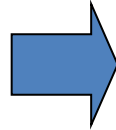
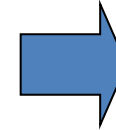


Path to High Efficiency Gasoline Engine

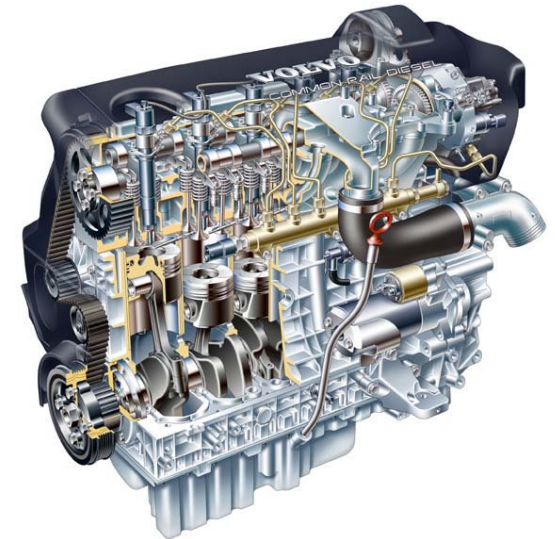
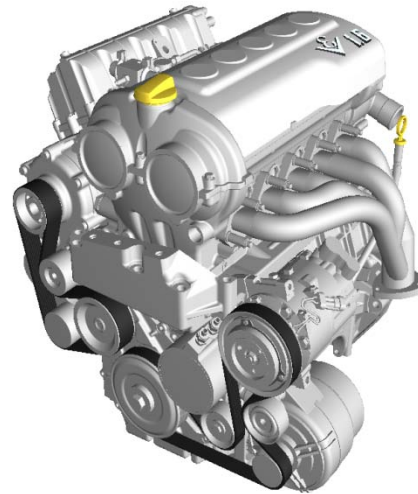
SI



HCCI



PPC

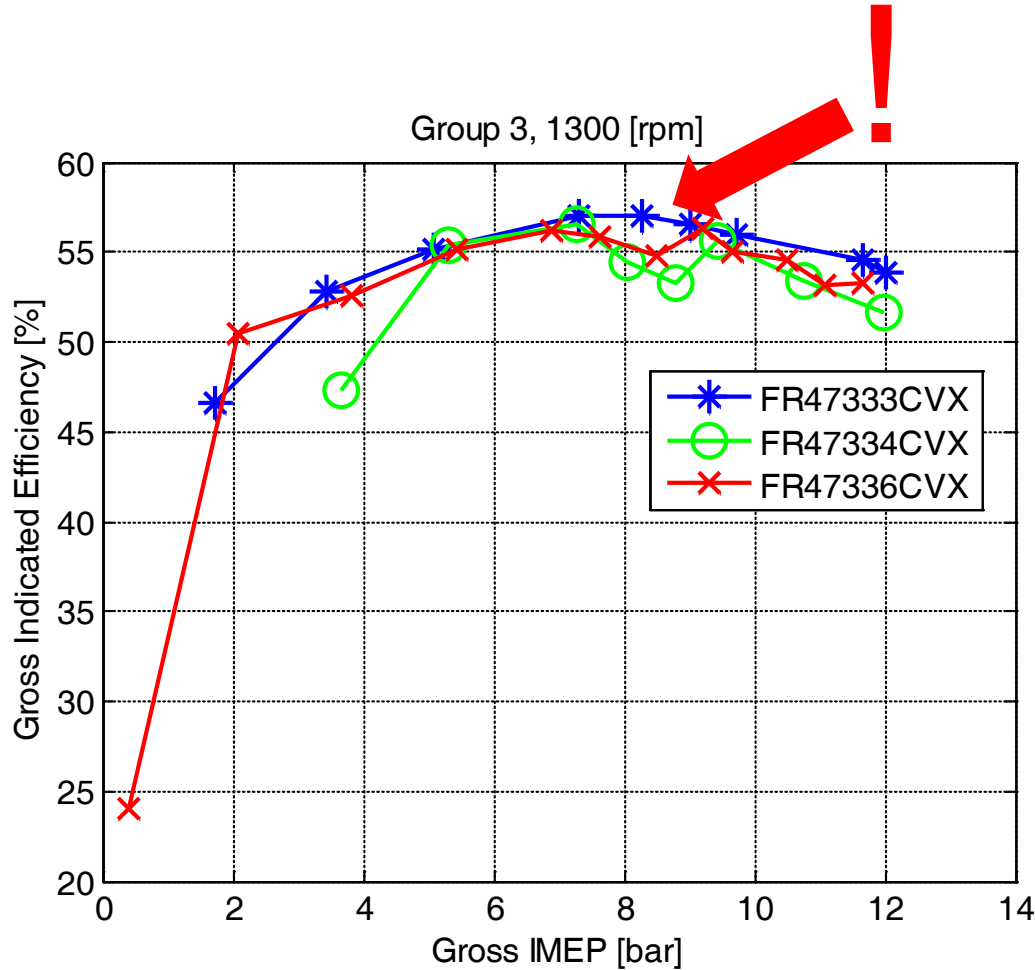


Prof. Bengt Johansson

Division of Combustion Engines
Department of Energy Sciences

Lund University

Scania diesel engine running on gasoline



$\eta_i=57\%$ \leftrightarrow $Isfc = 147 \text{ g/kWh}$ (@43 MJ/kg heating value)



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NO_x, PM, HC and CO engine out



