
***Bridging the Gap between
Fundamental Physics and Chemistry
and Applied Models
for HCCI Engines***



Dennis N. Assanis



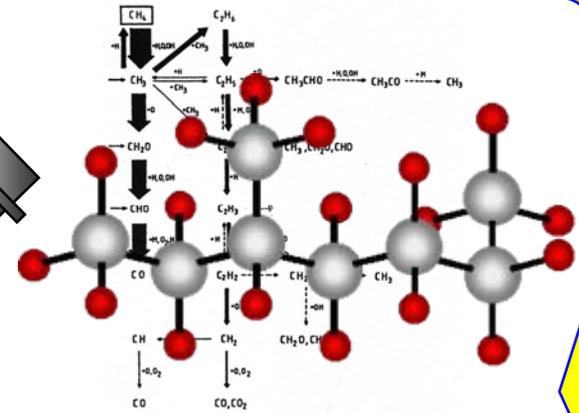
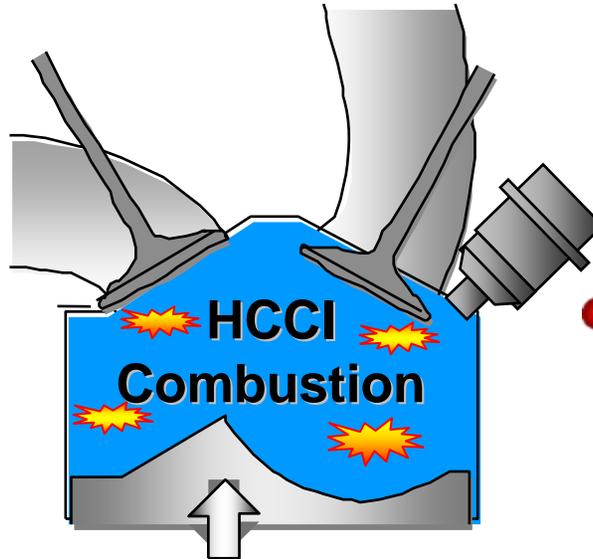
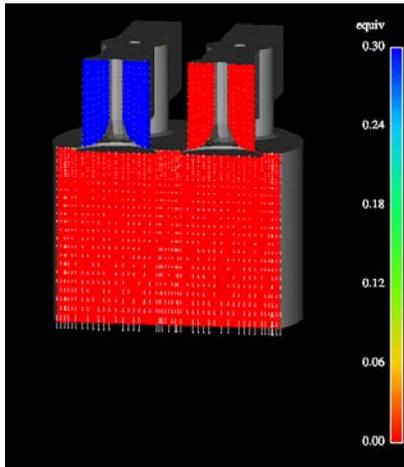
DEER Conference
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Chicago, IL

HCCI Engine Grand Challenges

Physics Models

Experiments

Chemical Kinetics



Enabling Technologies

Sensors, Actuators, Control

Bridging the Gap Between HCCI Fundamentals and Applied Models



A University Consortium on Homogeneous Charge Compression Ignition Engine Research - Gasoline

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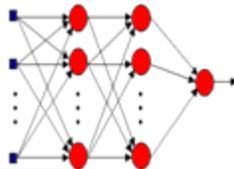
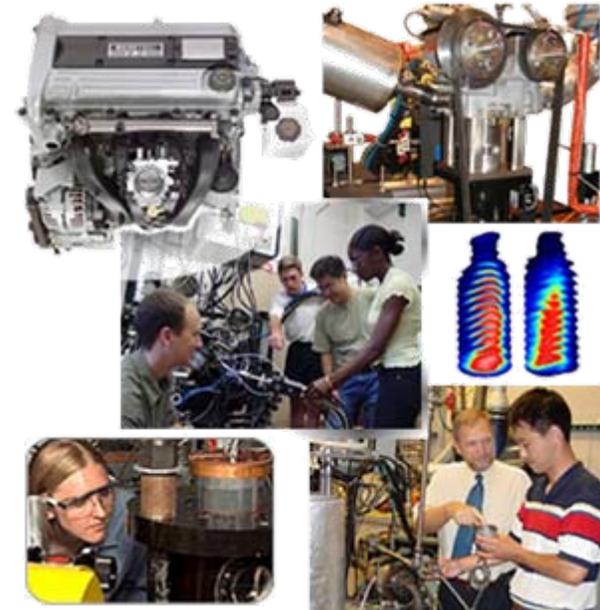
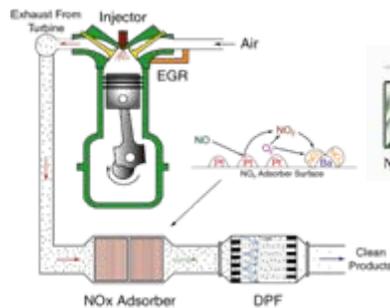
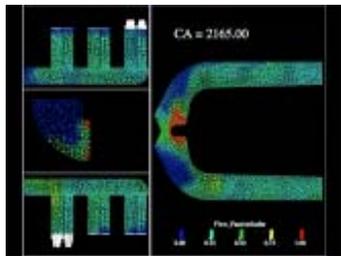
HCCI University Consortium

