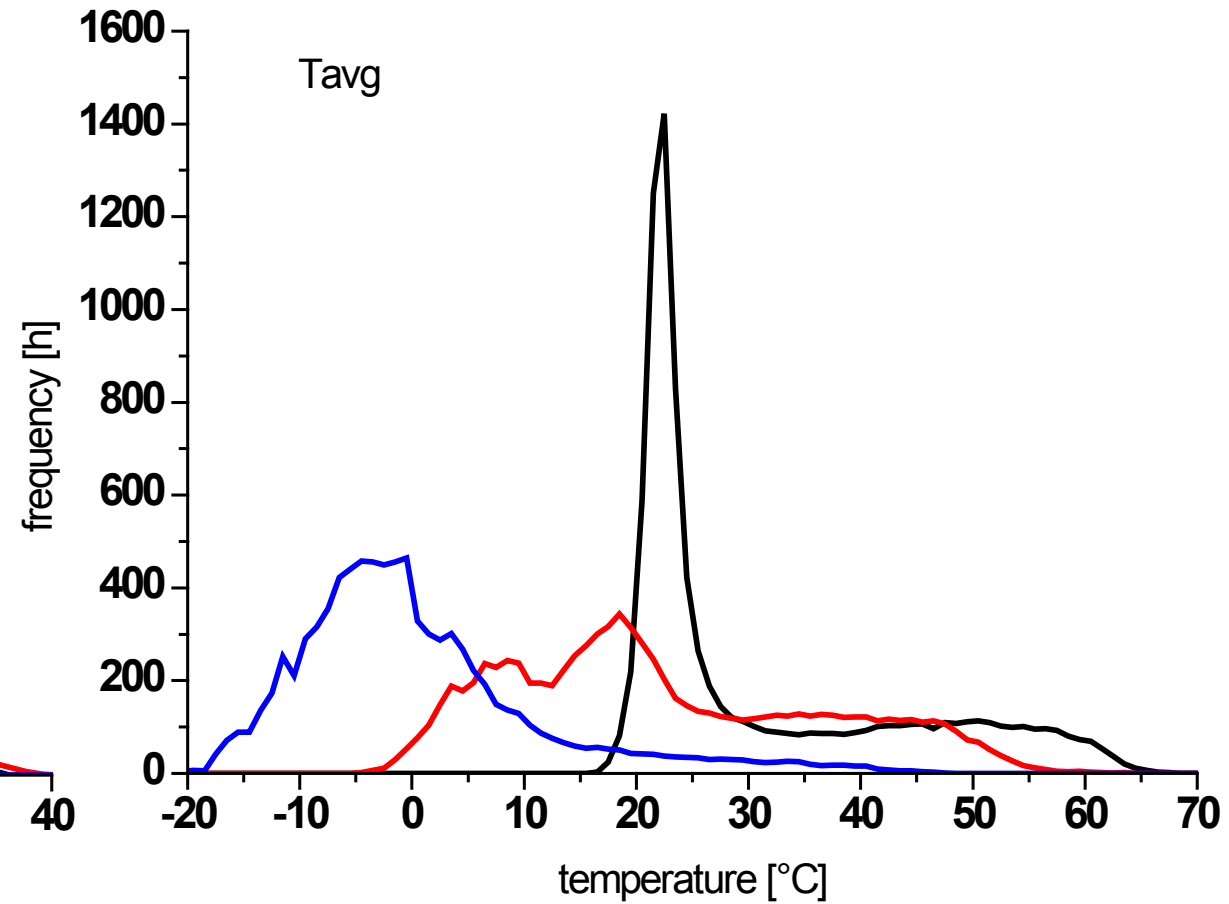
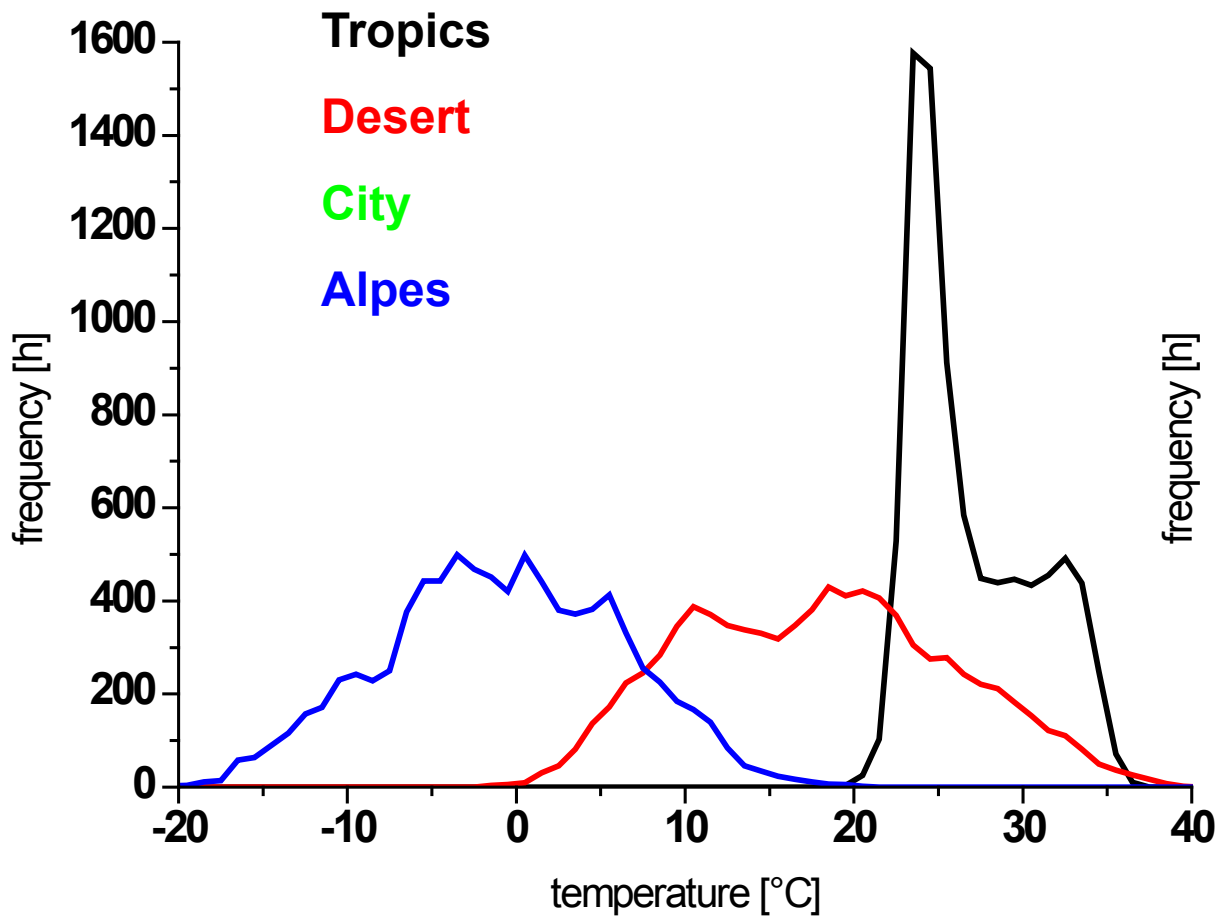
Macro – climate

=>

Micro – climate

Ambient temperature

Average module temperature (c-Si)

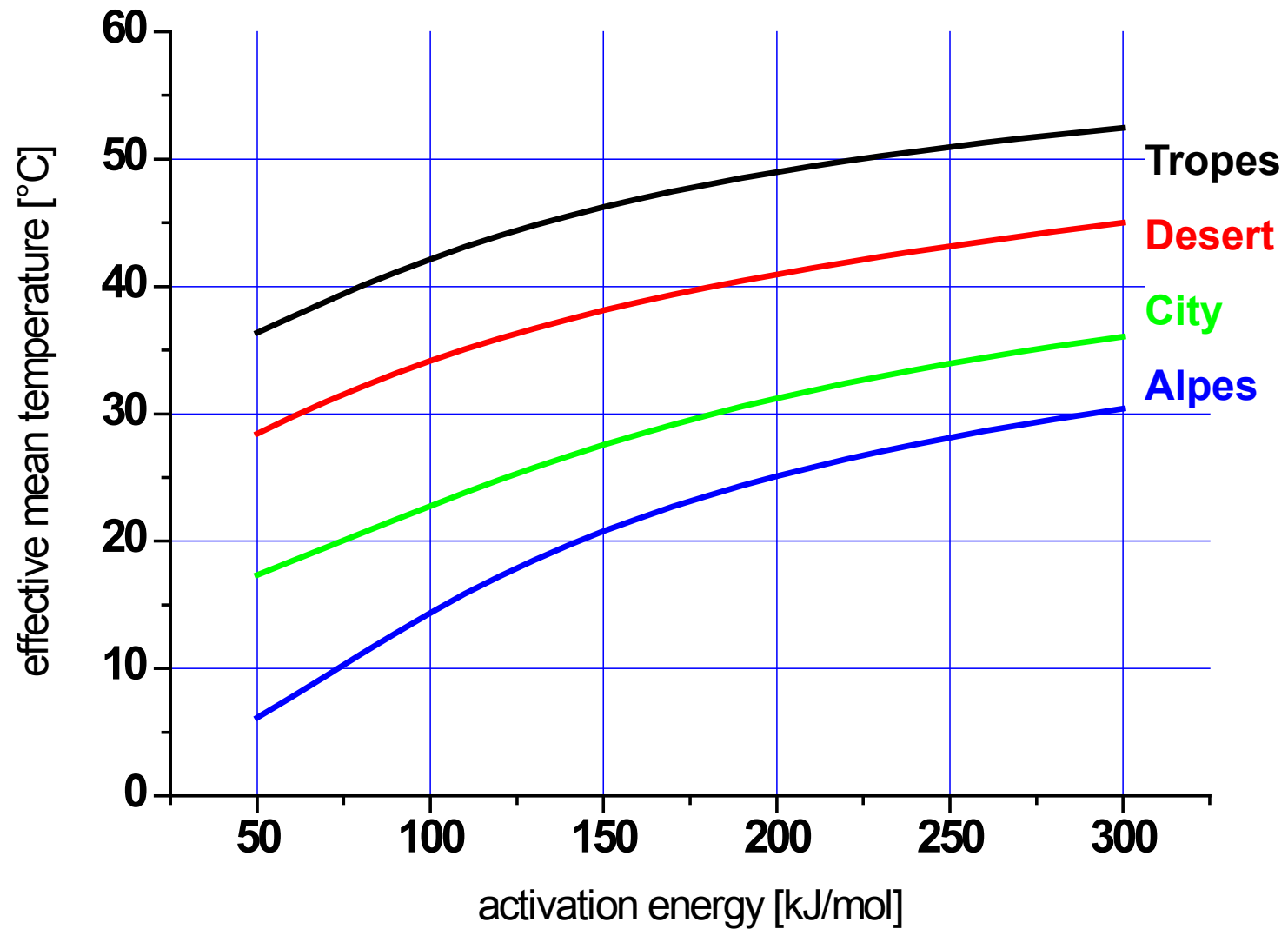


$$\exp[-E_p / RT_{\text{eff}}] = 1 / (t_{\text{max}} - t_{\text{min}}) \int_{t_{\text{min}}}^{t_{\text{max}}} \exp[-E_p / RT(t)] \Delta t$$

Effective Mean Temperature,

Constant test temperature that
Corresponds to the natural load in
the same period