Outline

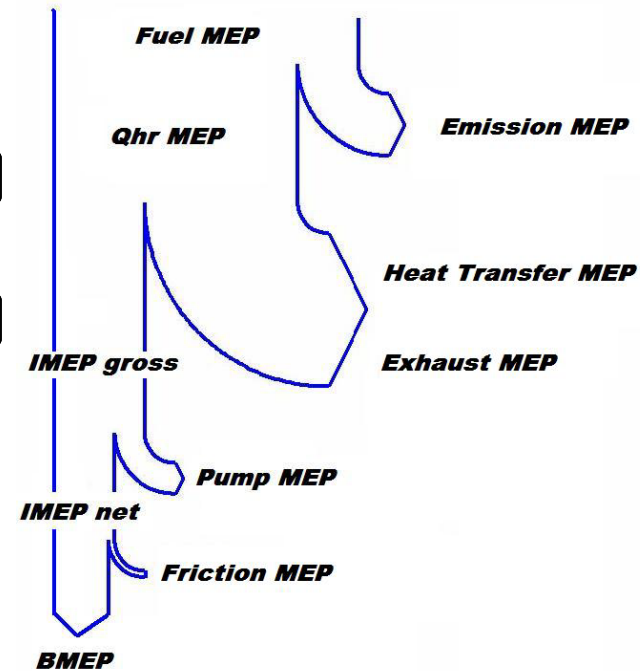
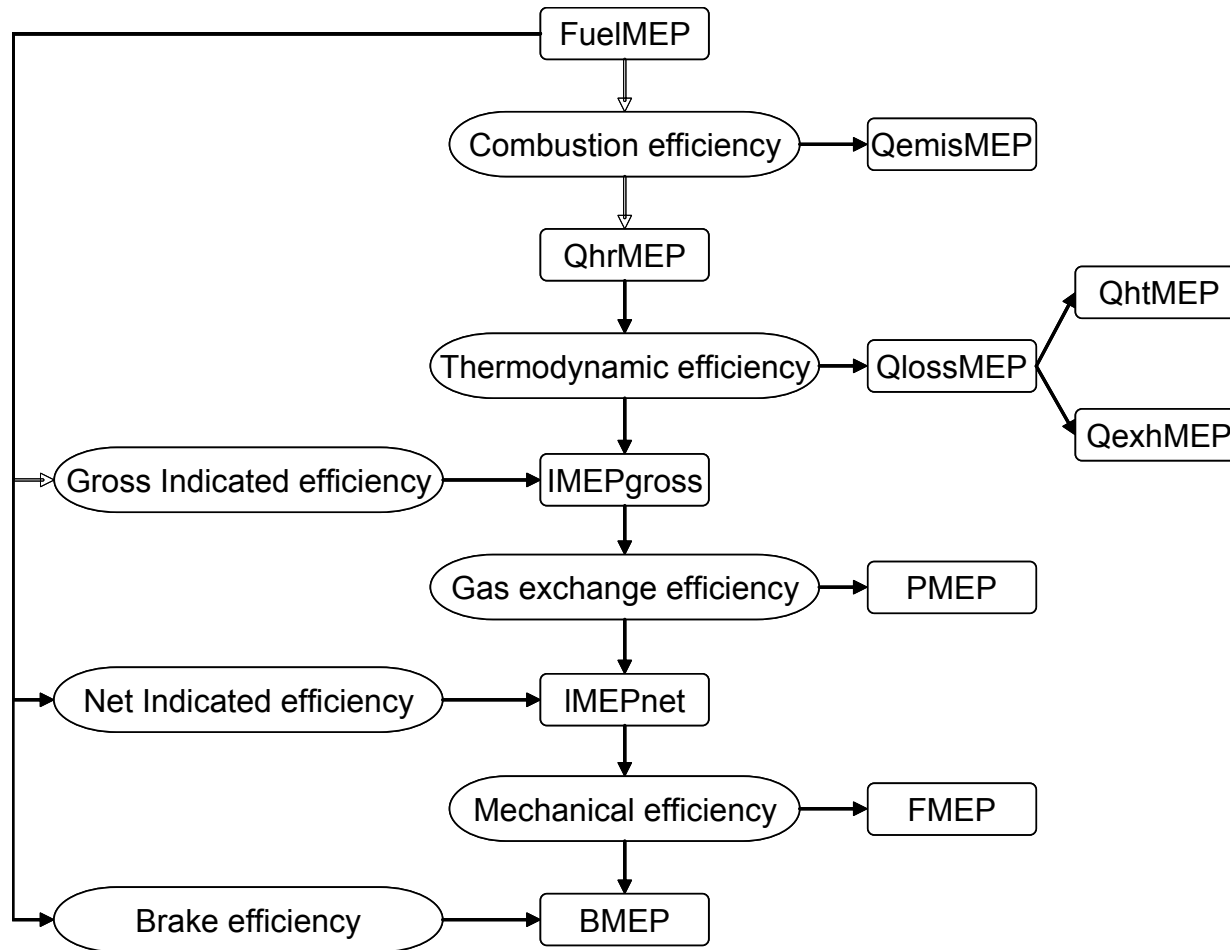
- **HCCI and fuel efficiency**
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Efficiencies?



Energy flow in an IC engine



$$\eta_{Brake} = \eta_{Combustion} * \eta_{Thermodynamic} * \eta_{GasExchange} * \eta_{Mechanical}$$