Acknowledgements



Collaborative
Research
Laboratories

Engine Systems Research

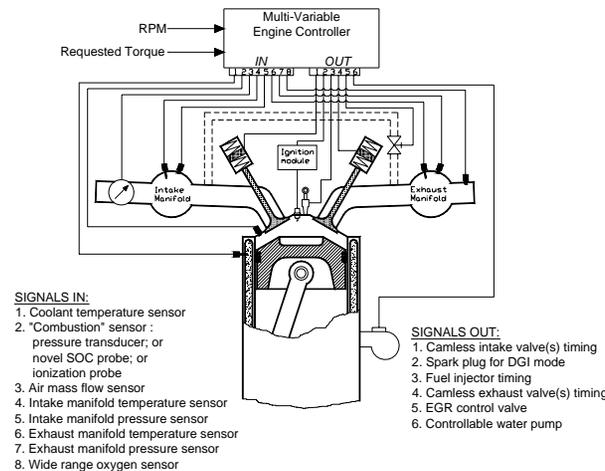


Bridging the Gap Between HCCI Fundamentals and Applied Models

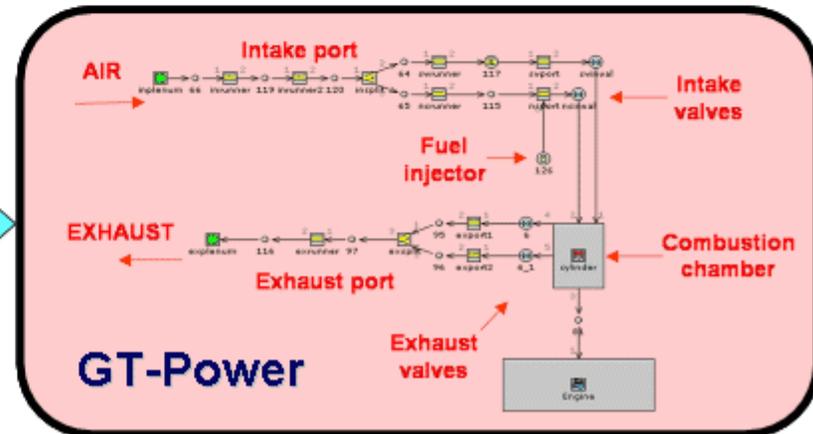
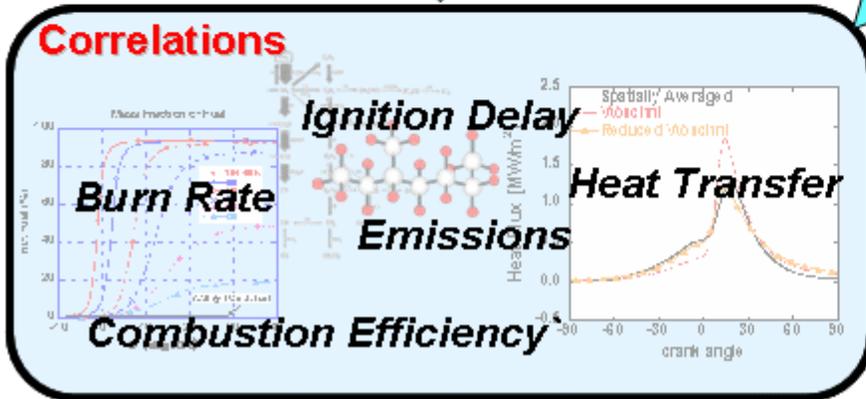
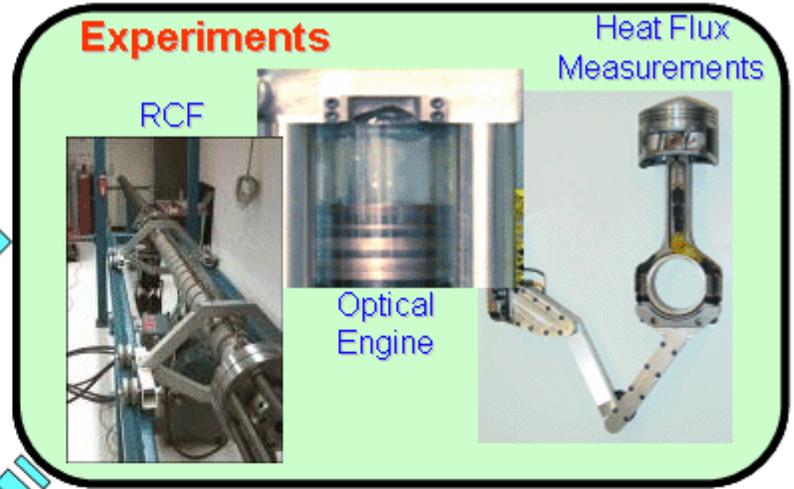
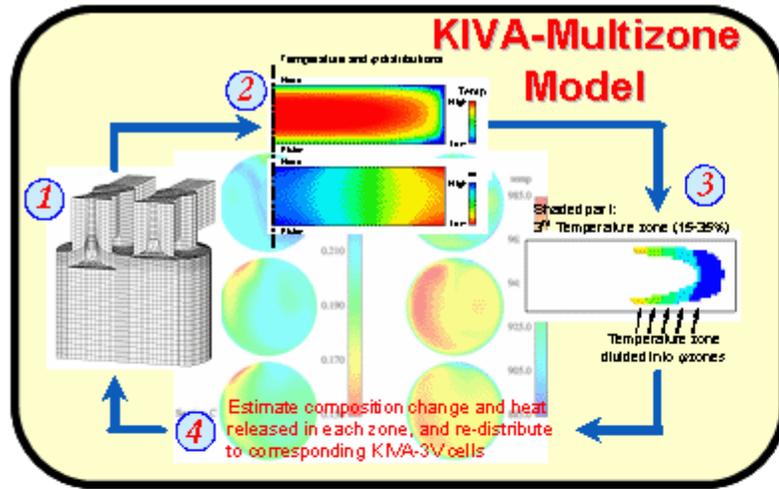


Objectives

- Bridge the gap between fundamental HCCI physics and chemistry considerations and applied models
 - Balance model fidelity with computational expediency and ultimate goal in mind
- Demonstrate a cascade sequence where high fidelity models and experiments feed phenomenological models appropriate for systems analysis
- Apply system models to assess candidate control schemes