Depends on the activation energy
of the degradation process



Life testing for degradation factor temperature

If there would be a degradation process without any external reaction partners

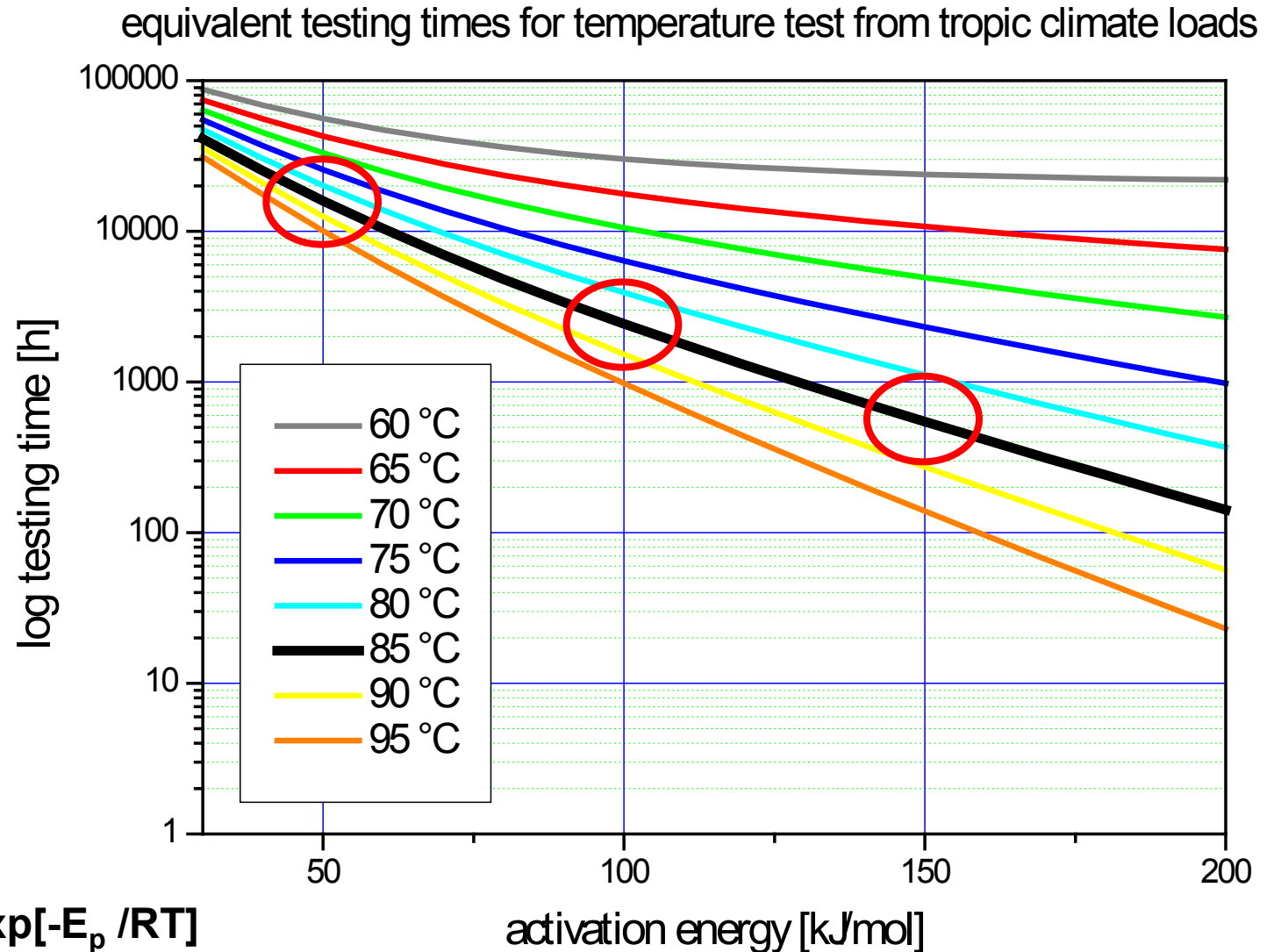
Might be tested simultaneously with the damp-heat test:

Some 100 to 10000 h

Equivalent Temperature Testing Times

for c-Si

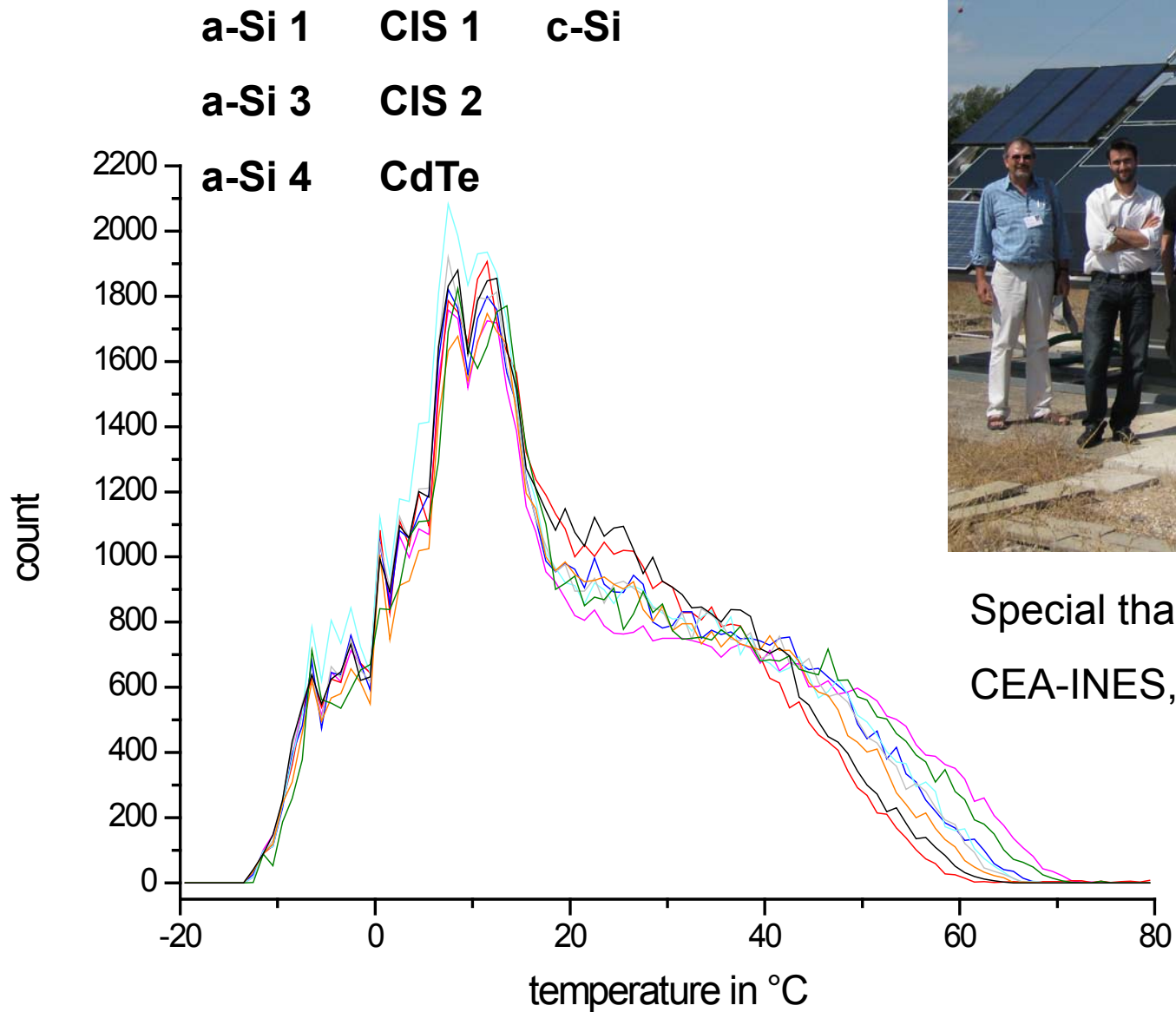
for 25 a in tropical climates



$$t_{\text{test}} = 25 \cdot 8760 \exp[-E_p / RT_{\text{eff}}] / \exp[-E_p / RT]$$

Histogram of measured module temperatures in Cadarache, F

What about Thin Film Modules?



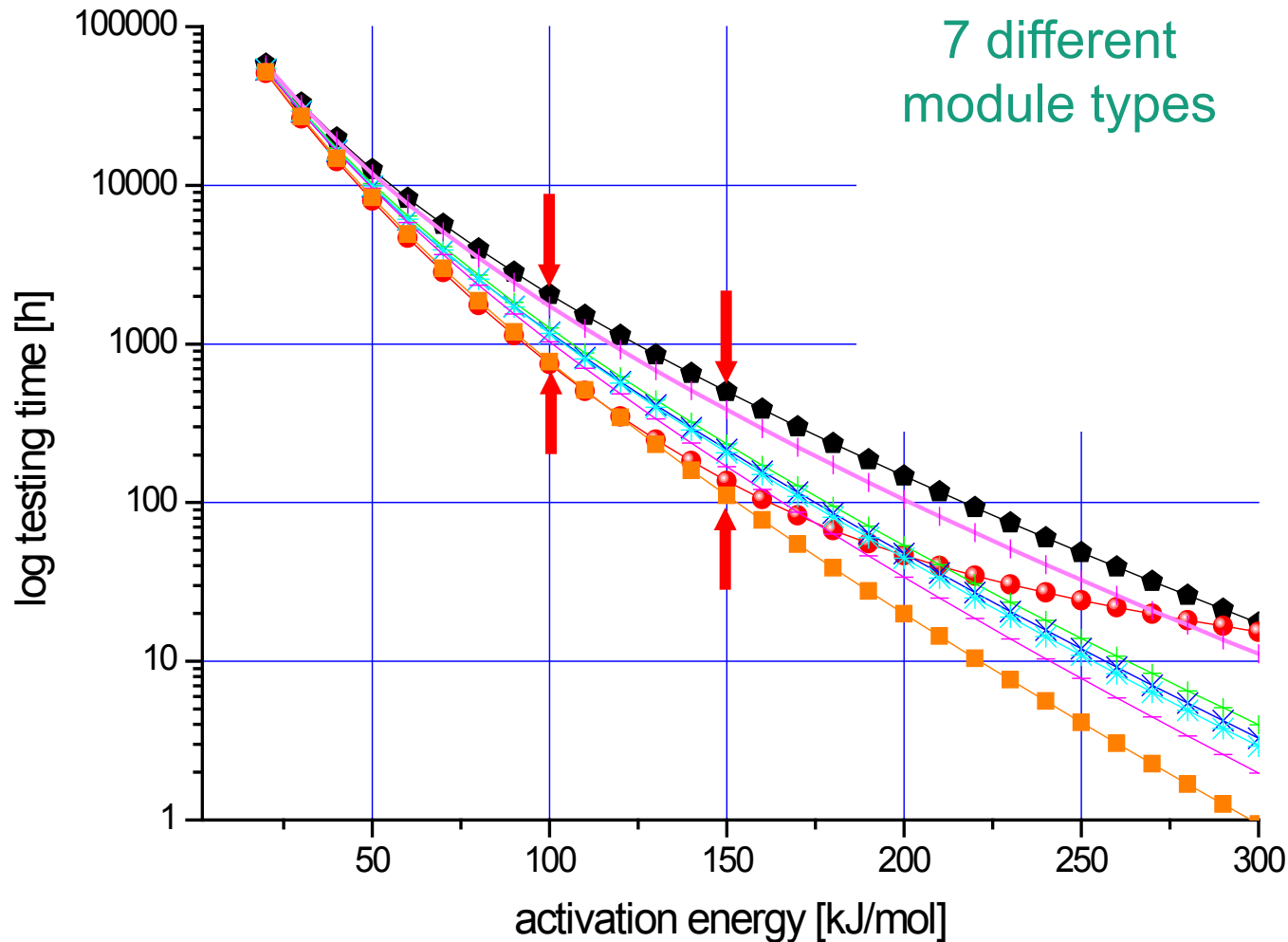
Special thanks to Antoine Guerin de Montgareuil,
CEA-INES, Cadarache, France