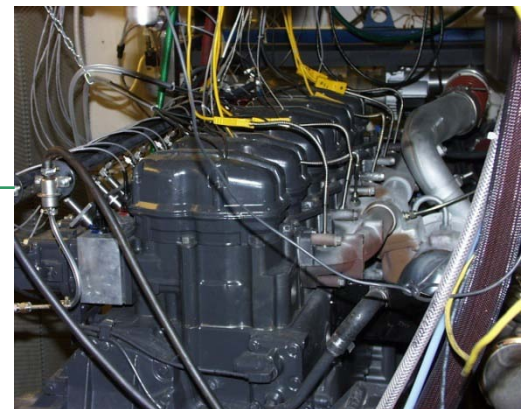
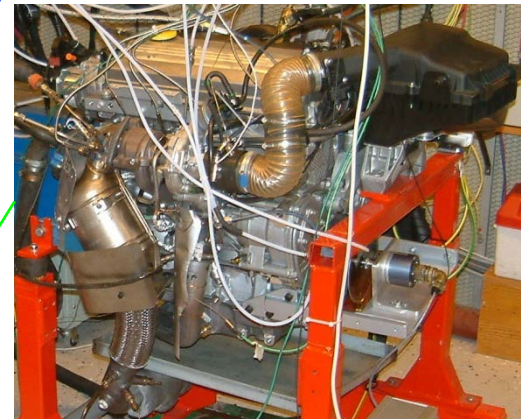
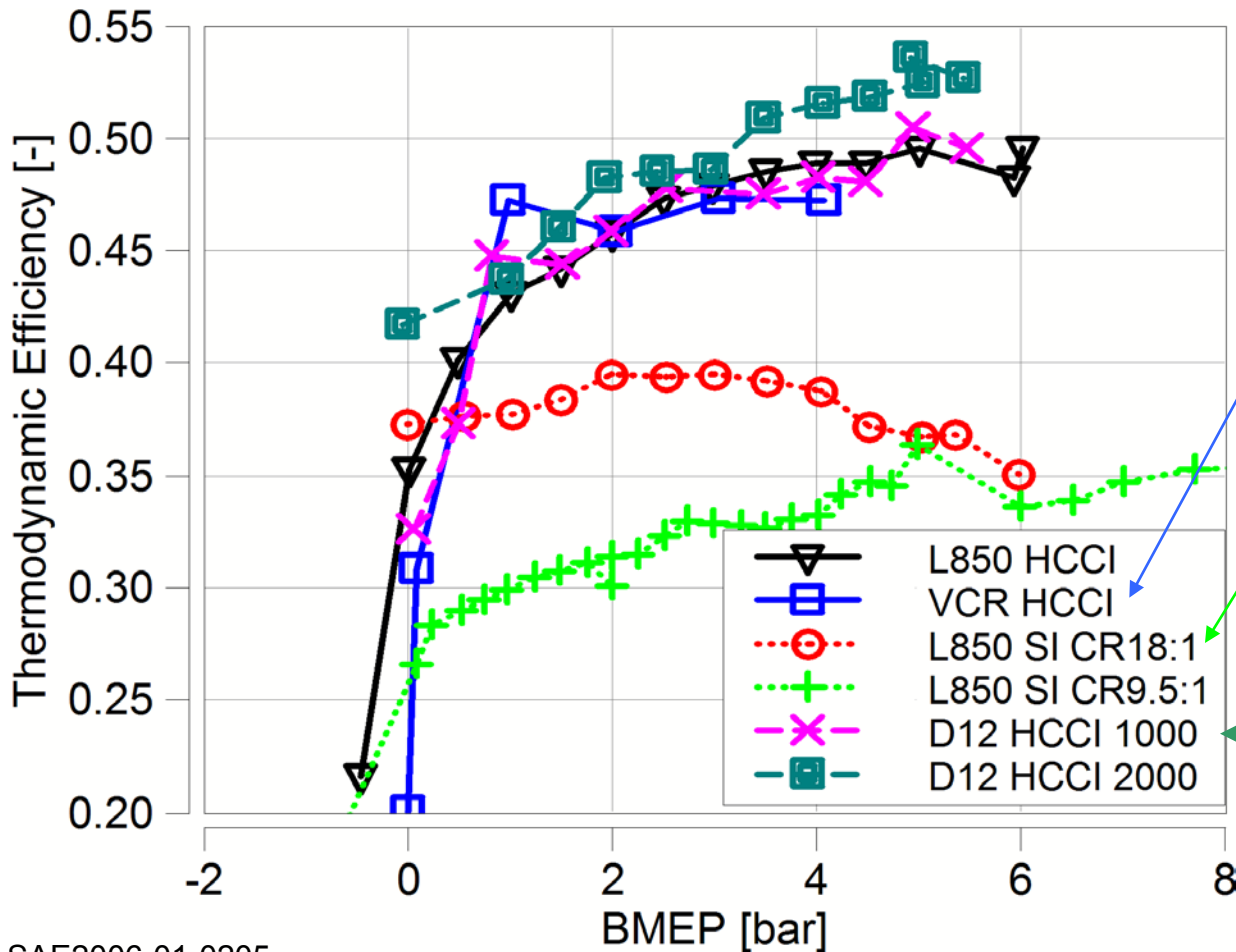
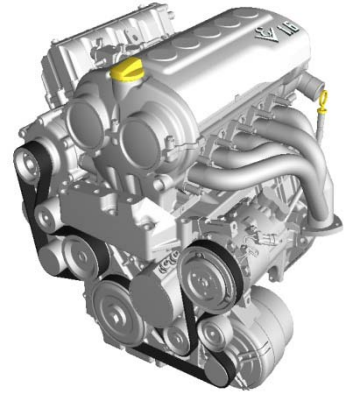
Thermodynamic efficiency

Saab SVC variable compression ratio, VCR, HCCI, Rc=10:1-30:1;