Approach



Engine University Consortium Set-Ups

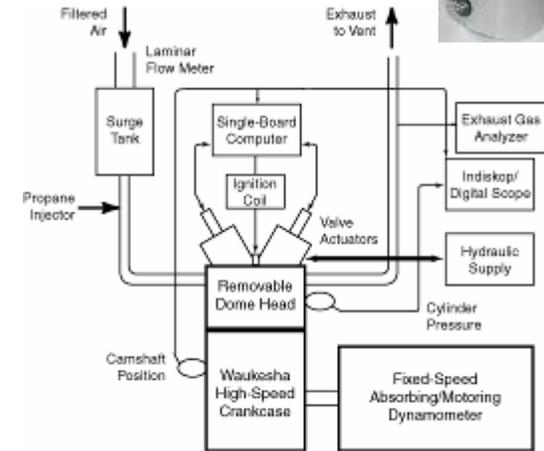
UM Optical Engines



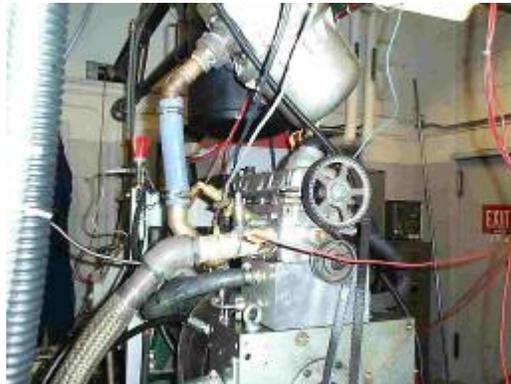
UM Heat Transfer Engine



Stanford Camless



MIT VW Engine with VVT

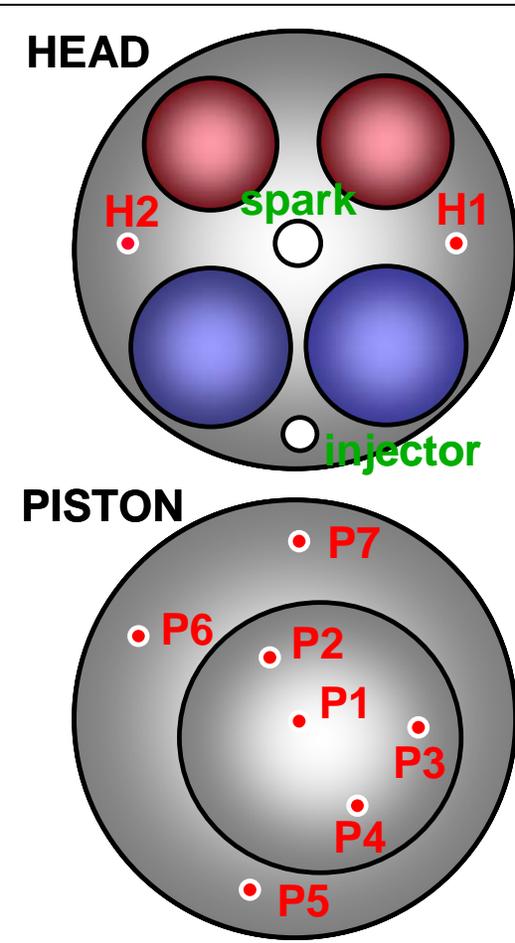


UCB VW TDI engine

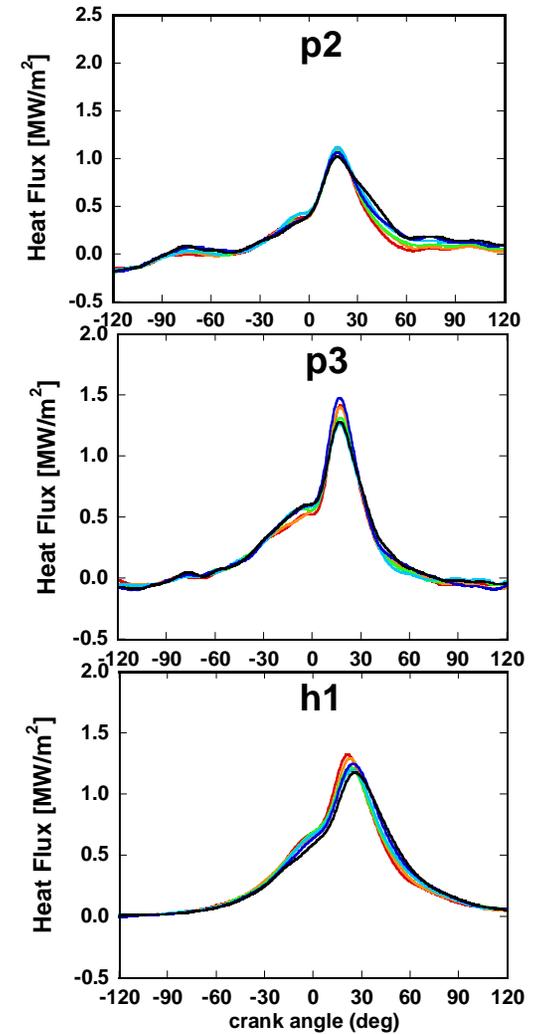


UCB CAT Single Cylinder



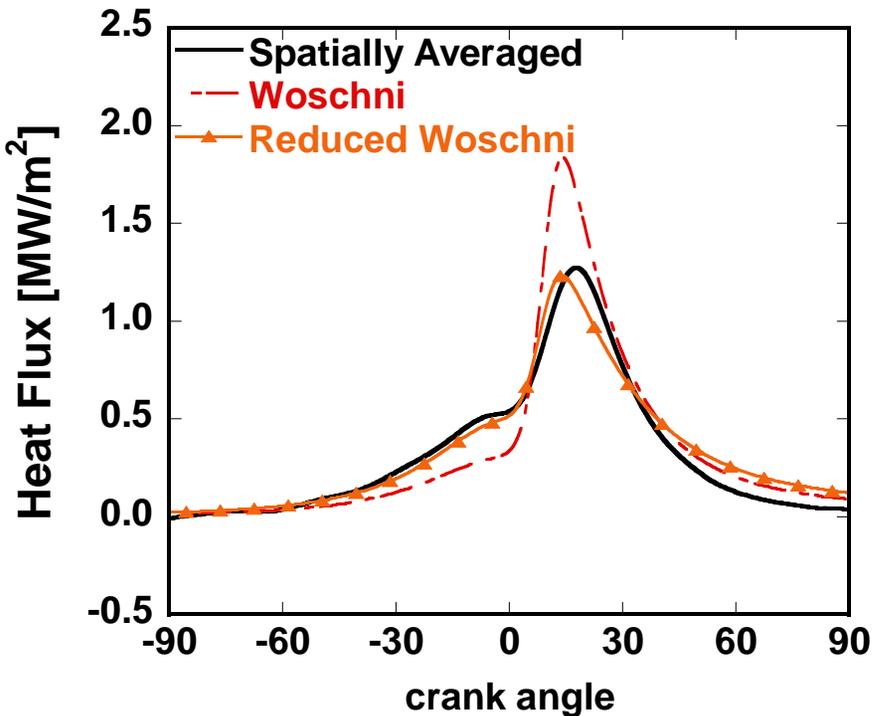


TELEMETRY



Concept of Modified Woschni Correlation

Models need to be calibrated to provide accurate total heat loss



- Classic Woschni underpredicts heat transfer during compression and leads to unrealistic ignition predictions
- Modified Woschni heat transfer model:

—Original: $A_2 = 1$

—Modified: $A_2 = 1/6$

$$h = \chi_{\text{Woschni}} 3.26 \cdot B^{-0.2} \cdot p^{0.8} \cdot T^{-0.53} \cdot w^{0.8}$$

$$w = A_1 C_1 \bar{S}_p + A_2 C_2 \frac{V_d T_r}{p_r V_r} (P - P_m)$$

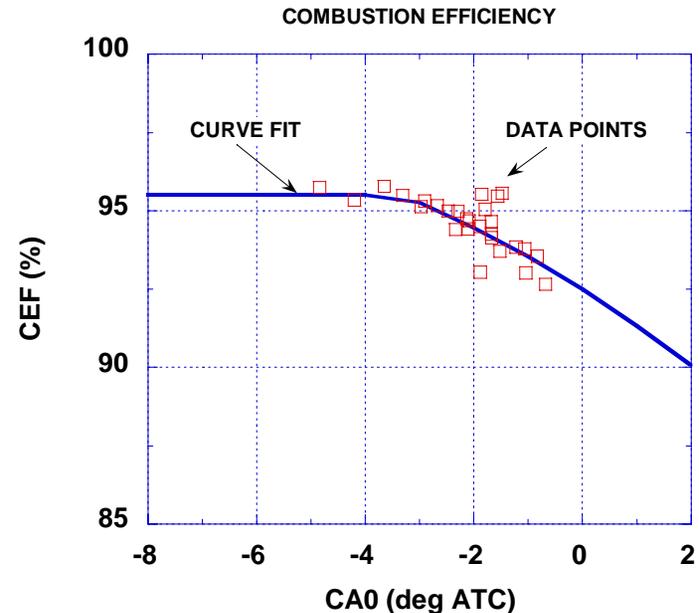
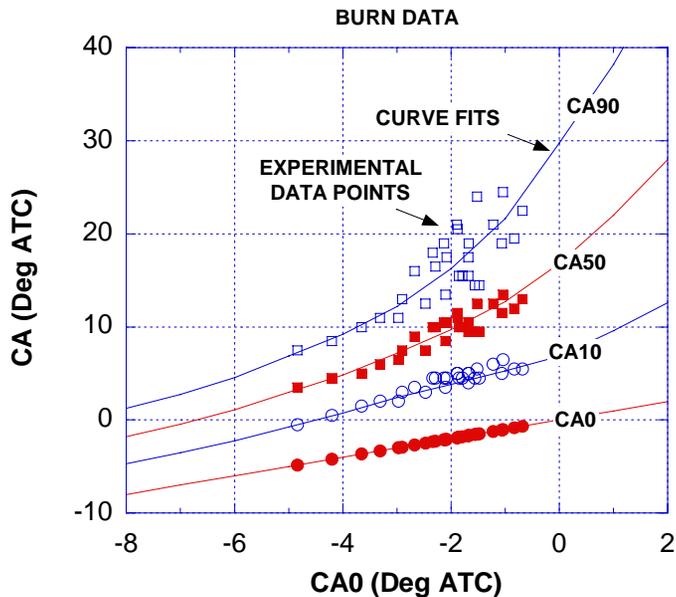
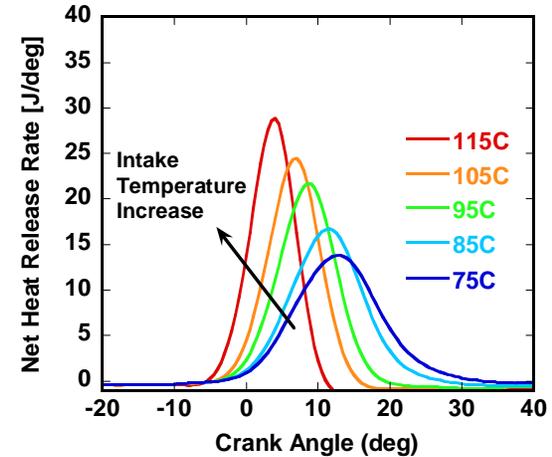
$$C_1 = 2.28 + 0.308 \frac{\pi B w_p}{\bar{S}_p}, \quad C_2 = 0.00324$$