Module temperature for one year

Corresponding temperature testing times at 85°C for 25 a exposure in Cadarache, France

based on monitored module temperatures

testing times @ 85°C for different thin film modules exposed in Cadarache

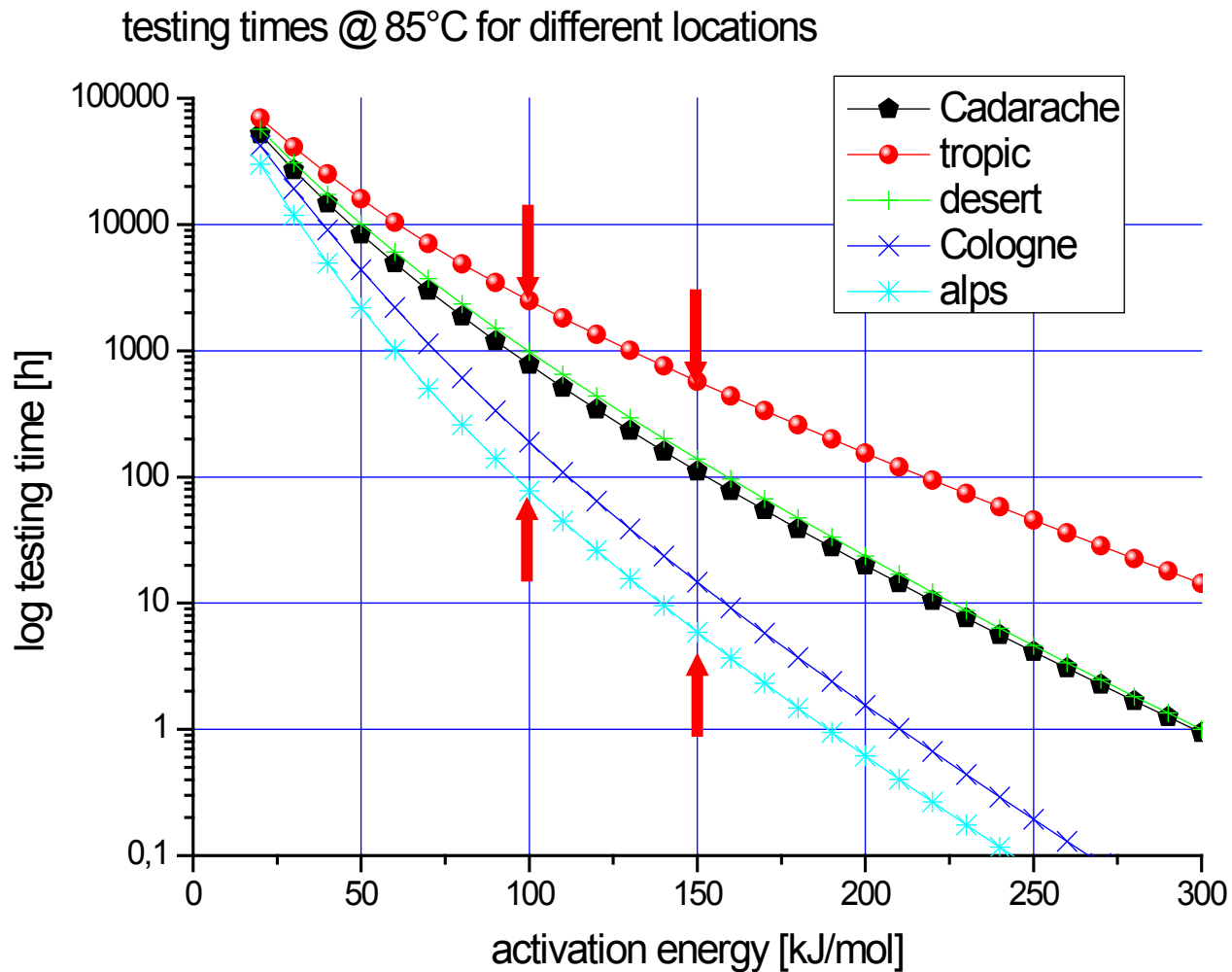


Different cell-types:

Factor 2 – 4 in testing time (depending on the degradation processes)

In the range of damp/heat

Corresponding temperature testing times at 85°C for 25 a exposure of c Si modules in different climates based on monitored module temperatures



Worst case tropics



Different climate-types:

Factor 20 – 100 in testing time (depending on the degradation processes)

Physical modeling of module temperature for each of the different module types using David Faiman's approach (could be King, Fuentes.....as well)

Macro – climate

=> Micro – climate

Irradiation, wind, ambient temperature

=> T_{mod}

$$T_{mod} = T_{amb} + \frac{H}{U_0 + U_1 \cdot v}$$

T_{mod} module temperature

T_{amb} ambient temperature

v wind velocity

H solar radiation

U_0 , U_1 = module dependent parameters

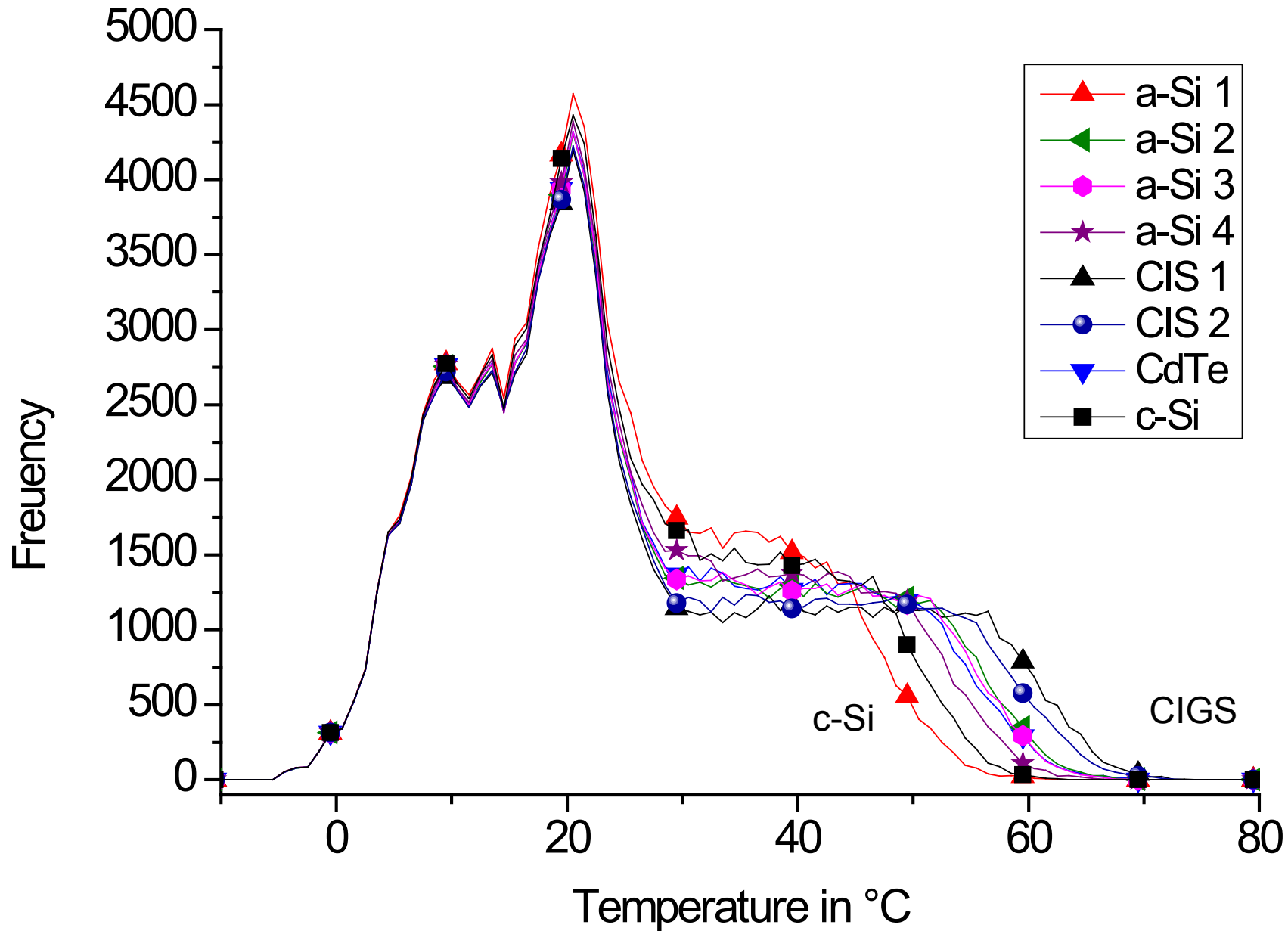
Neglected: IR-radiation exchange and natural convection

The parameters U are module-specific but location independent

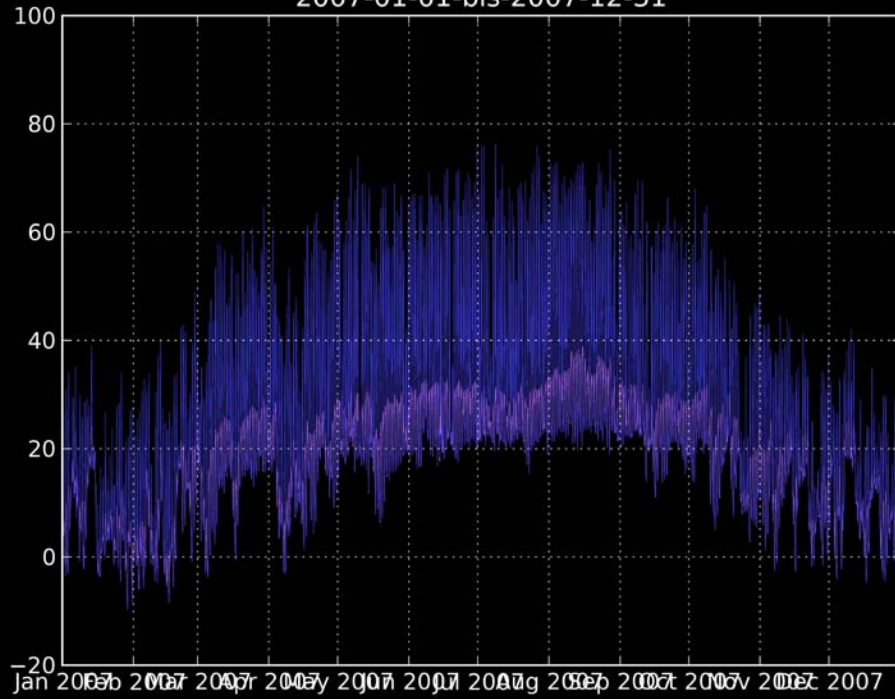
	U1	U0
a-Si 1	10,7	25,7
a-Si 3	5,8	25,8
a-Si 4	4,3	26,1
CIS 1	3,1	23,0
CIS 2	4,1	25,0
CdTe	5,4	23,4
c-Si	6,2	30,0

M.Koehl et.al.: Modelling of the nominal operating cell temperature based on outdoor weathering, Sol. Energy Mat. Sol. Cells (2011)