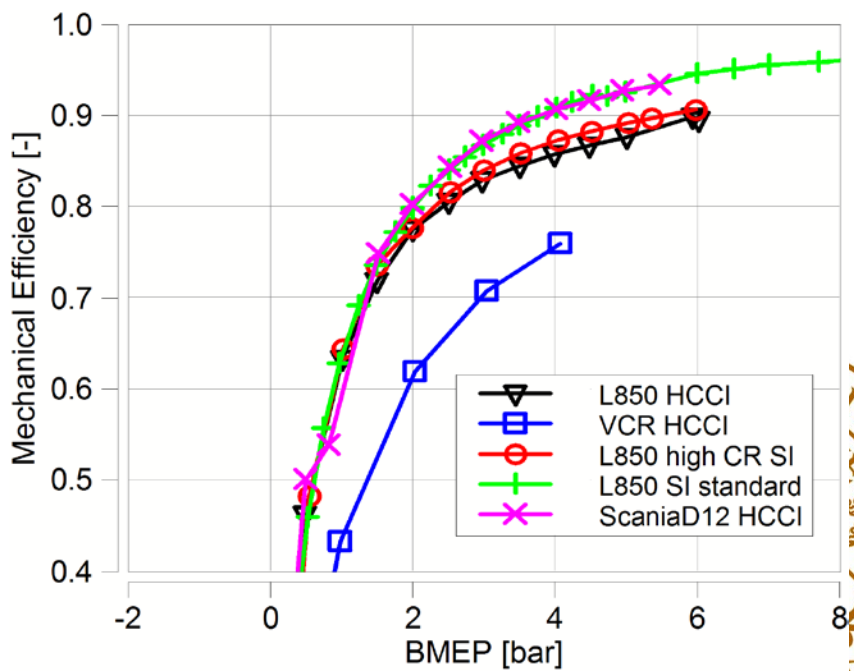
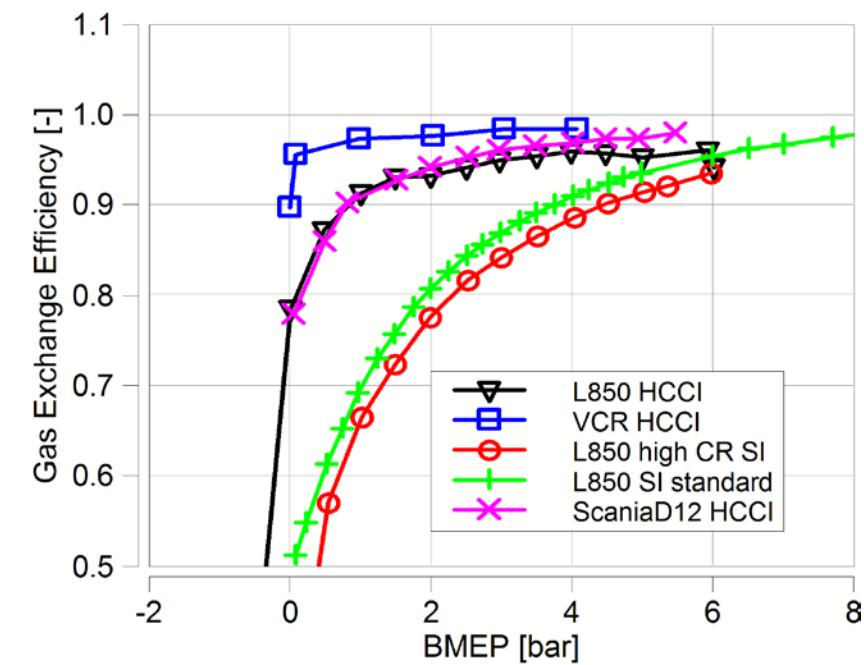
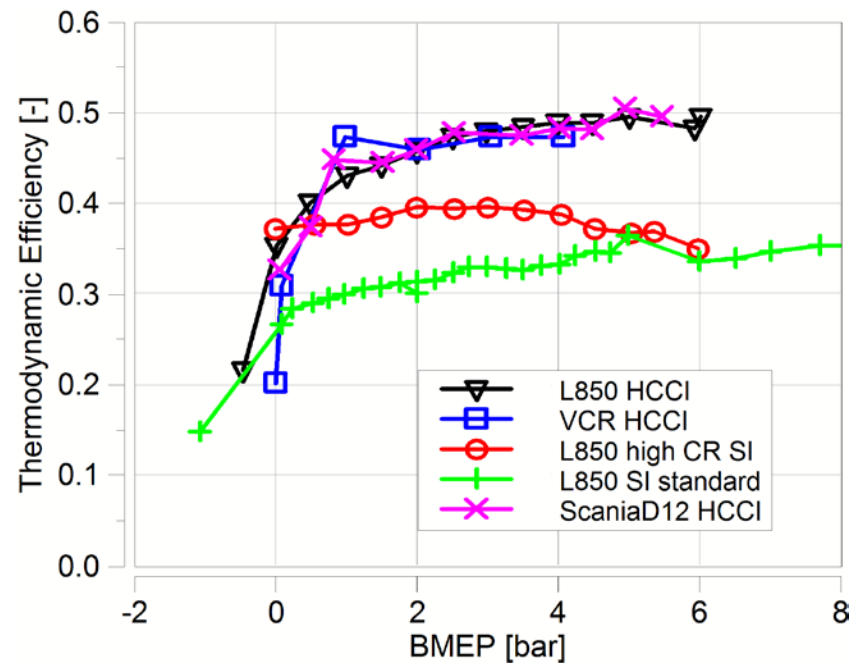
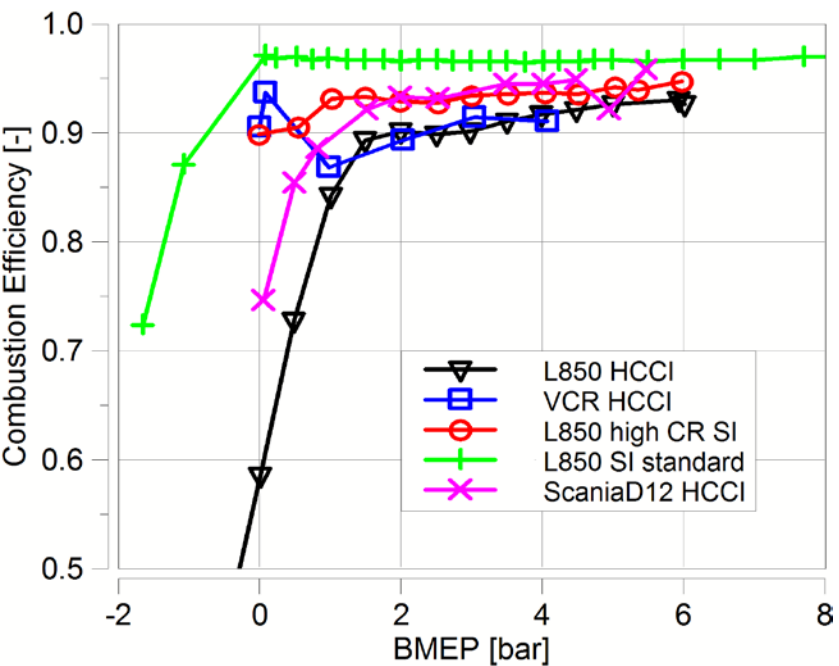
General Motors L850 "World engine", HCCI, Rc=18:1, SI, Rc=18:1, SI, Rc=9.5:1 (std)

Scania D12 Heavy duty diesel engine, HCCI, Rc=18:1;