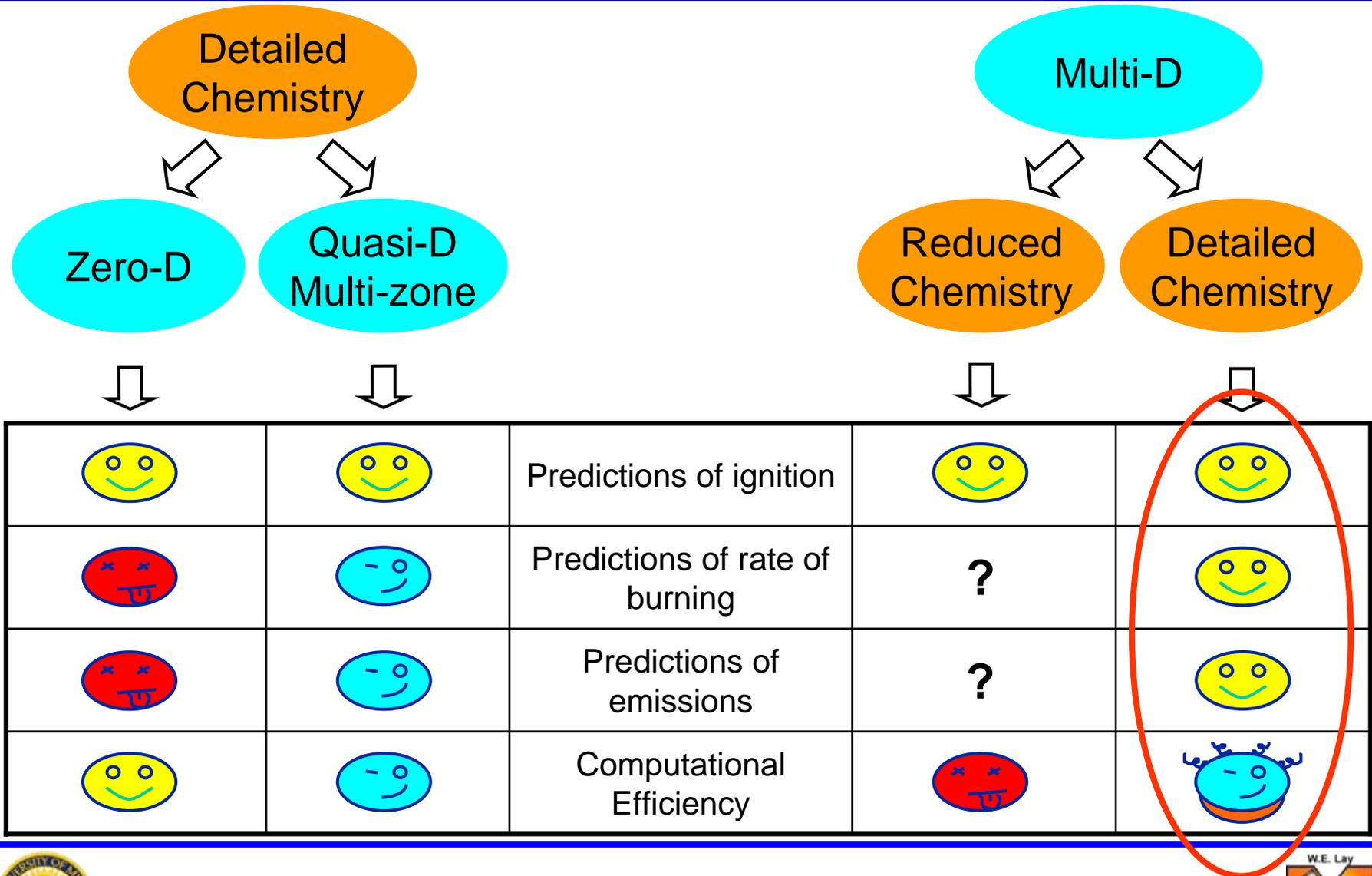
Experimental Burn Rate Data

- Varying RPM, load, T_{cool} , T_{inlet} , A/F ratio
- Generate correlations as function of ignition timing (one variable)

$$x_{NORM} = 1 - \exp[-((\theta - \theta_0) / \Delta\theta)^{w+1}]$$

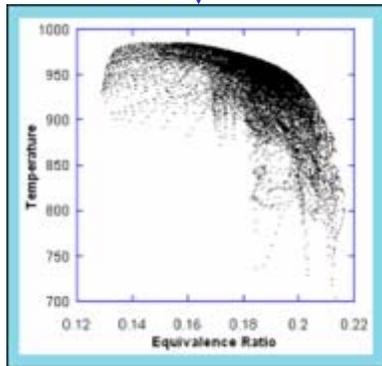
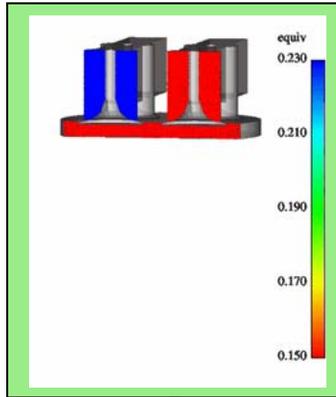


Modeling Approaches for HCCI Engines



Initial Modeling Approach: Sequential CFD + Multi-zone Model

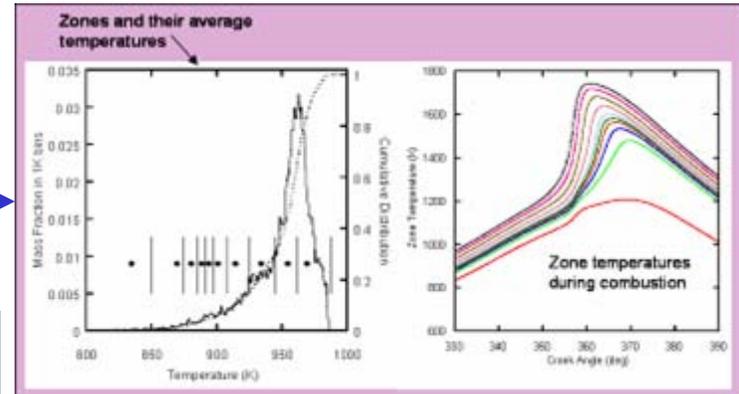
1 Open-cycle calculation using Kiva-3V



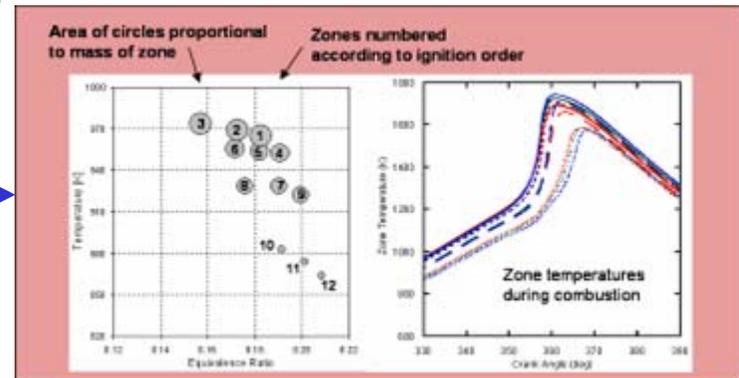
2 Temperature / Equivalence Ratio distribution obtained before TDC

3a

Calculation of combustion event using Multi-zone model with Temperature Zones only



TRANSITION POINT



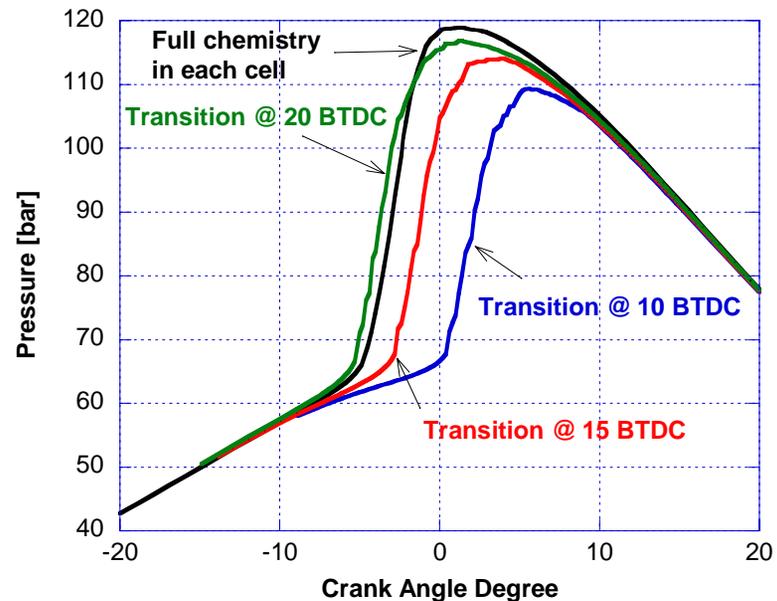
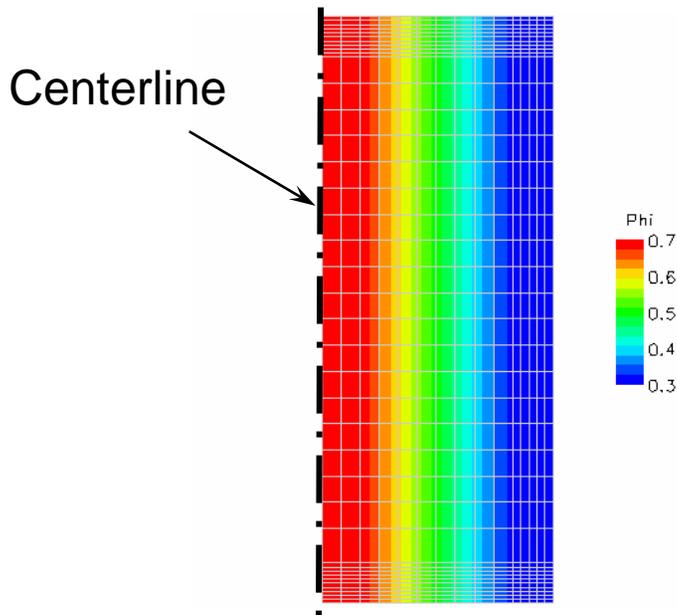
3b