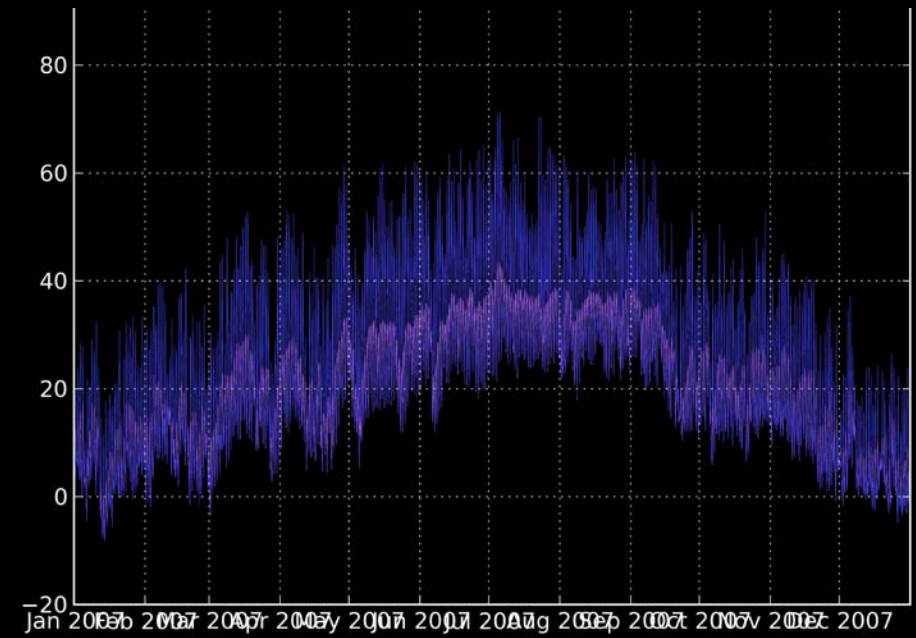
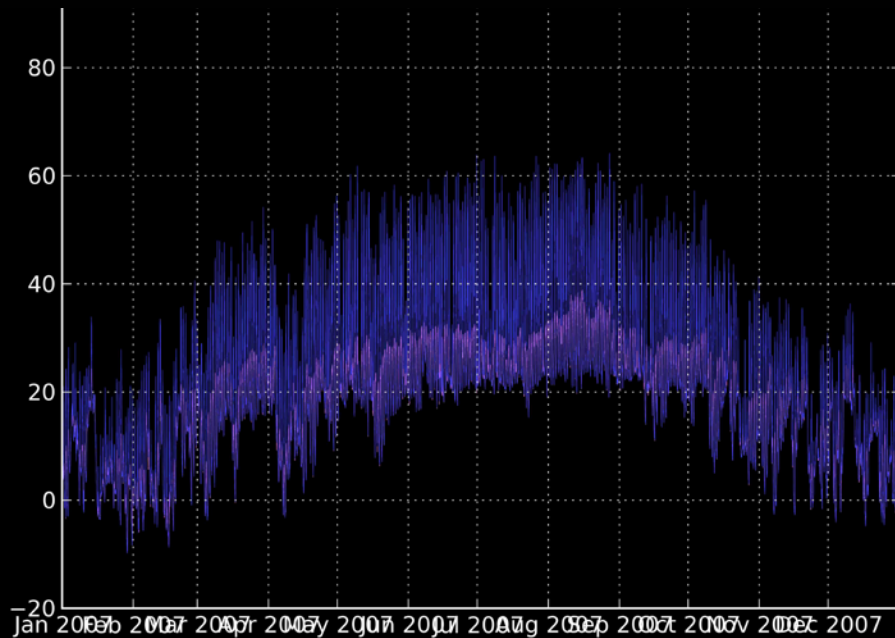
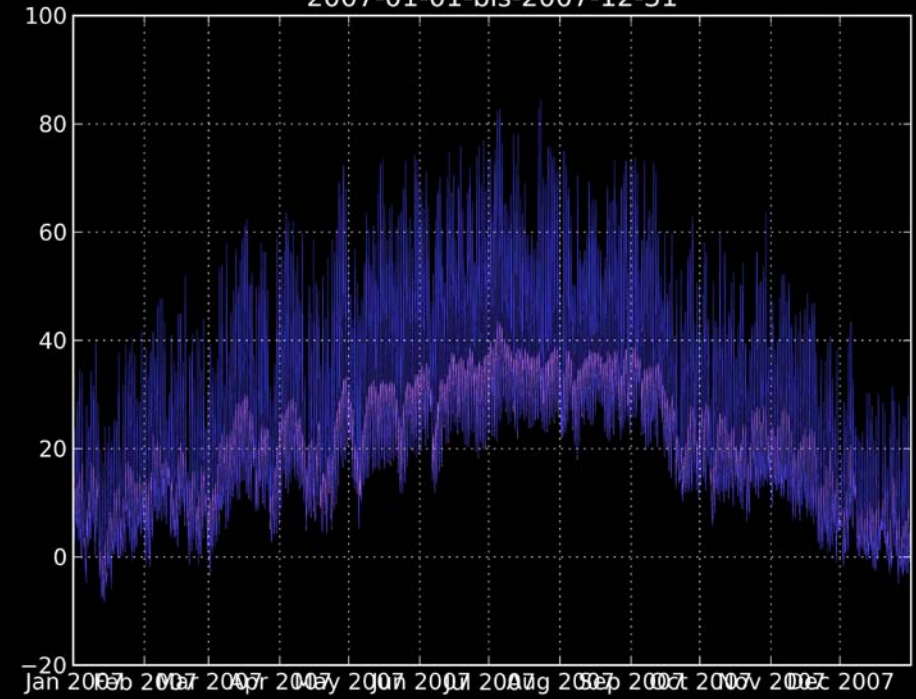
Histogram of simulated module temperatures in the Negev



Goodwin Creek|Tmod & Tamb (type thin-film)
2007-01-01-bis-2007-12-31



Desert Rock|Tmod & Tamb (type thin-film)
2007-01-01-bis-2007-12-31



Temperature load

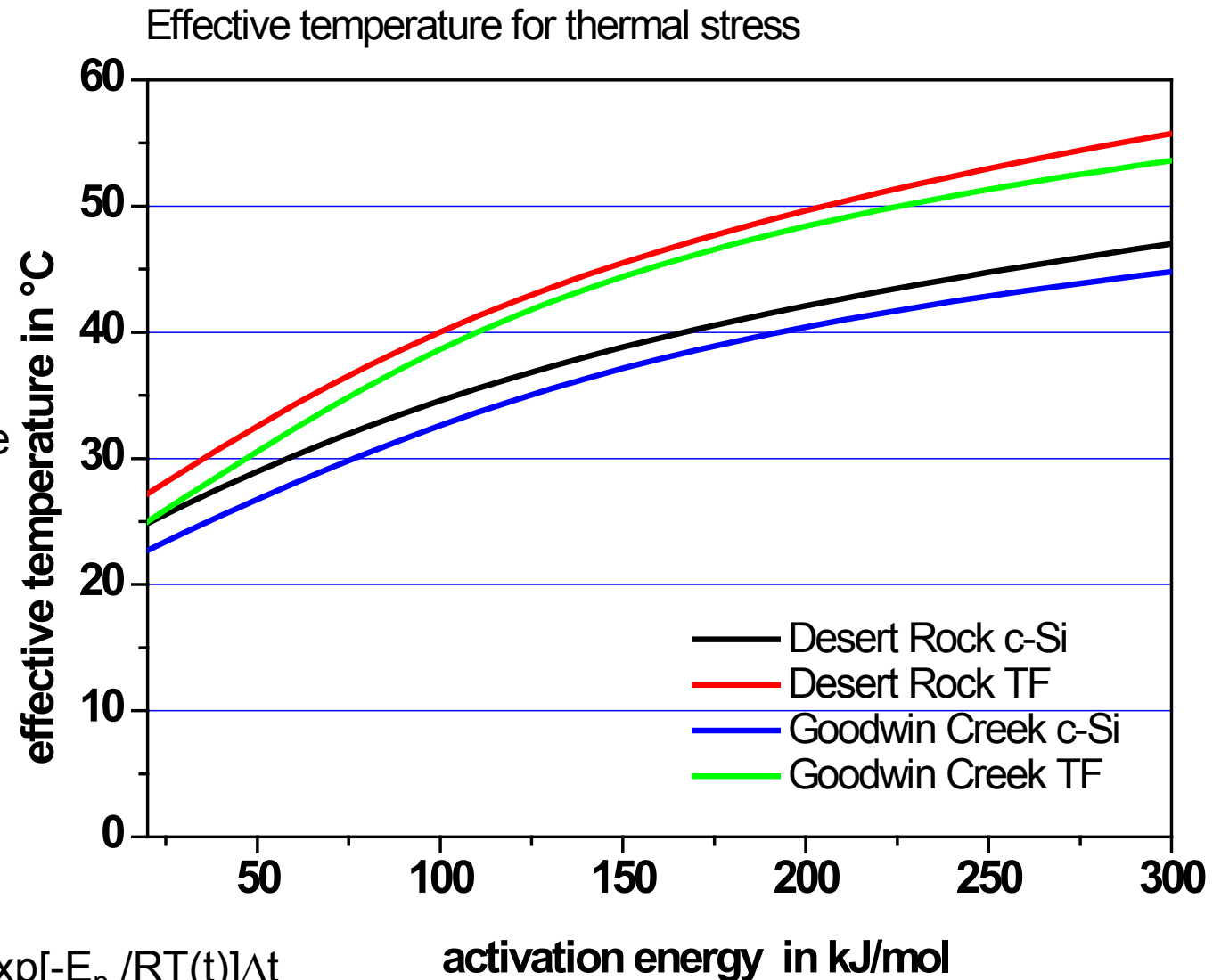
Accelerator for all degradation processes

Effective temperature:

The constant temperature needed for obtaining the same degradation as for outdoor exposure

Characteristic for location and module type

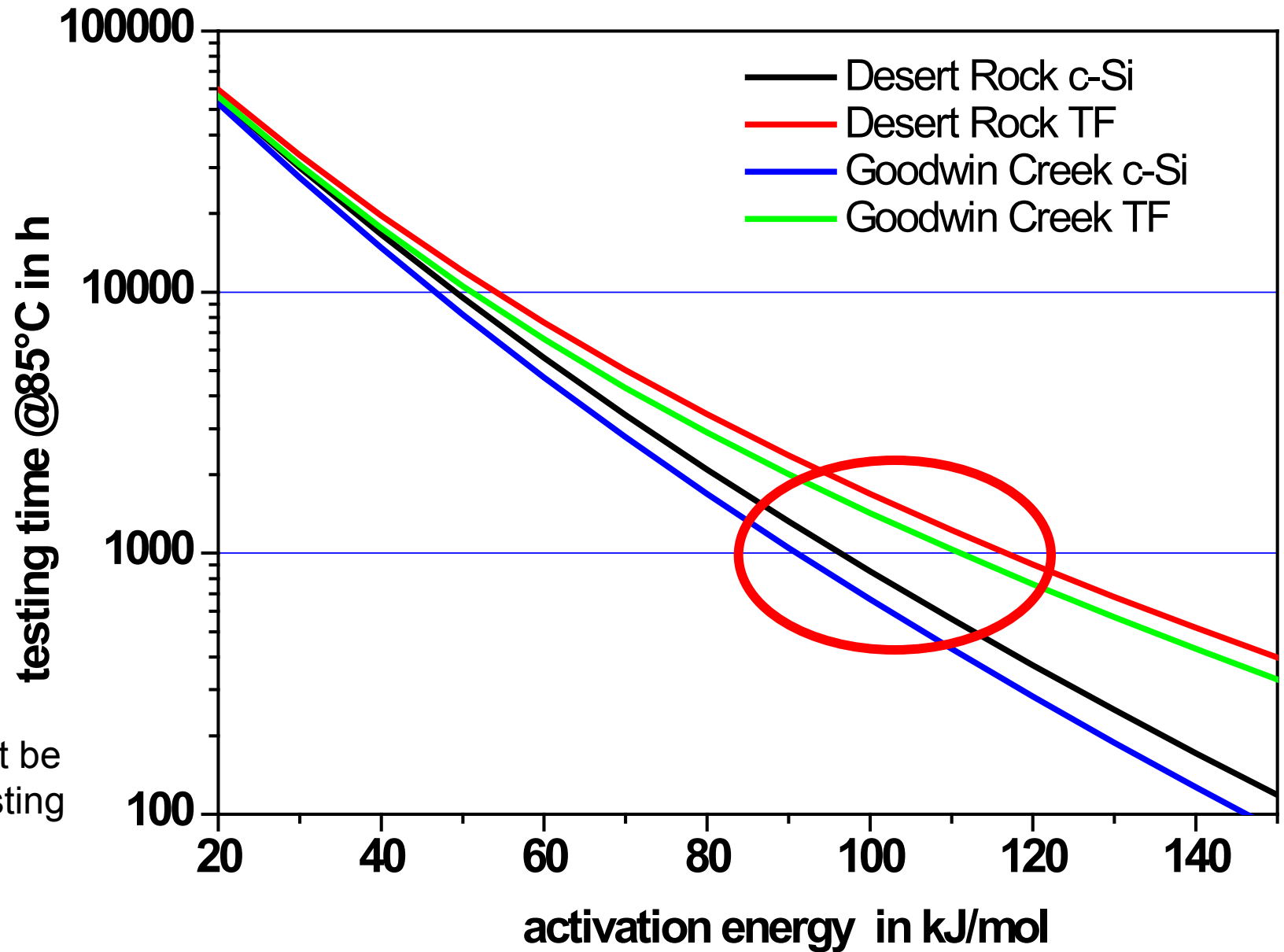
Type is more relevant here



$$\exp[-E_p / RT_{\text{eff}}] = 1/(t_{\text{max}} - t_{\text{min}}) \sum_{t_{\text{min}}}^{t_{\text{max}}} \exp[-E_p / RT(t)] \Delta t$$