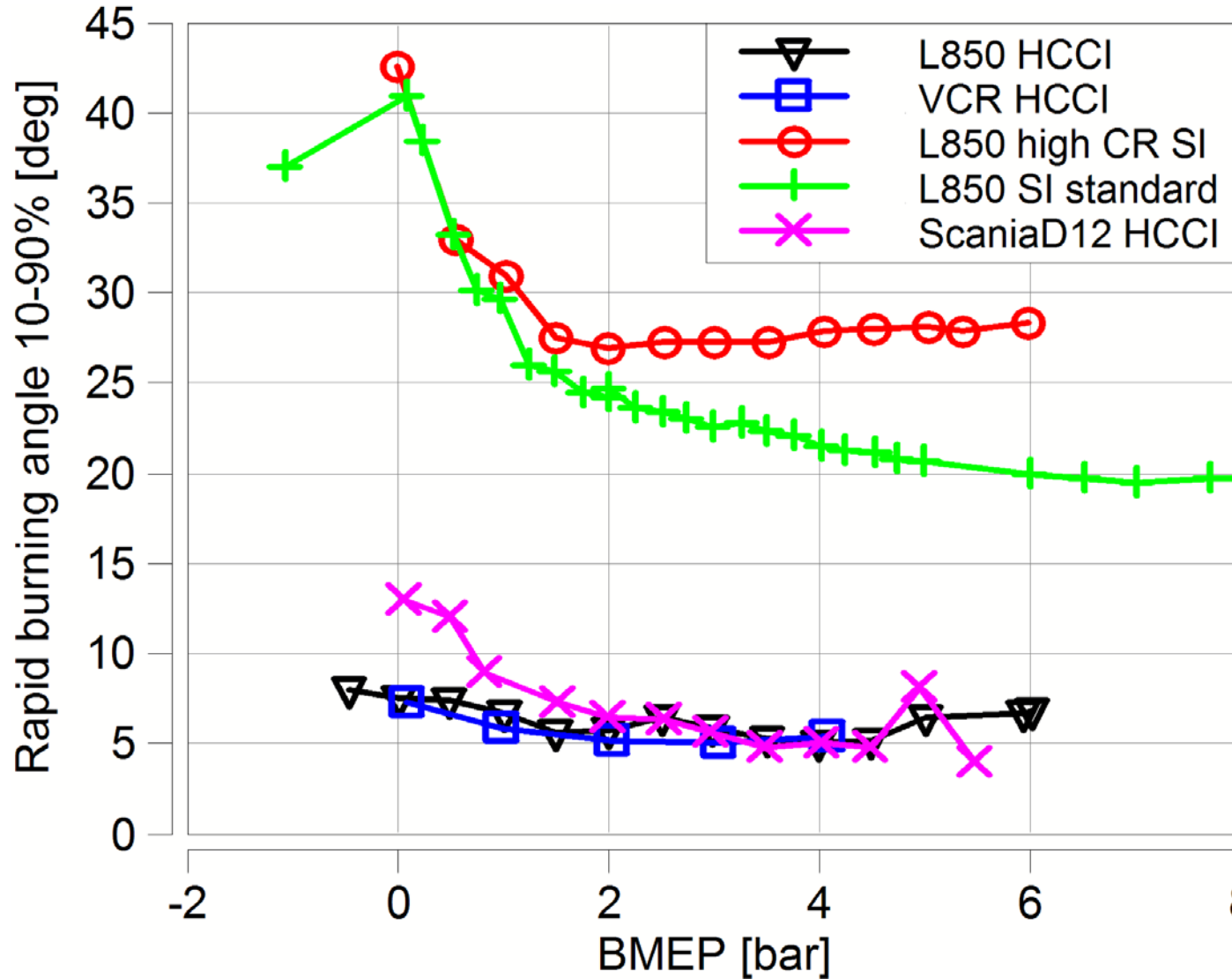
Fuel: US regular Gasoline



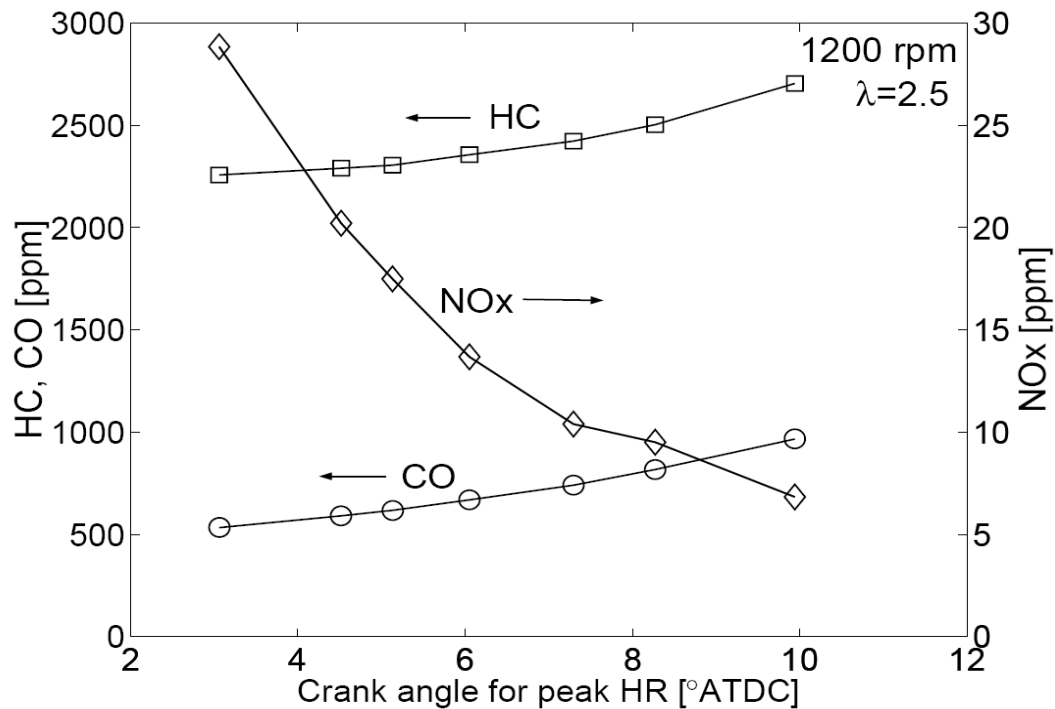
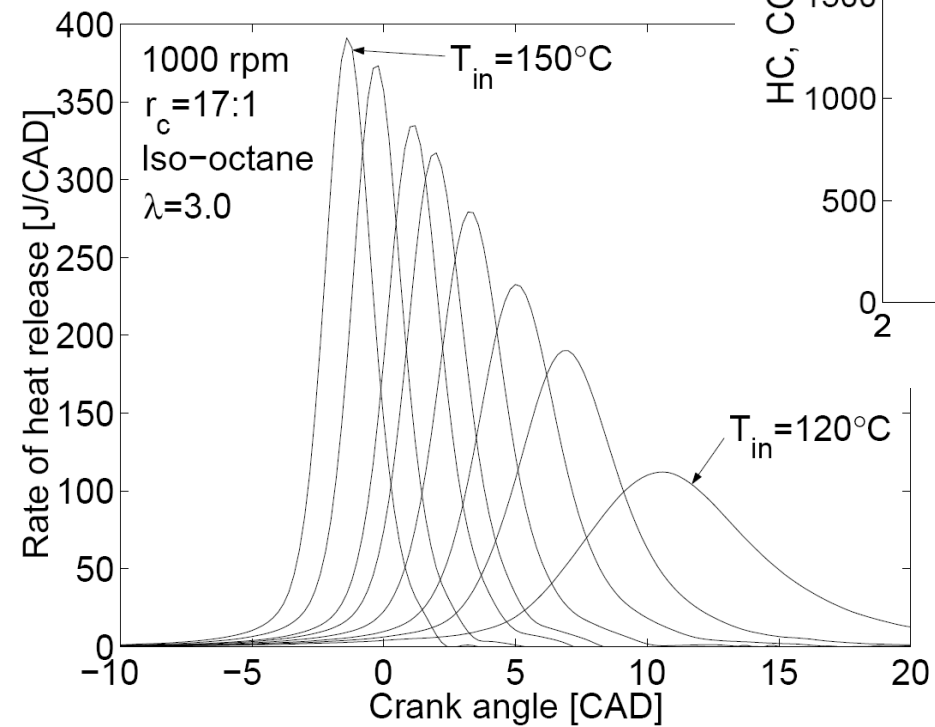
All four efficiencies