Calculation of combustion event using Multi-zone model with T/ϕ Zones



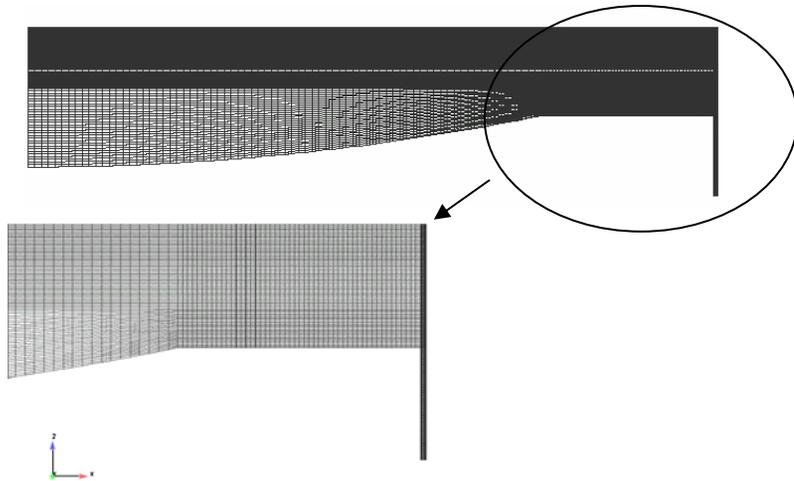
Sensitivity to Transition Timing

- Calculations at LLNL showed that the point of transition from KIVA to the multi-zone code can affect the results (SAE 2005-01-0115)
 - Imposed ϕ distribution on a 2D coarse grid (Fuel CH_4)
 - Solution obtained using sequential multi-zone approach compared against detailed solution (KIVA-3V linked with Chemkin)
 - Implication: Temperature and composition stratification is important

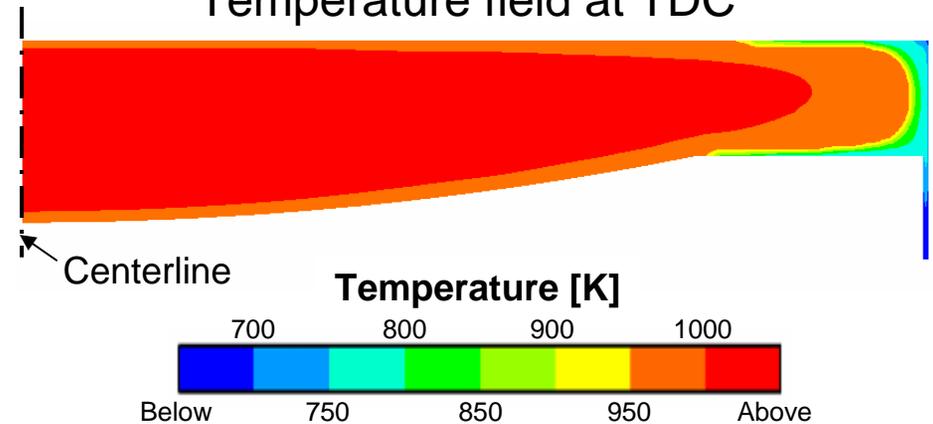


Naturally Occurring Thermal Stratification

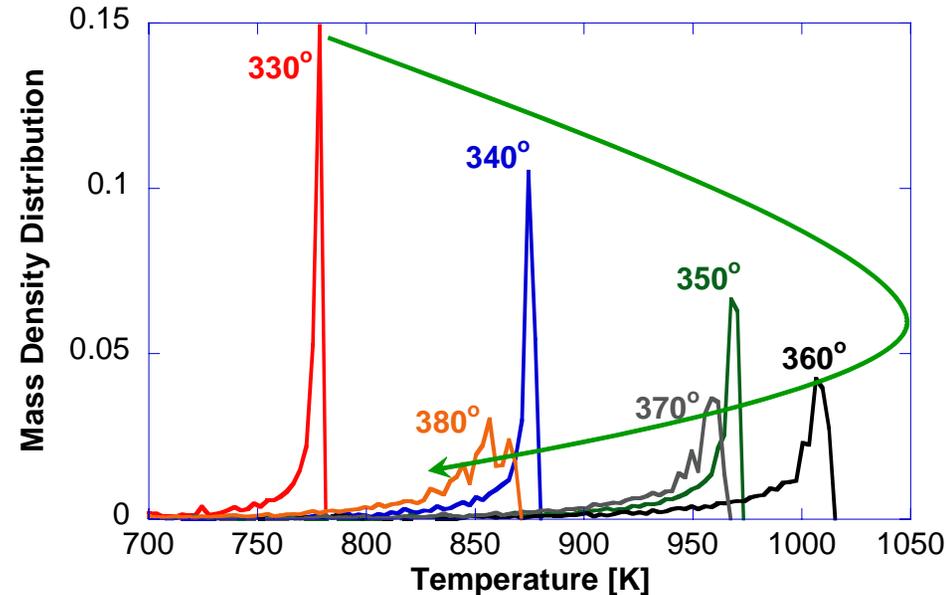
Collaboration with Sjöberg and Dec (Sandia) - SAE 2004-01-2994