Temperature testing

Equivalent testing time for 25 years temperature load @ 85°C



Temperature testing might be included in damp-heat testing without distinguishing the degradation processes

UV-radiation

Problems:

1. Measurement of UV-radiation
2. Reciprocity (Dose is $I \cdot t$, or $t = \text{Dose}/I$)
3. Spectral sensitivity of the samples is not known
4. Differences of the UV-sources of the test facilities *
5. Temperature impact

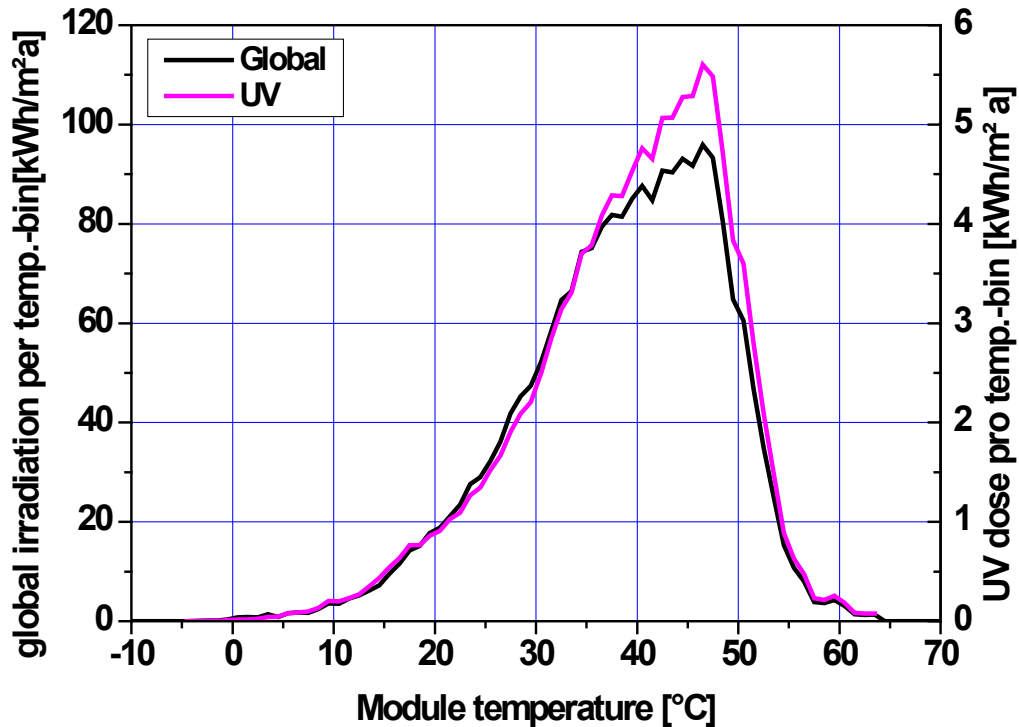
**IEC TC82 WG2 – Round Robin for measurements of UV testing devices*

Outdoor testing

Radiation monitoring

Accumulated dose of UV- and solar radiation for one year in the desert:

120 kWh/m² (about 8 x IEC)

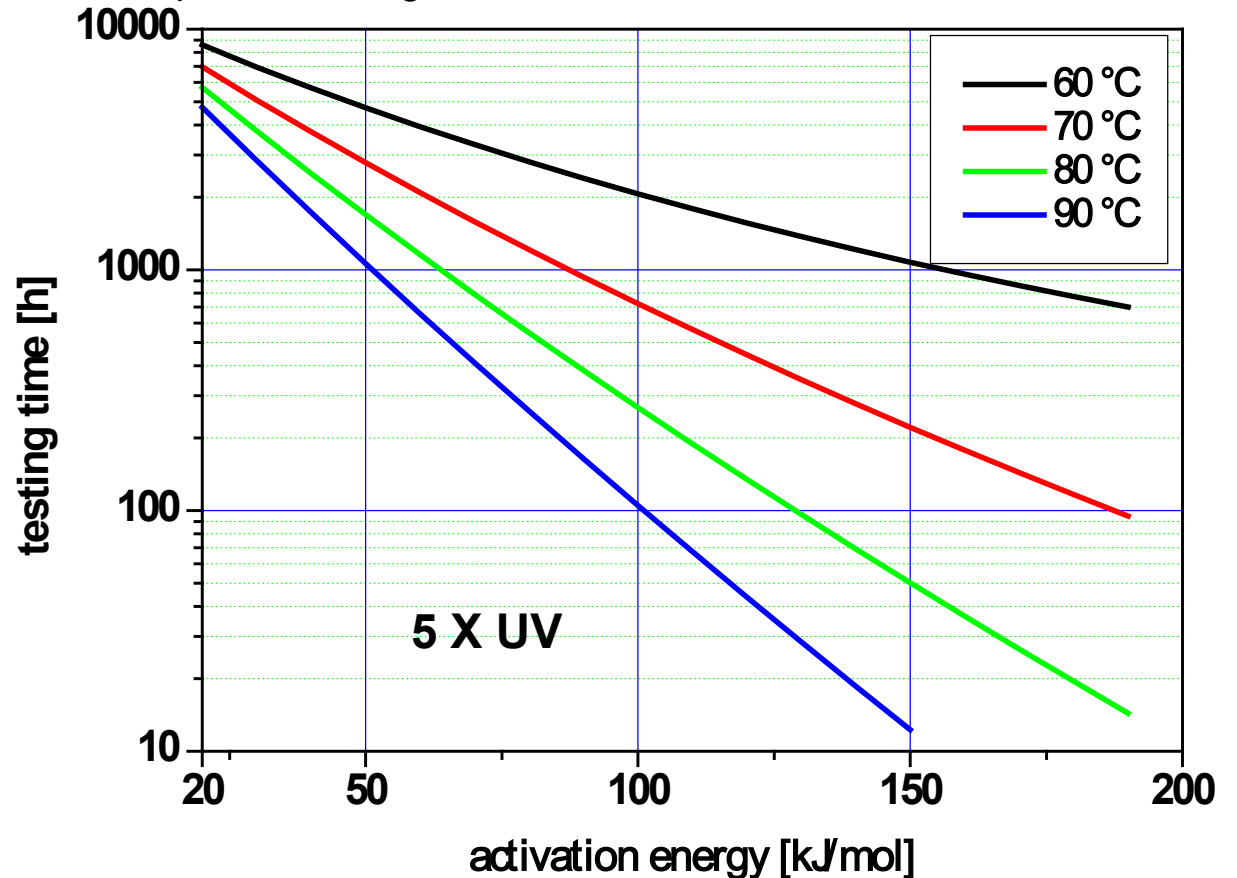


UV = 5.X % of solar radiation

Reciprocity: $p = 1$

$$t_{\text{test}} = (I_i / I_{\text{test}})^p \Delta t_i \cdot \exp [-(E_a / R) \cdot (1/T_{\text{test}} - 1/T_i)]$$