Problem with HCCI: Too fast combustion



Phasing HCCI combustion late helps burn rate but reduce η_c



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Background

Combustion concepts

- + Clean with 3-way Catalyst
- Poor low & part load efficiency

Spark Ignition (SI) engine (Gasoline, Otto)

- + High efficiency
- Emissions of NO_x and soot

Compression Ignition (CI) engine (Diesel)

- + High efficiency
- + Ultra low NO_x

Homogeneous Charge Compression Ignition (HCCI)

- Combustion control
- Power density

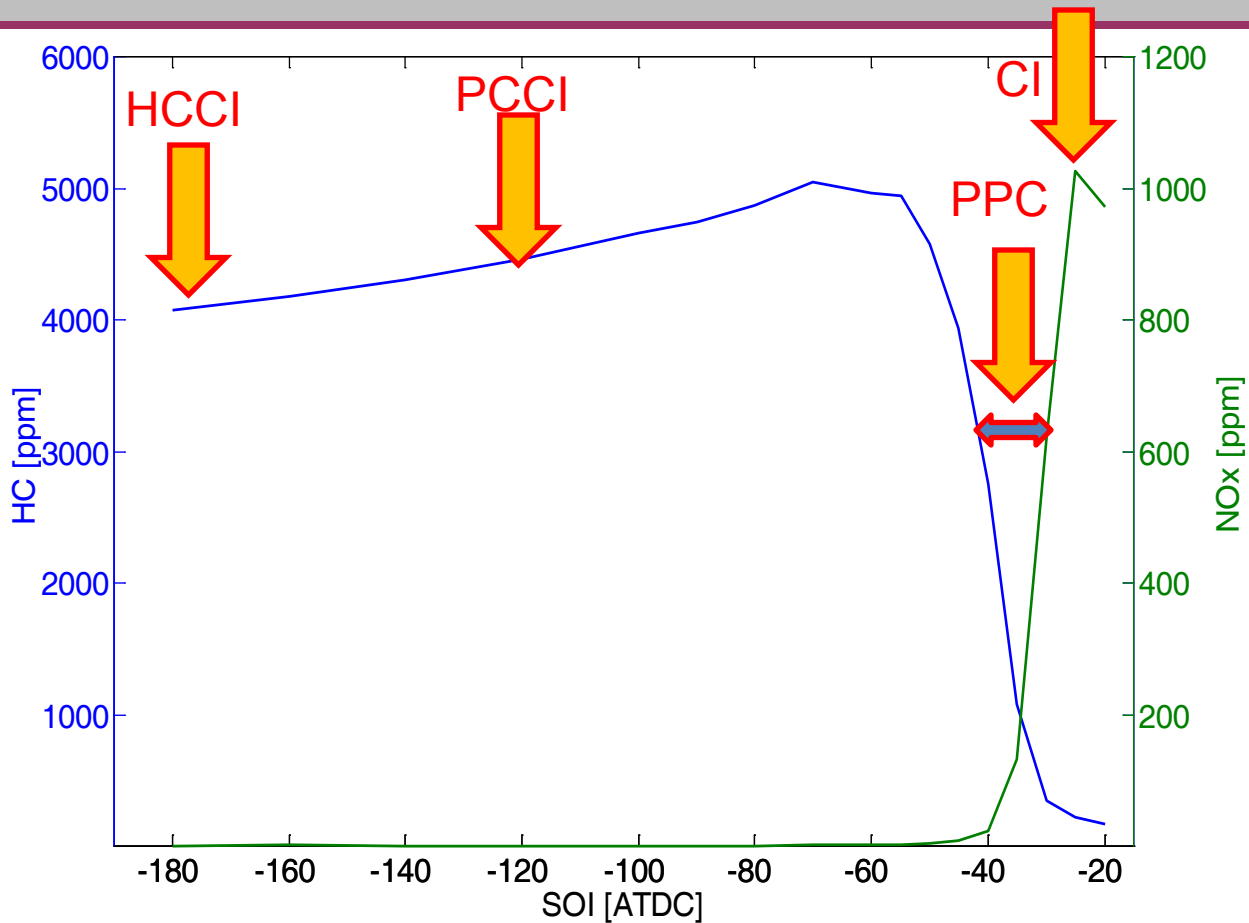
Spark Assisted Compression Ignition (SACI)
Gasoline HCCI