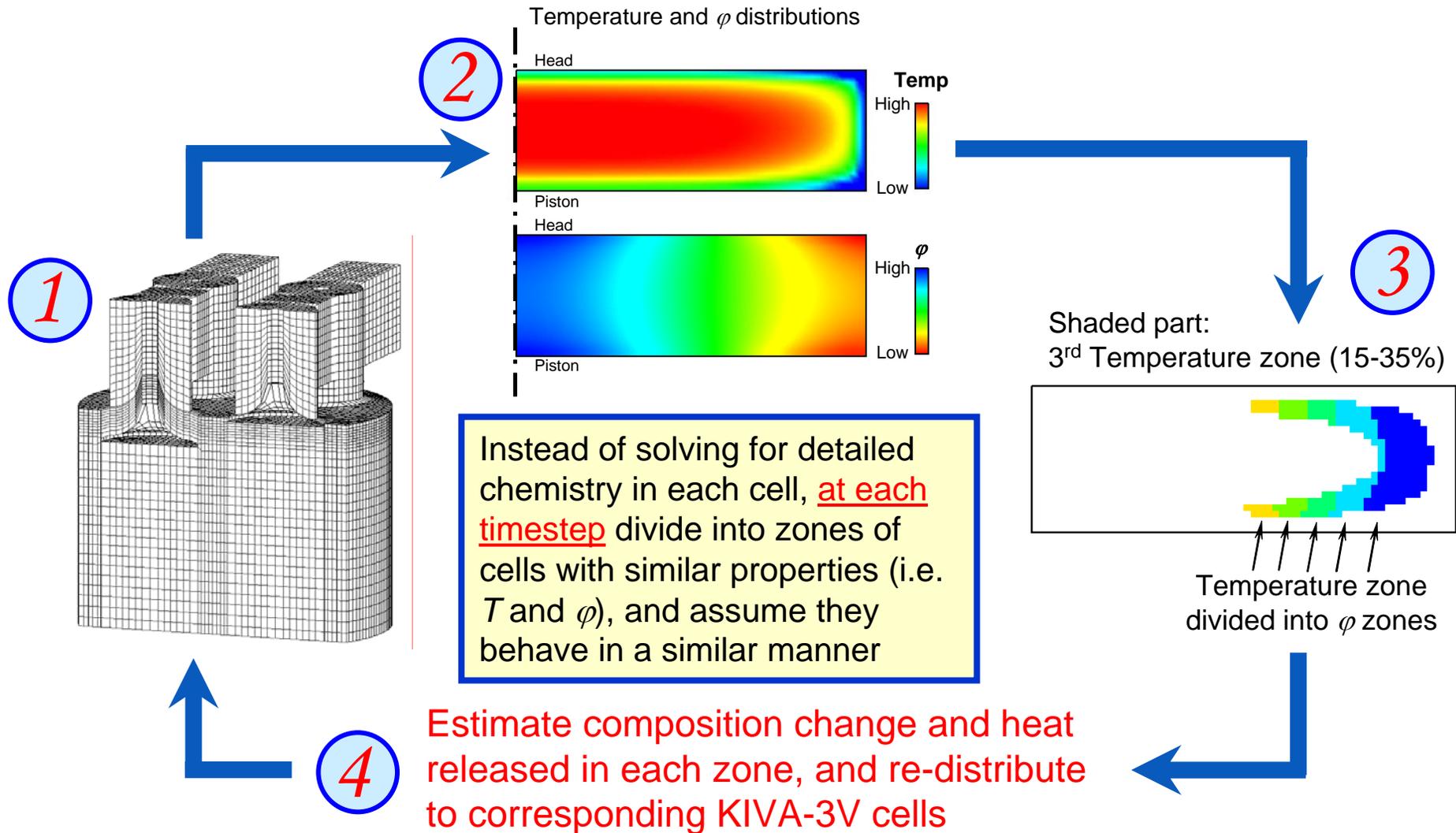
Temperature field at TDC



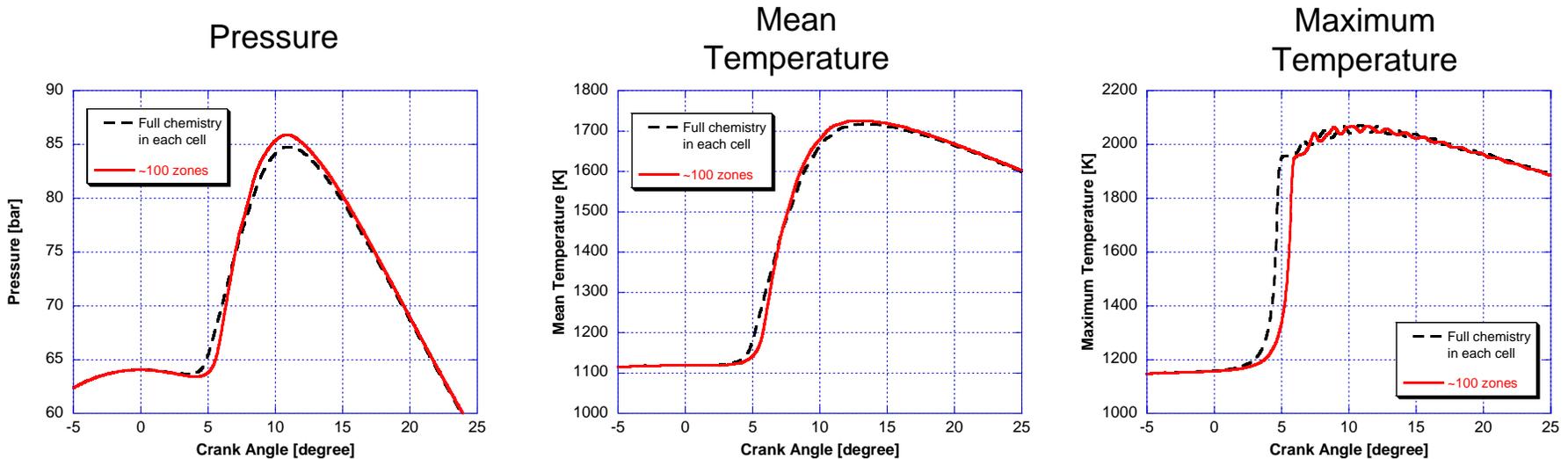
Temperature and composition distributions continue to evolve until late in the compression stroke. Decoupling of flow and chemistry is problematic.



Coupling of KIVA-3V with Multi-Zone Model (KMZ)



Validation of Fully Coupled Kiva-3V with Multi-Zone Model



- The new model gives results that match very well the “exact” solution obtained by solving for detailed chemistry in every cell
- Computational time is reduced significantly (~90% for 10,000 cells)

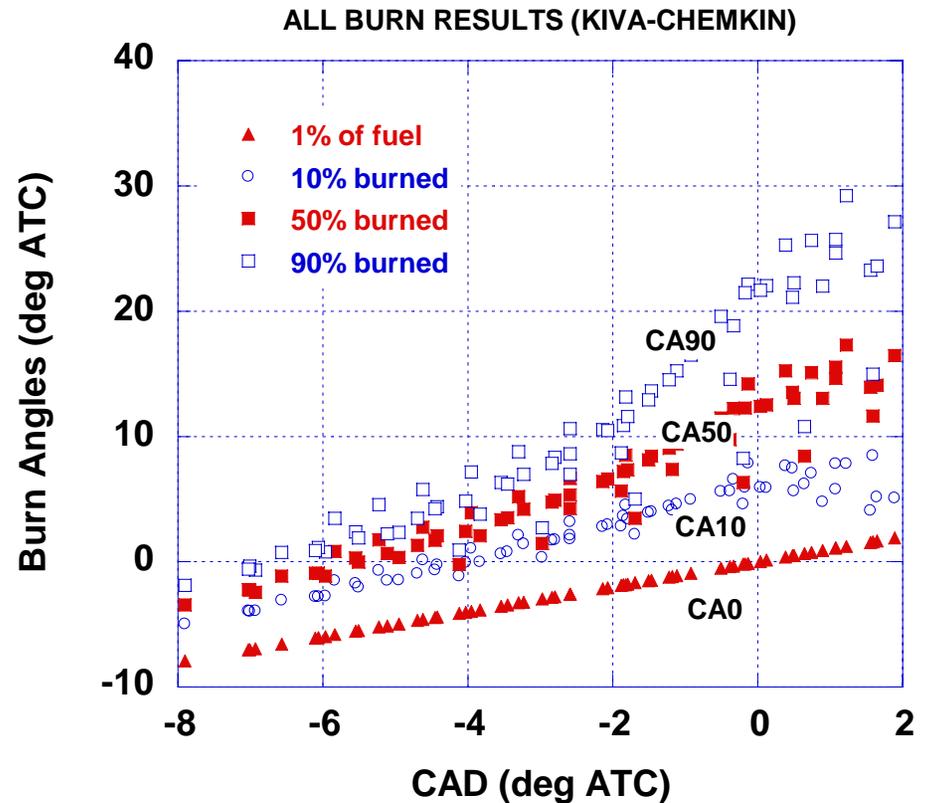
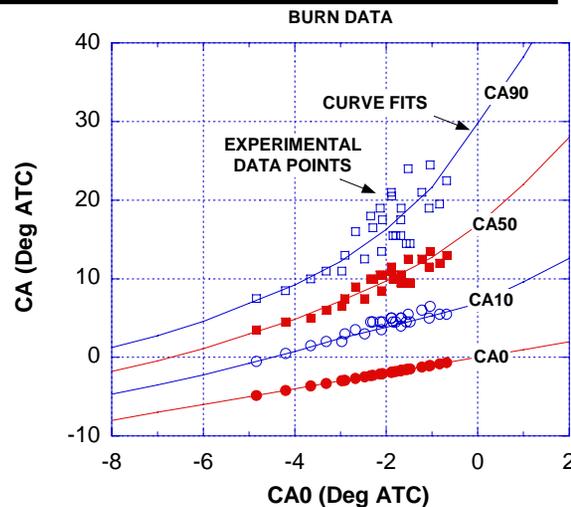


Numerical Experiments: KMZ generated “data”

- Run T sweeps of KMZ model for various operating parameters
- Generate burn angles as function of ignition timing, as well as other variables