equivalent testing times for five suns UV test for desert climate loads



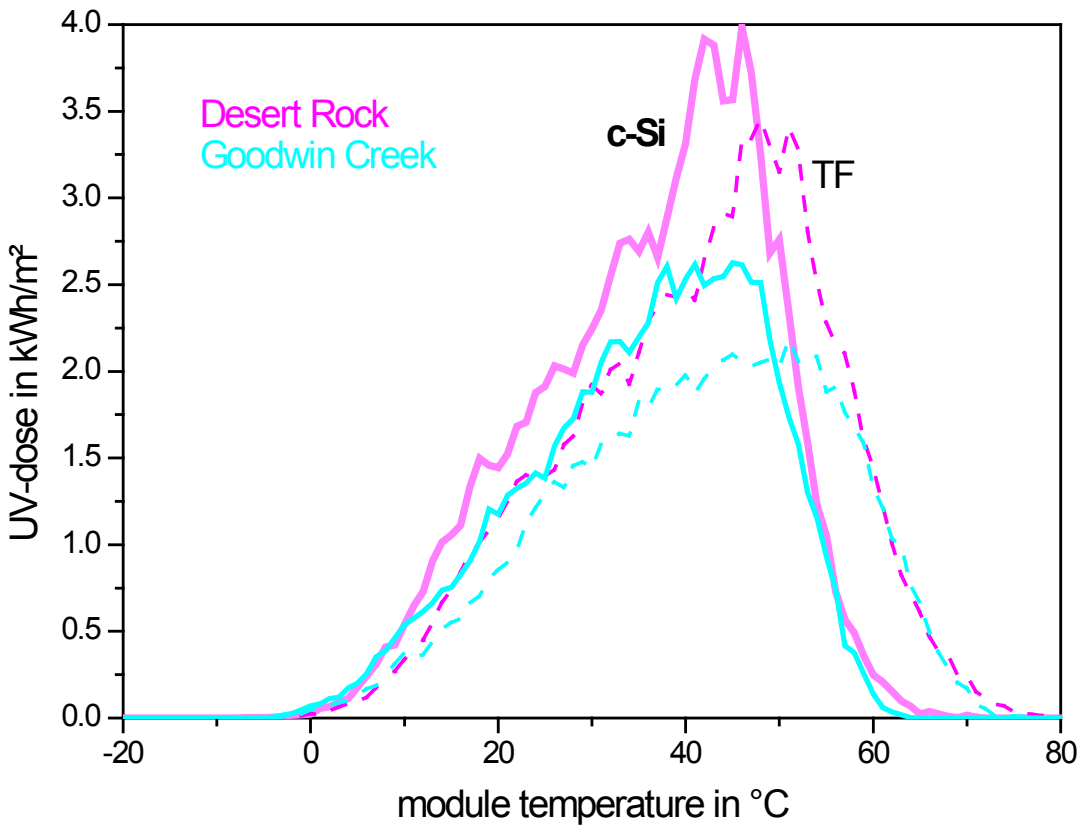
UV - radiation modelling

Desert Rock: 106 kWh/a m²

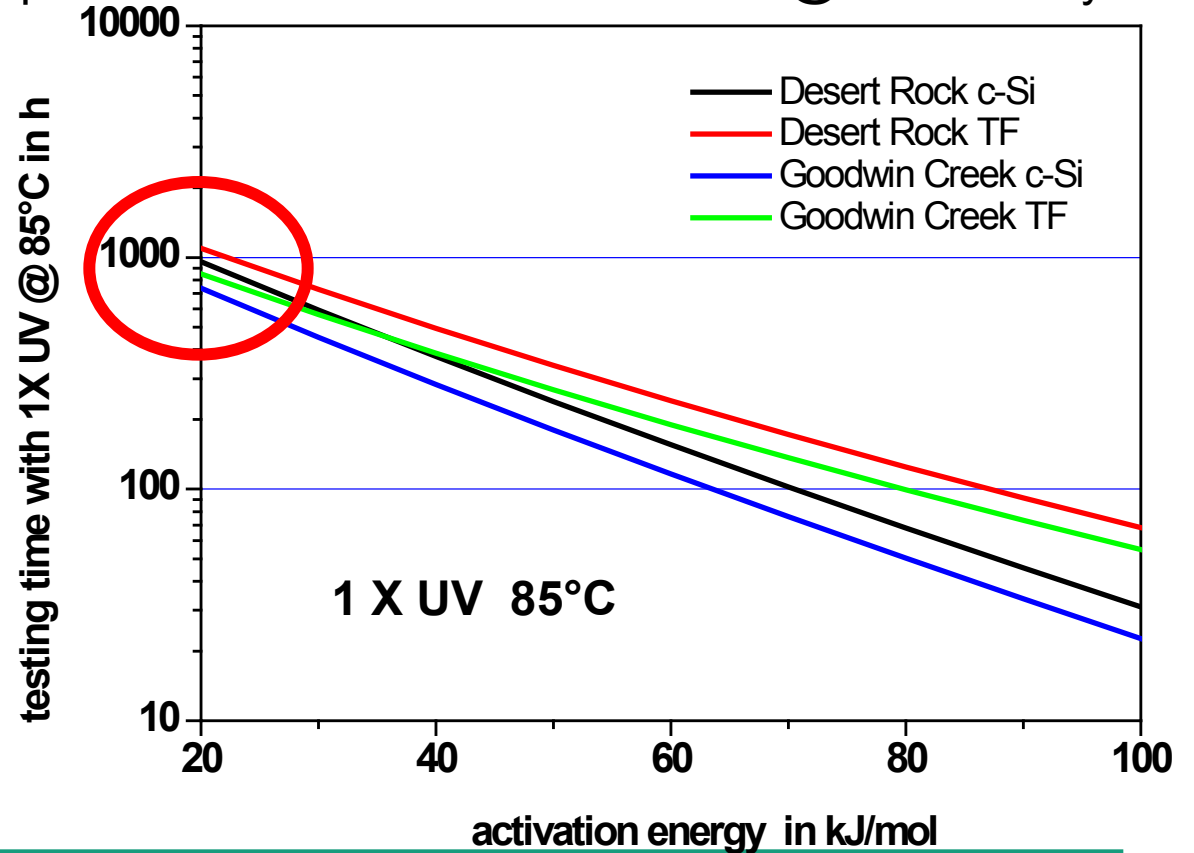
4-5 suns

Goodwin Creek: 83 kWh/a m²

Elevated temperature



Equivalent constant load for 1 sun UV @ 85°C for 1 year



Humidity

Problems:

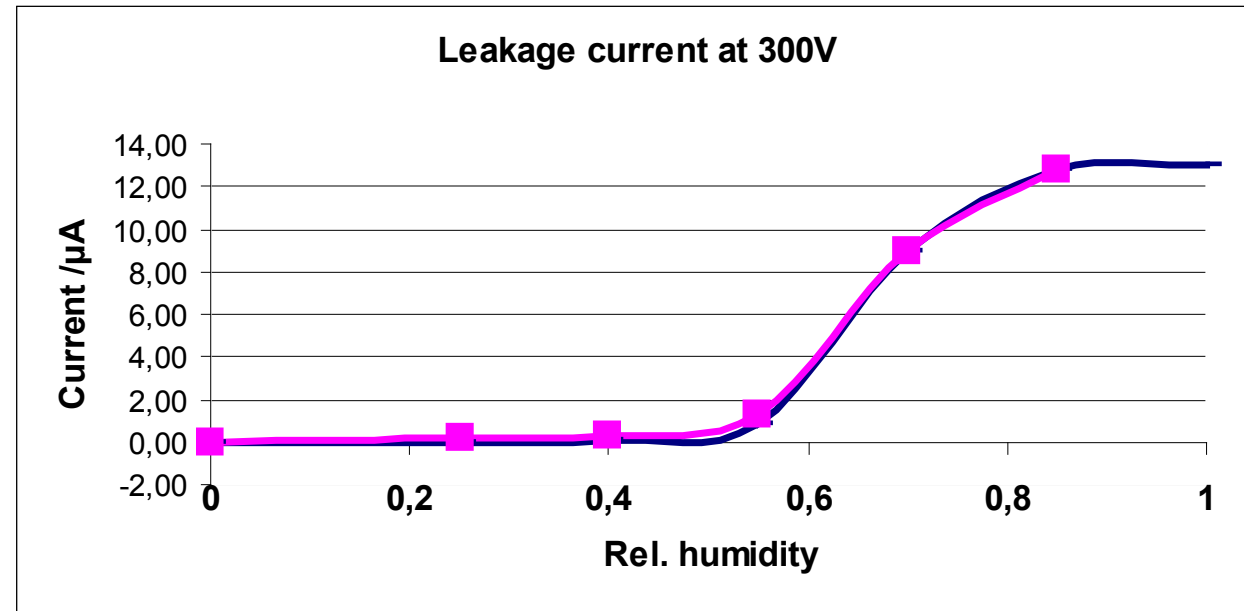
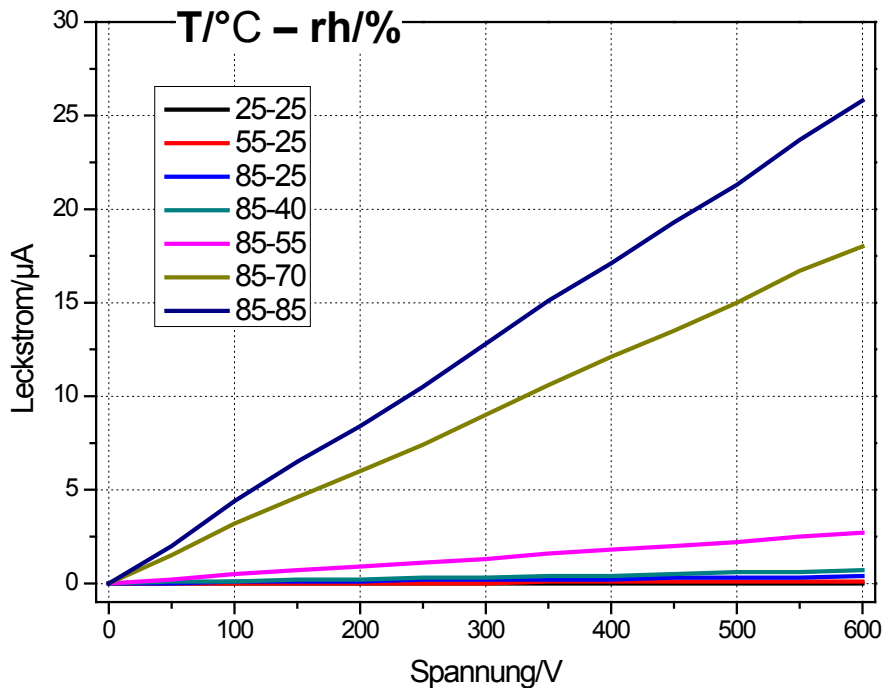
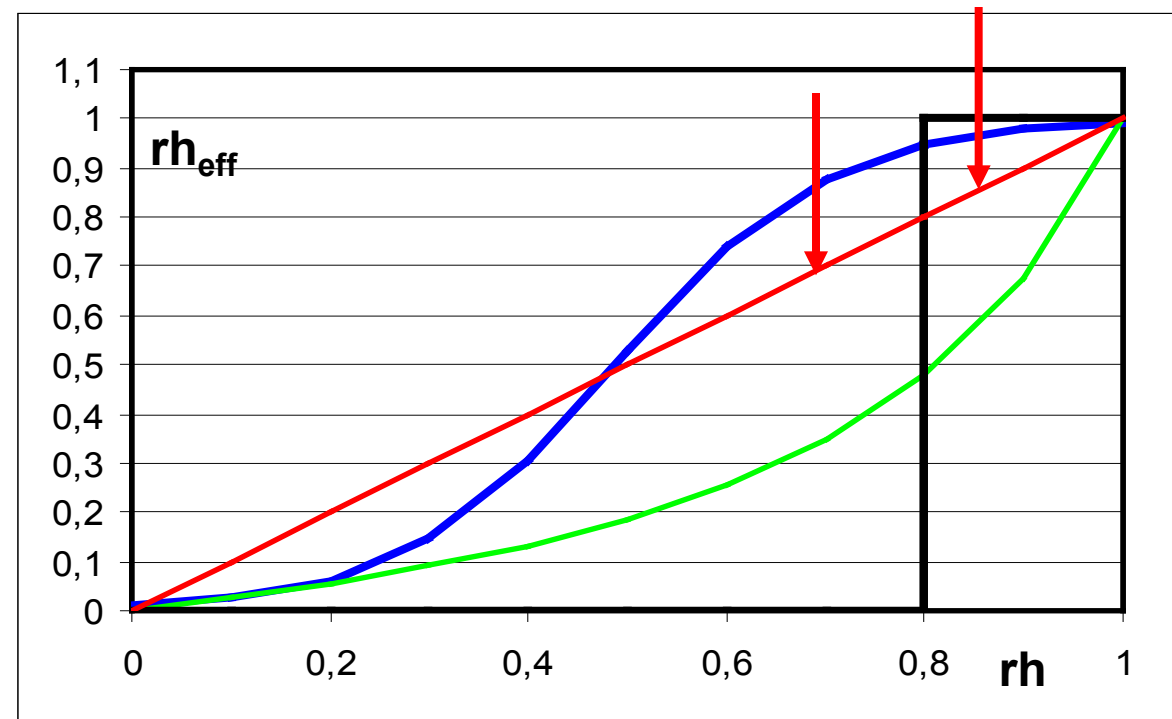
1. Assessing micro – climate
 2. Transient behaviour (changing partial pressure gradients)
 3. Slow diffusion in encapsulants or edge sealants (hard to accelerate)
- => non-uniform polymer degradation above cells after 4000h damp-heat*

*C. Peike et.al.: Non-destructive degradation analysis of encapsulants in PV modules by Raman Spectroscopy, *Sol. En. Mat. Sol. Cells* (2011)

Effective humidity

Modelling humidity impact onto modules based on surface humidity

- Climatic cabinet
- Leakage current



Sigmoidal Model: $I_{leak} = G / (G + \exp(-rh * k)) * (G/f(0) - 1)$

Simulated histograms of the relative humidity

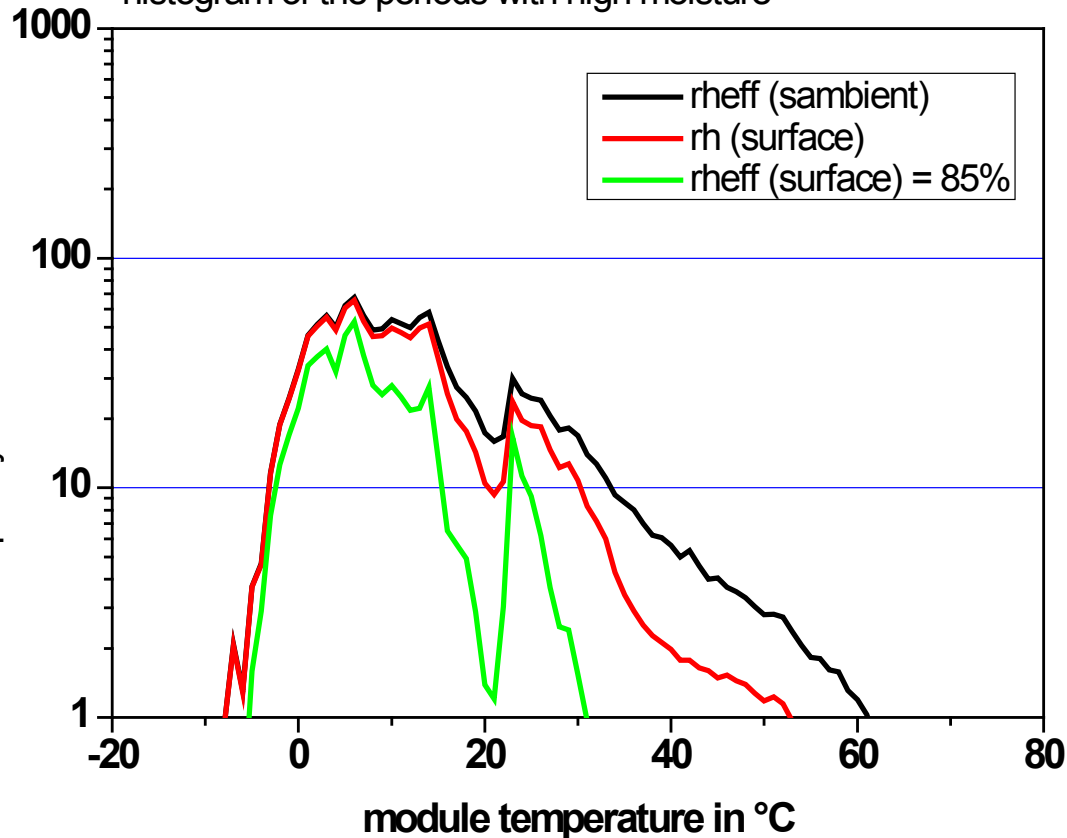
Ambient humidity = partial pressure / saturation pressure (T_{amb})