Partially premixed combustion (PPC)
Diesel HCCI

- + Injection controlled
- Less emissions advantage



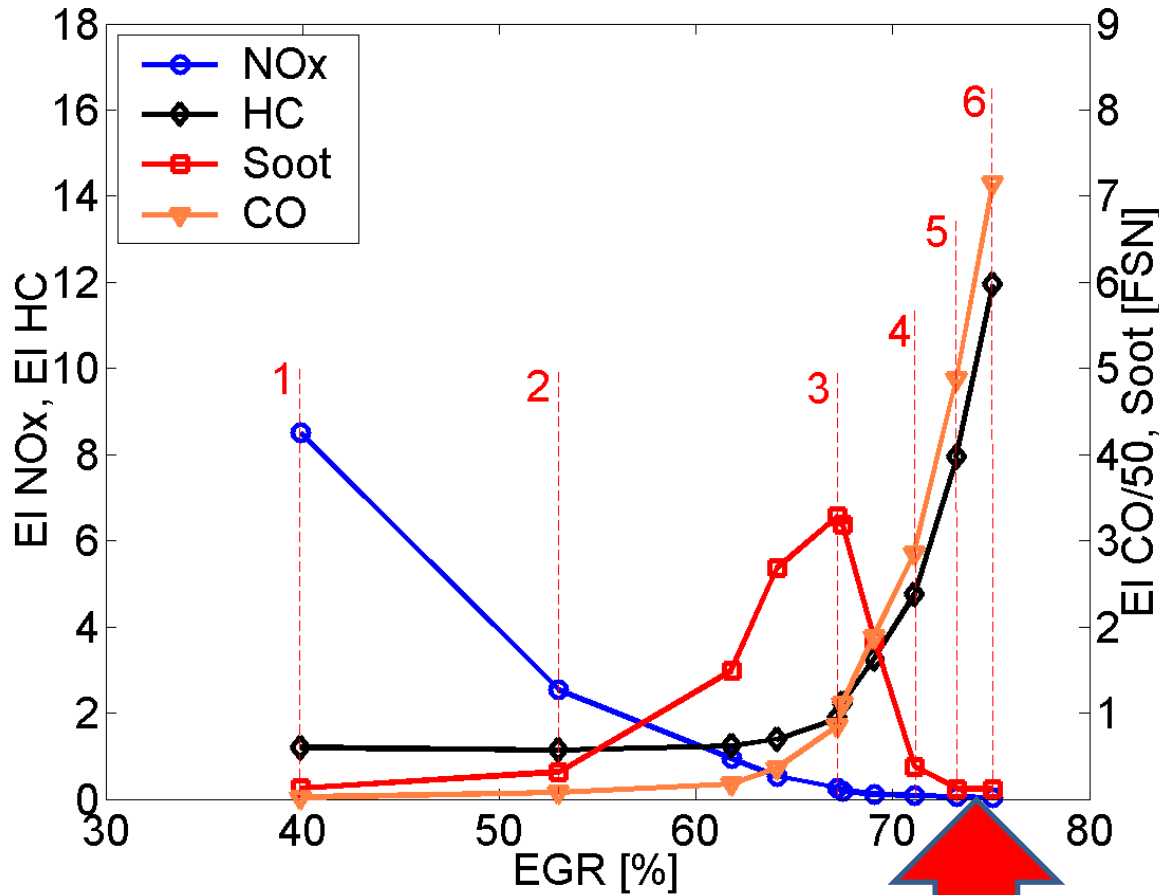
Partially Premixed Combustion, PPC



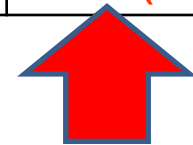
Def: region between truly homogeneous combustion, HCCI, and diffusion controlled combustion, diesel



PPC: Effect of EGR with diesel fuel

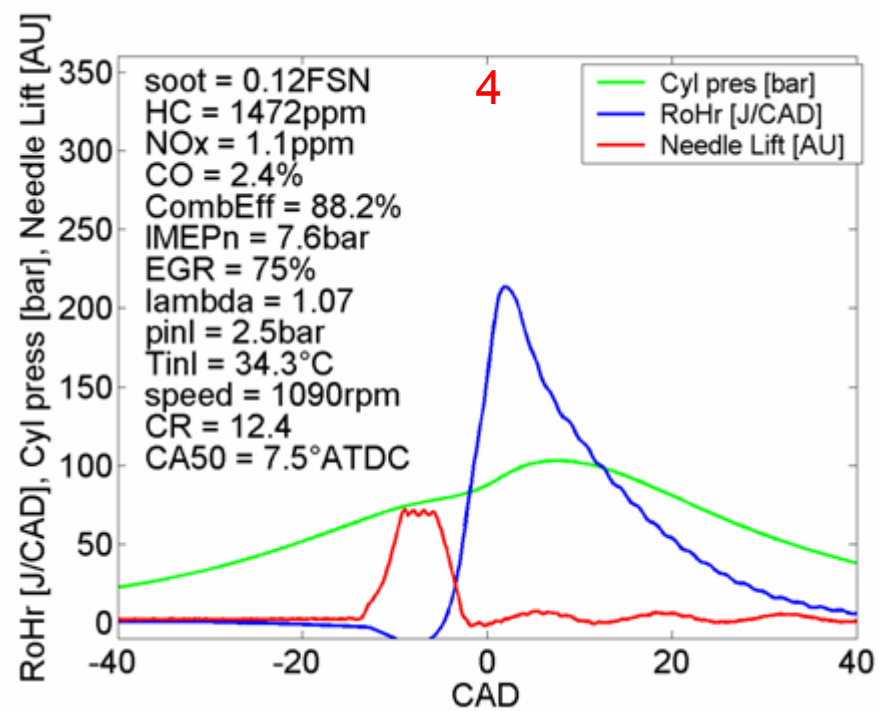
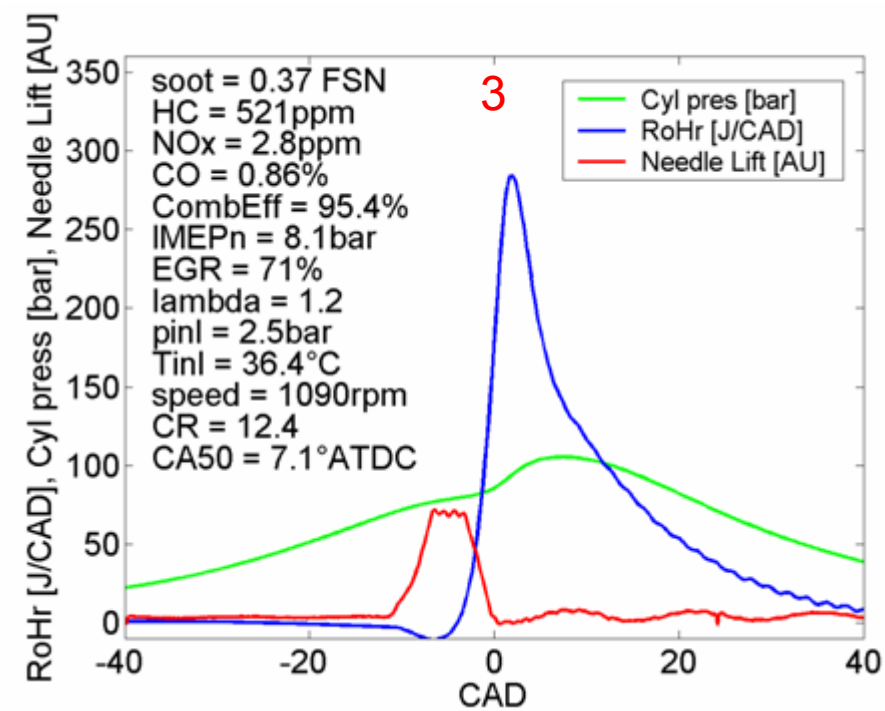
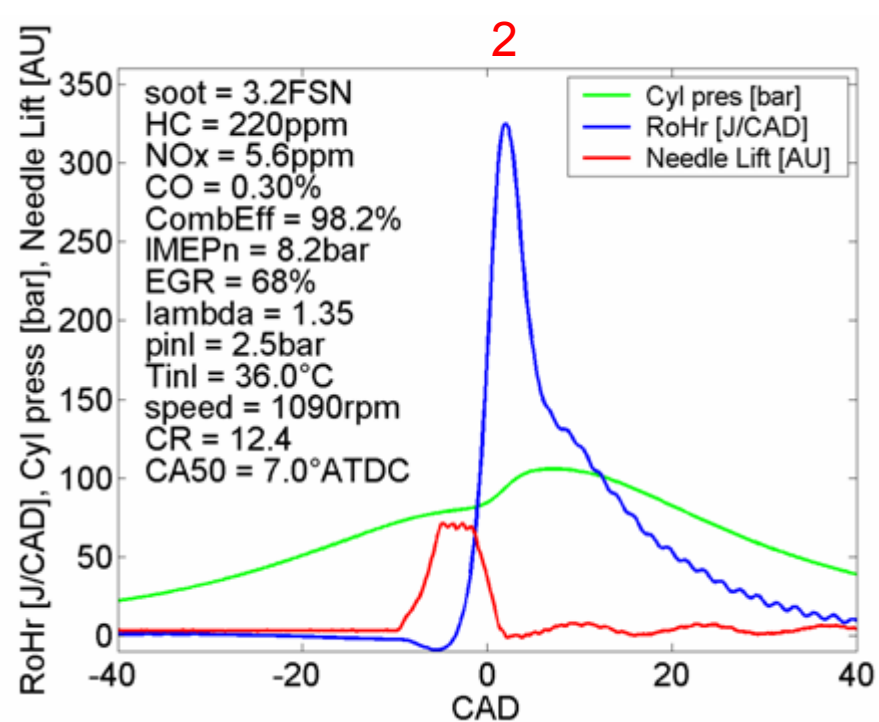
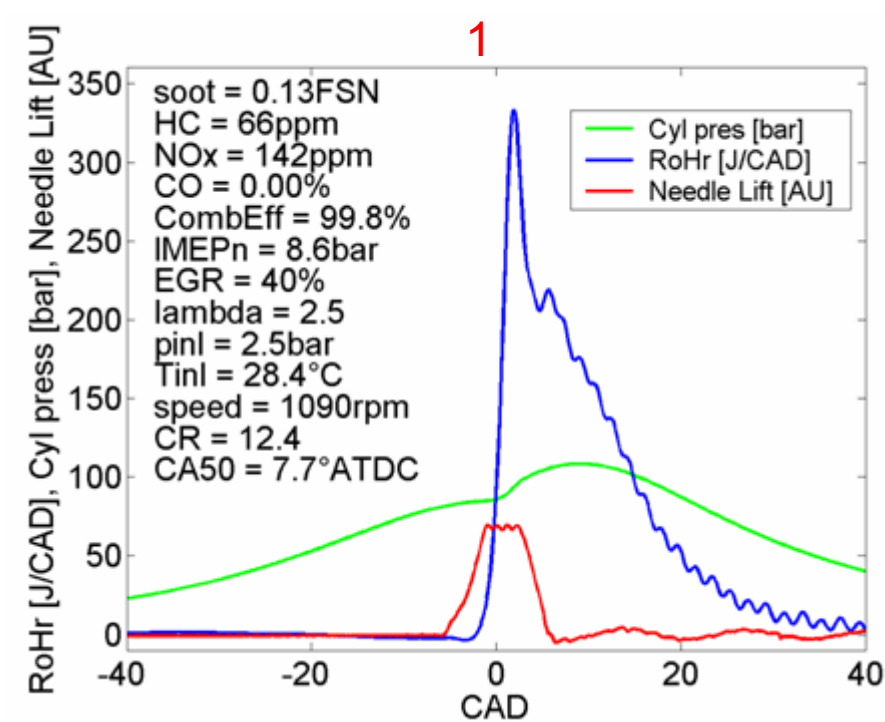