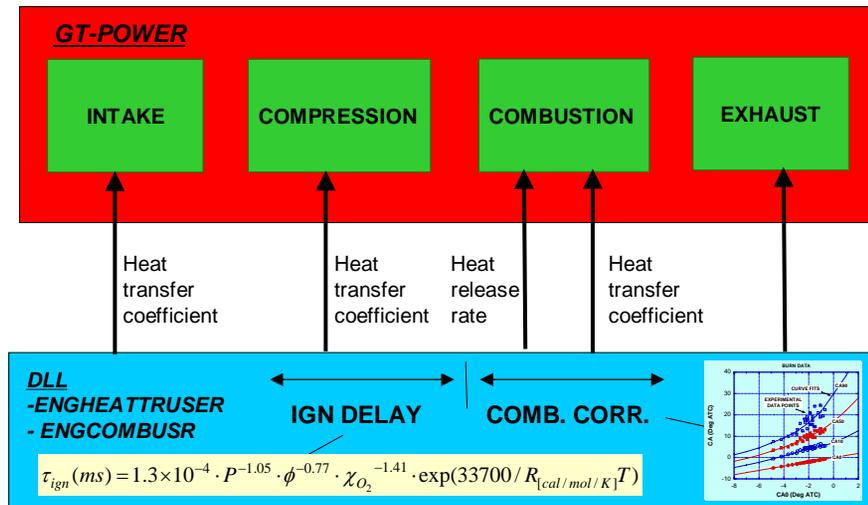
Variable	Sweeps
CR	<u>16</u> , 9
RPM	<u>2000</u> , 1200
Load (fuel)	<u>9</u> , 13 mg

Experimental Data

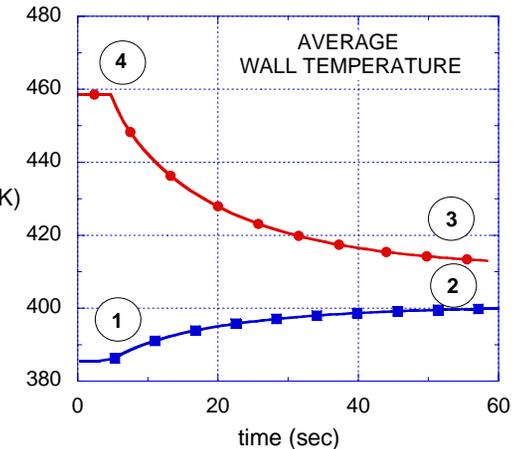
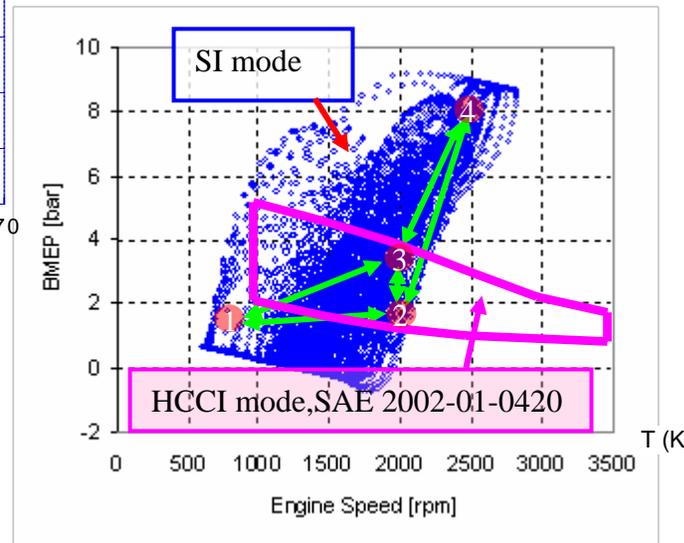
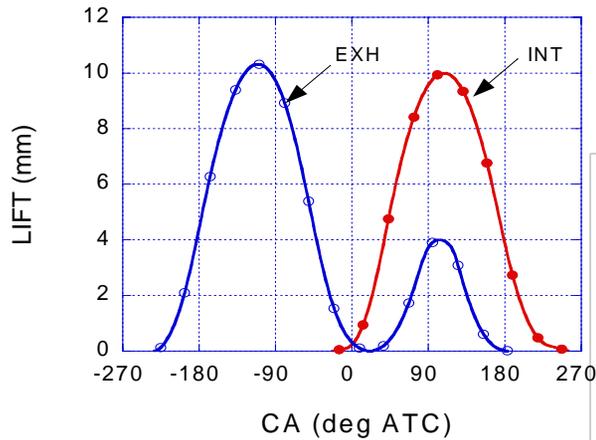


System Studies Approach

- Use GT-Power as platform for system modeling
- Use experiments and CFD models to provide simplified combustion models with correct trends for ignition, burn rates and combustion efficiency
- Develop single-cylinder engine model with manifolds including thermal system submodel
- Explore implementation issues at multi-cylinder and vehicle level, especially related to thermal transients