Surface humidity = partial pressure / saturation pressure (T_{modul})

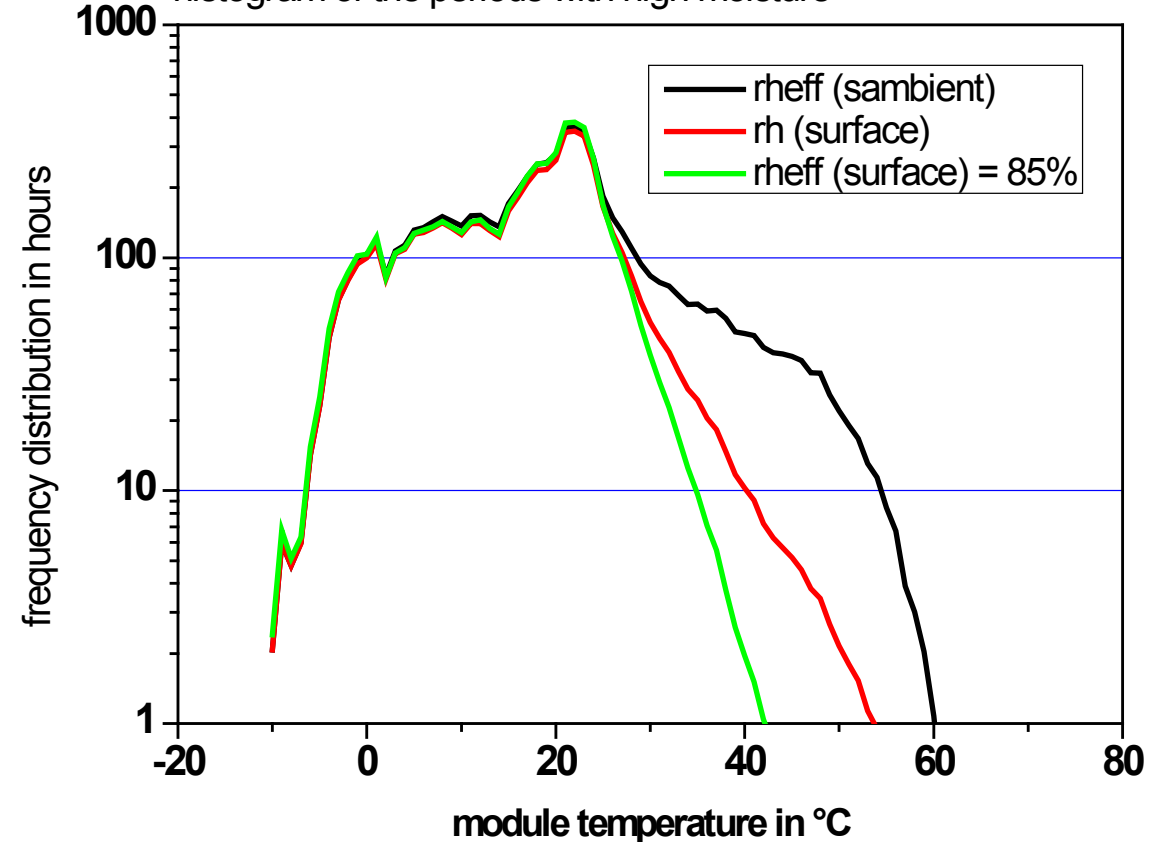
Eff. Humidity: $rh_{eff} = 1/(1+ \exp(-rh*k) *(1/f(0)-1))$

Humidity dose: $\Delta t_{eff} = \Delta t * rh_{eff} / 0.85$

Desert Rock 2007-01-01-bis-2007-12-31_ (type TF)
histogram of the periods with high moisture



Goodwin Creek 2007-01-01-bis-2007-12-31_ (type cSi)
histogram of the periods with high moisture

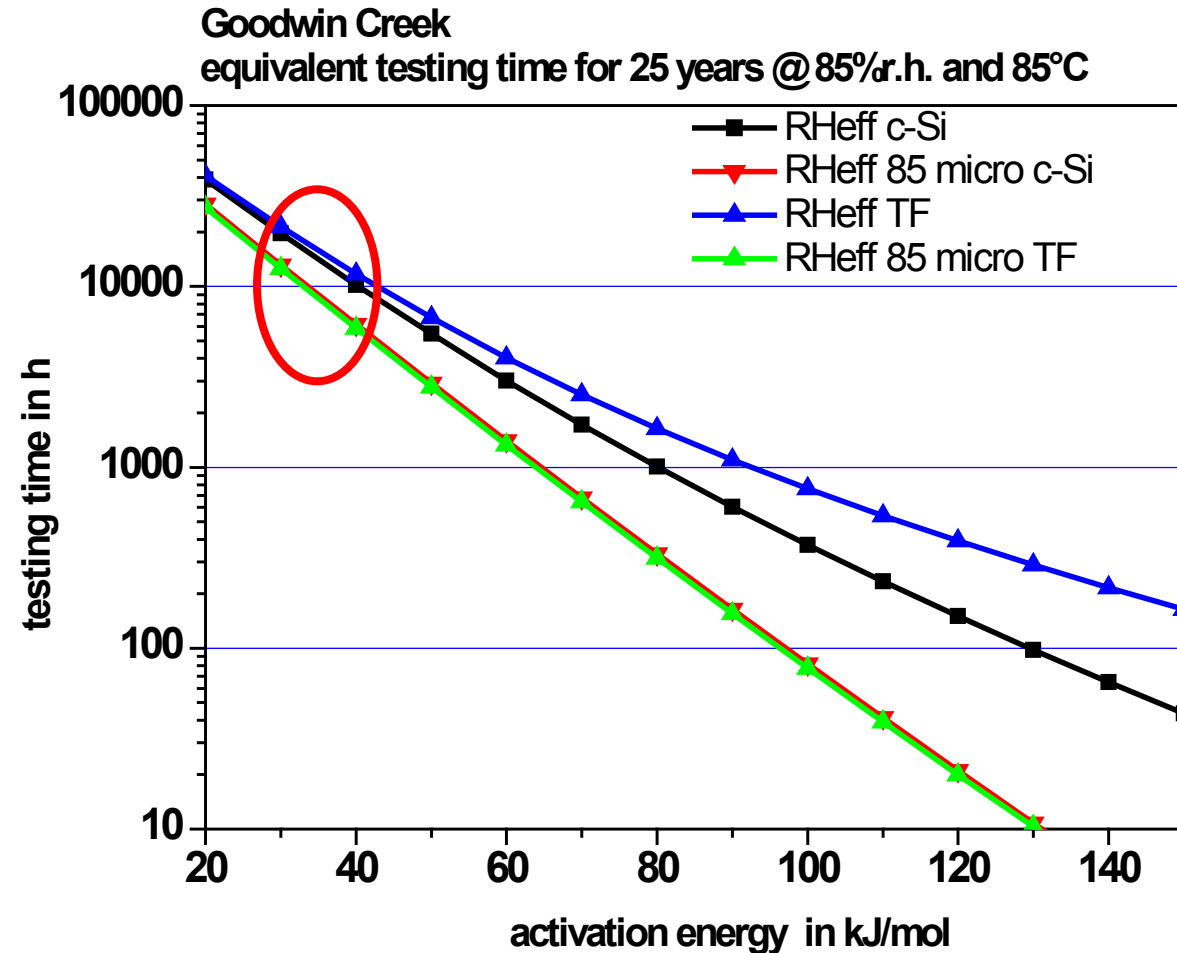
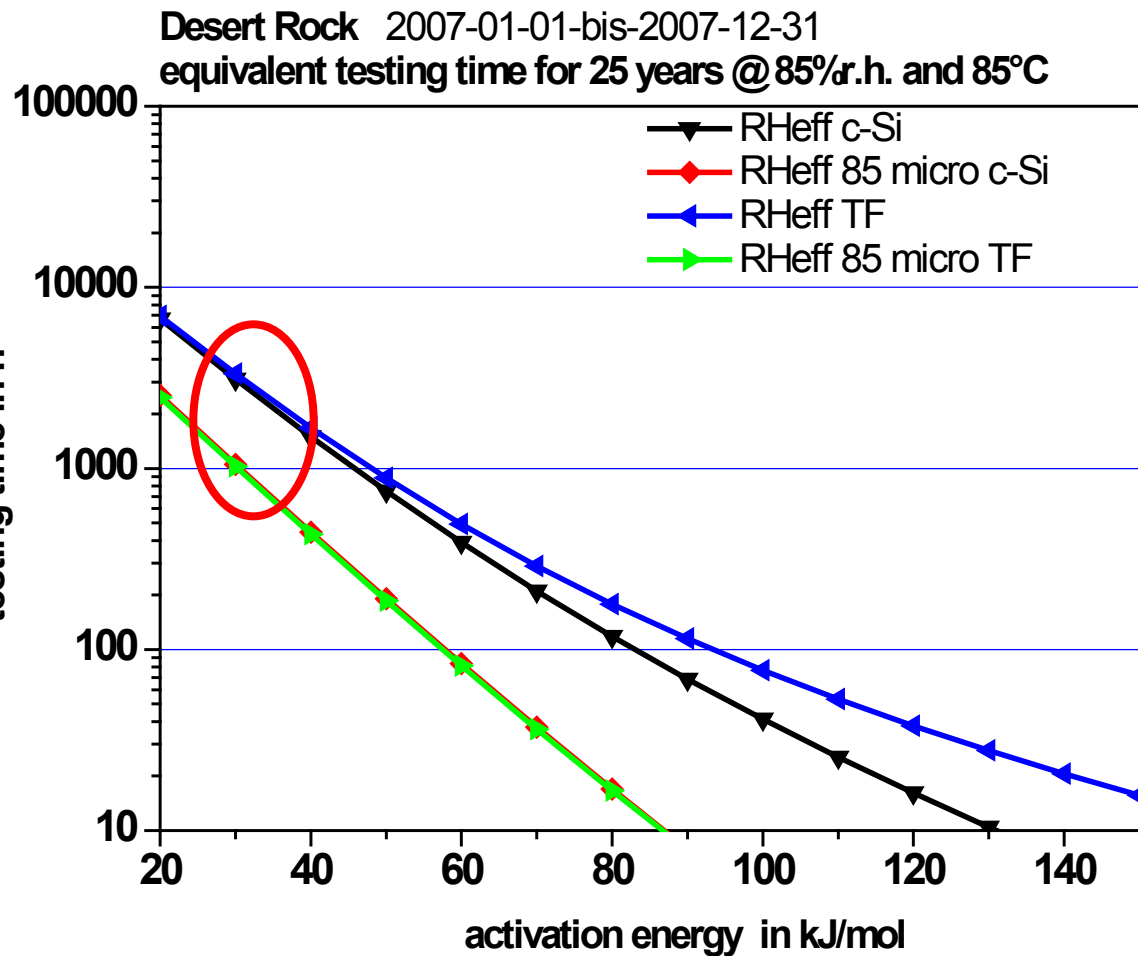


Damp-heat test conditions at 85°C and 85% rh

Considering the surface humidity instead of the ambient humidity reduces the testing time by a factor of 2 for humid and 3 for desert climates

Ten times longer testing time needed for the more humid site

The 1000h test suits for desert rock (could be 500 h)



Testing times needed for service life testing (25 years)

Unfortunately strongly depending on the degradation processes in the materials

Test designs are needed which allow assessment of the material-dependent parameters in the time transformation functions

Service life testing times /h	E = 50 kJ/mol				E = 100 kJ/mol			
	Goodwin Creek		Desert Rock		Goodwin Creek		Desert Rock	
	c-Si	TF	c-Si	TF	c-Si	TF	c-Si	TF
Temperature (85°C)	8200	10500	9500	12000	666	1425	853	1680
Humidity (85/85)	2916	2780	191	185	82	77	4	4
UV (1sun @ 85°C)	4500	6700	6000	8500	575	1375	775	1700
UV (1sun no T-activation)	38000		48000					

Modelling the micro-climatic stress conditions

Time-series of climatic data

ambient temperature and humidity, solar irradiation, wind speed

Modeling the module temperatures

ambient temperature, solar irradiation, wind speed, module-specific coefficients
(mounting situation might be considered)

Modeling the UV-radiation

5.5% of the solar radiation, module temperature

Modeling the effective surface humidity

ambient temperature and humidity, module temperature

Conclusion

Modelling the ALT conditions

Use a simple time-transformation function (Arrhenius based, eg)

Time, module temperature and other degradation factors, but separately first

Modeling the module temperature stress

as function of the material-specific activation energy,

(could be eventually included in damp-heat testing)

Modeling the UV-radiation impact

as function of the material-specific activation energy (which is low, UV-dose more important)

Modeling the moisture test

Higher test temperatures needed, as function of the material-specific activation energy,

What else is needed?

Validation of the time-transformation function

Or introduction of alternatives

Try to determine material dependencies like
activation energies for finding dose-response functions

Consider the other degradation factors,
Temperature cycling, frost-thaw, high pot, salt, ammonia.....

Define or adopt climate-classes and the respective stresses

Mapping, standardised ALT for each class or individual qualification

Or assess dose response-function and model for given location

Define service-lifetime requirements

Design life-time, performance limit

Materials

Micro-climate

Local climate

ALT conditions

Service life

Thanks

for your attention

NREL for the invitation



To my colleagues

Daniel Philipp

Franz Brucker

Philipp Huelsmann

Markus Heck

Stefan Brachmann

Karl-Anders Weiss

Stefan Wiesmeier

To our partners

TÜV Rheinland

Schott Solar

Solarfabrik

Solarwatt

Solarworld

Solon



Workshop on Reliability of PV-Modules

Testing

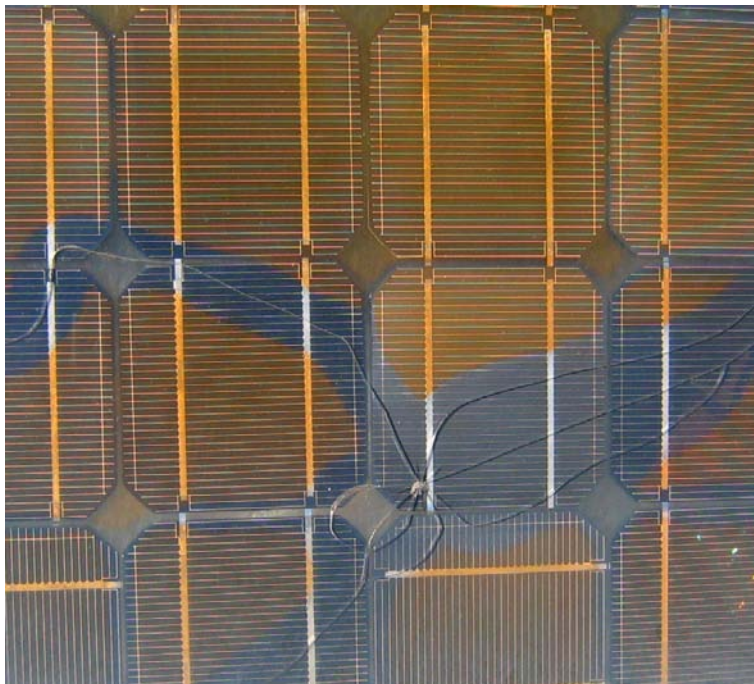
Analysing

Simulating module - reliability

Organised by Fraunhofer ISE and Humboldt-Univ. Berlin

Supported by JRC, PCCL, TÜV Rheinland, VDE - Institute

<http://www-pbp.physik.hu-berlin.de/pvr/>



Berlin - Adlershof

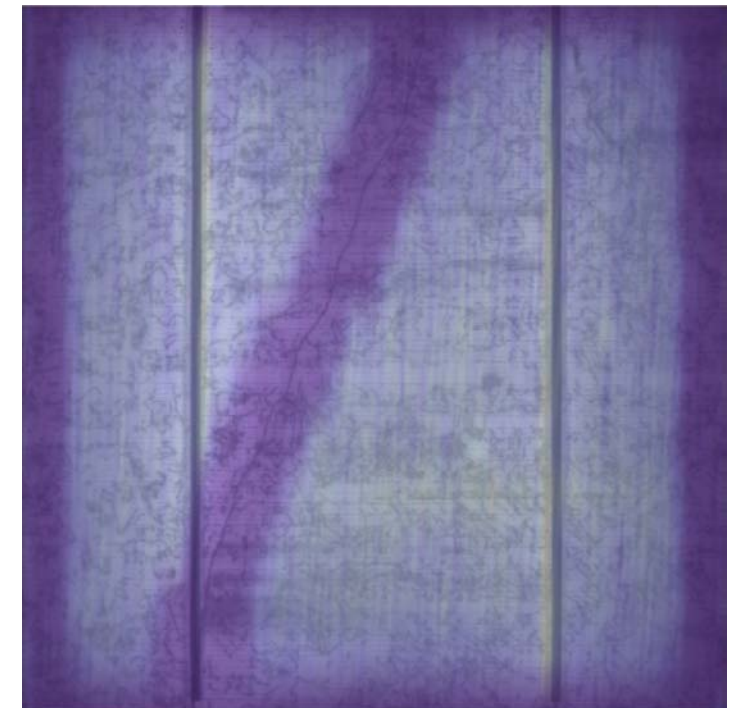
Germany

April 5 – 6 2011

Meeting of the IEC TC82 WG2

Sub-group on Back-Sheets

After the Workshop

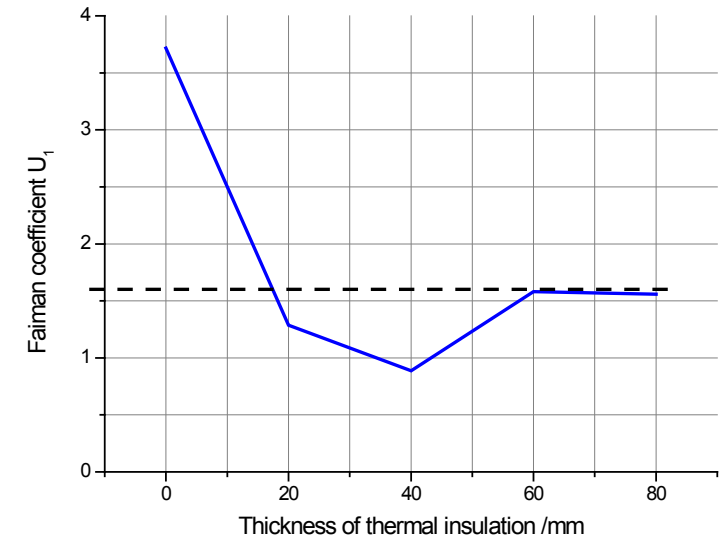
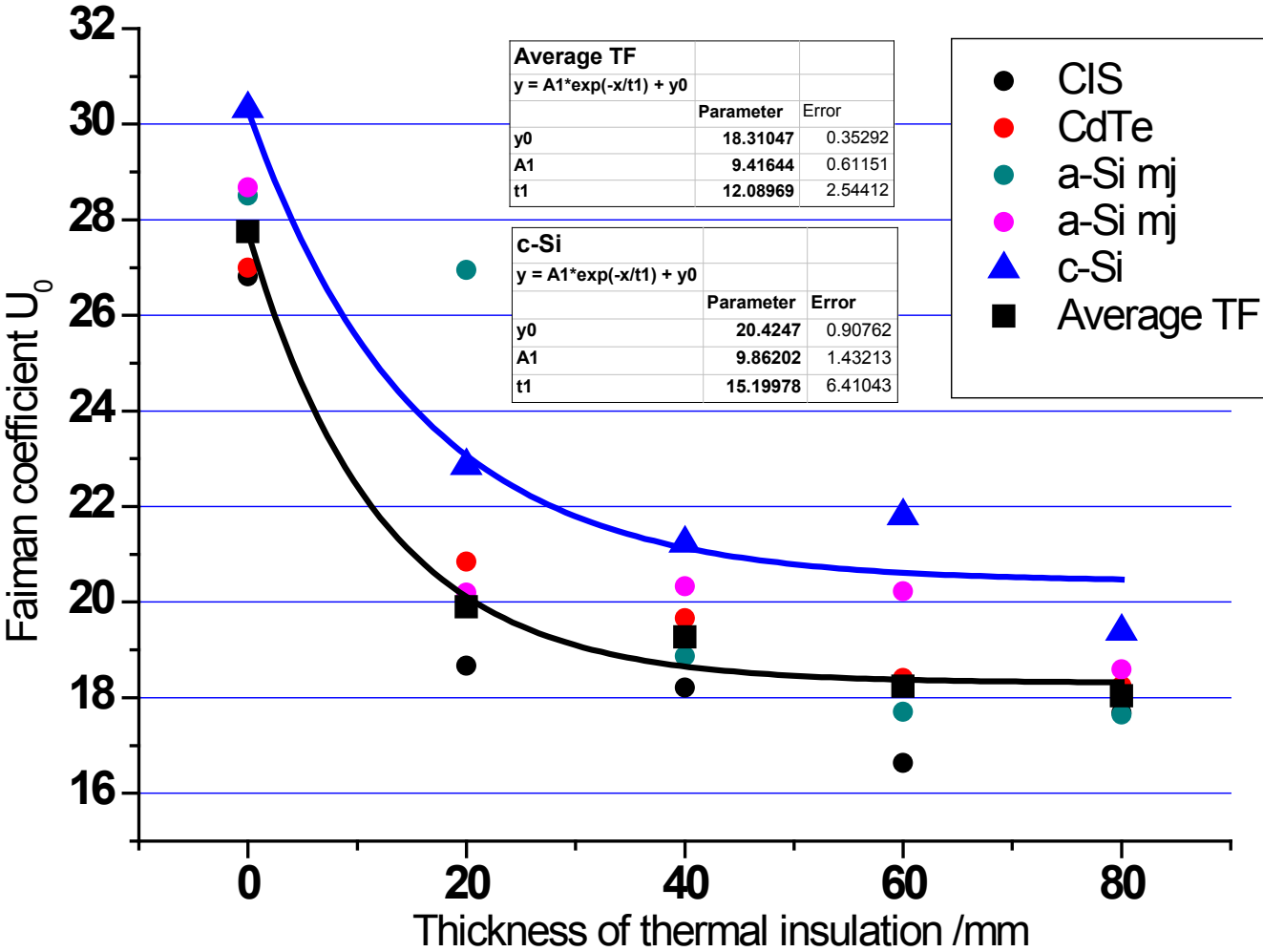


Temperature simulation towards BIPV

Increasing thermal insulation on the back-side

Short monitoring periods

Inclination 45°



Wind impact reduction by 50%

	Free		BIPV		45°	Incl.
	U0	U1	U0	U1		
c-Si	30	6	20	3		
TF	27,7	4	18,3	2		
c-Si	42,2		54,8		NOCT	800W
TF	43,7		59,4		Wind: 1 m/s	20°C
c-Si	40,2		51,3		STC	1000W
TF	44,3		58,0		Wind: 6 m/s	25°C
c-Si	68,3		85,0		Maximum	1000W
TF	71,1		89,6		Wind: 0 m/s	35°C

Module temperature up to 18 K higher