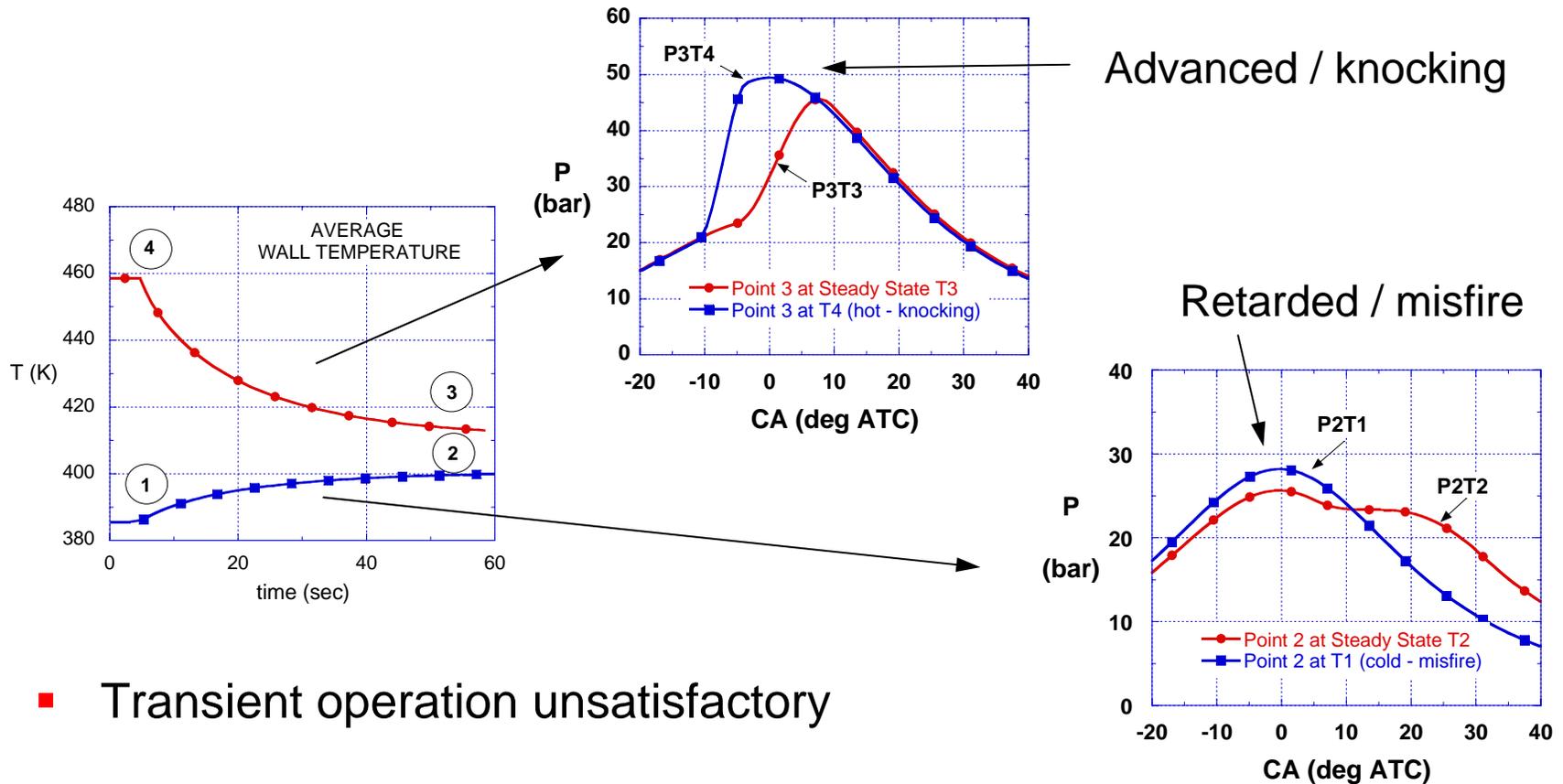


Thermal Transients – Simulating the UM Engine



Thermal Transients – Challenges

- Stable operation possible at steady state thermal points

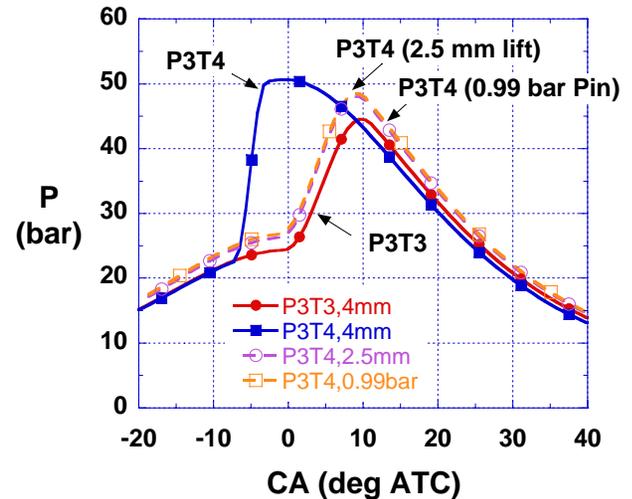
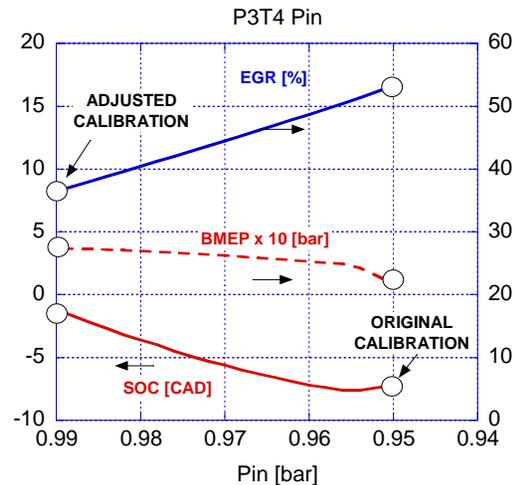
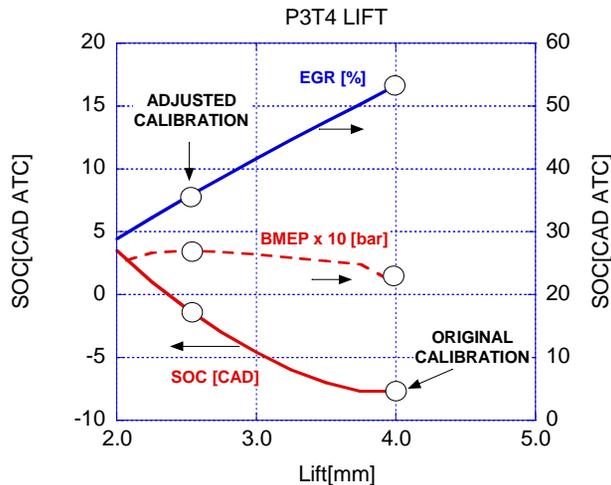


- Transient operation unsatisfactory



Transient Compensation

- Hot-to-cold compensation possible by reducing rebreathing lift or increasing P_{inlet} (both decrease EGR)

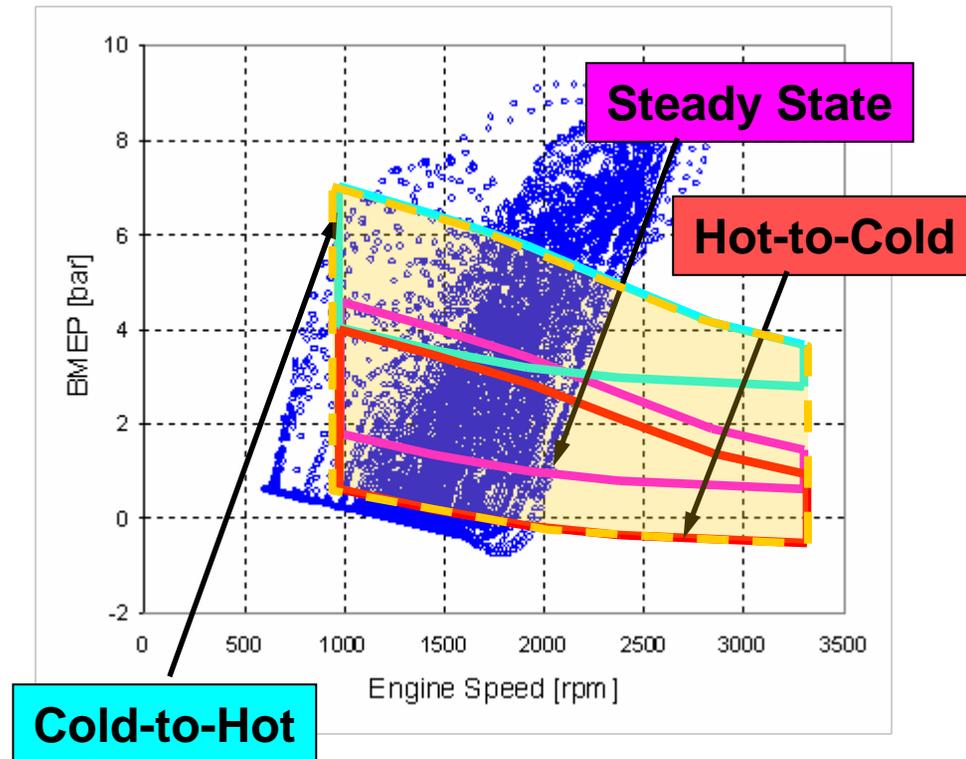


- Cold-to-hot compensation not achievable (not enough EGR heat is available)



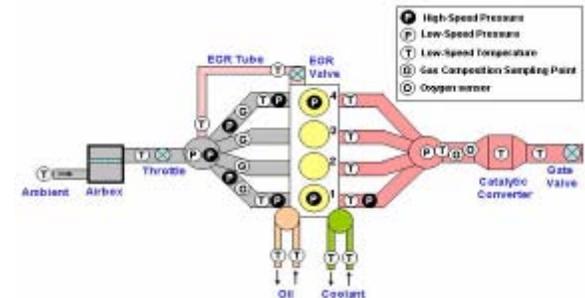
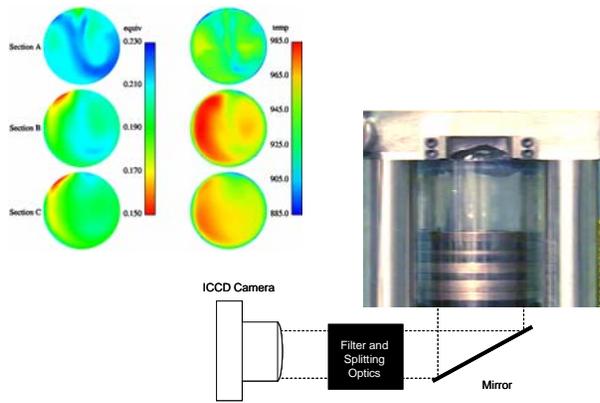
Thermal Transients - Implications

- HCCI regime is shifted depending on direction of transient
- Hot-to-cold will extend the low load HCCI region
- Cold-to-hot will require SI operation until walls warm up
- Challenge is to maximize HCCI operating regime



Future Work

- Refine modeling approaches and validate them against optical and metal engine measurements – emphasize DI, stratified operation
- Extract knowledge developed from detailed CFD + comprehensive chemistry models and capture it into practical correlations compatible with “smart” phenomenological single-zone models
- Provide a single-cylinder module to multi-cylinder system level, controls-oriented simulations
- Use models to develop strategies for HCCI engine in-vehicle operation with alternative fuels



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