Load	8 bar IMEP
Abs. Inlet Pressure	2.5 bar
Engine Speed	1090 rpm
Swirl Ratio	1.7
Compression Ratio	12.4:1 (Low)



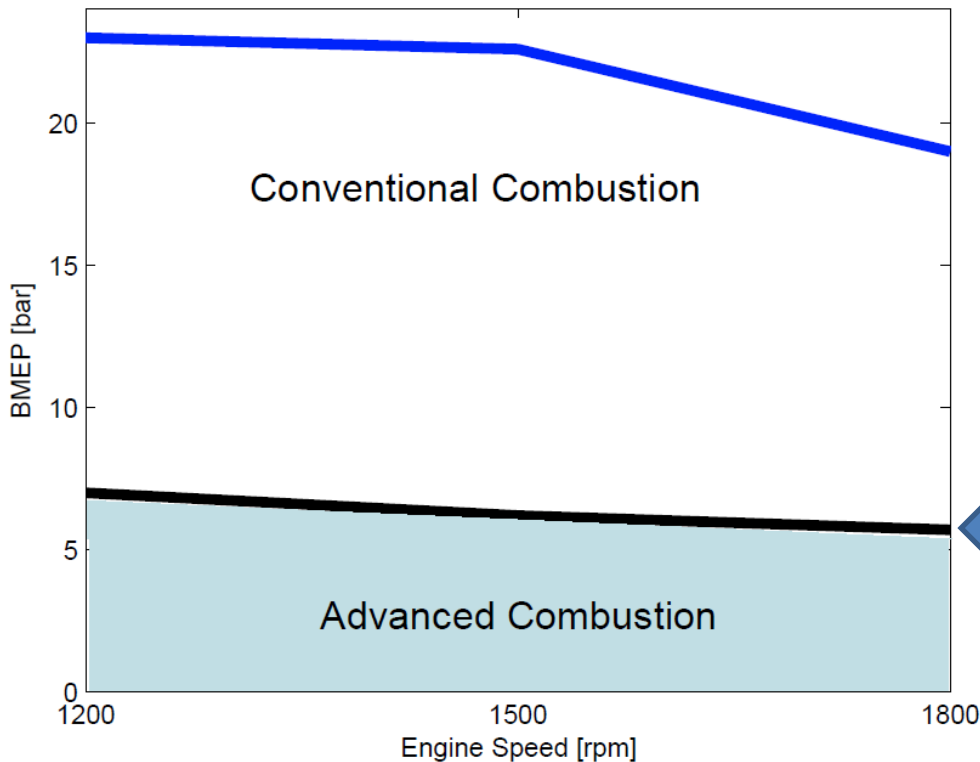
Scania D12 single cylinder





Lund/Delphi/Volvo PPC Project

Volvo D13 Multi-cylinder engine



← NO_x < 0.3 g/kWh
PM < 2 FSN
using
Swedish MK1 **diesel** fuel

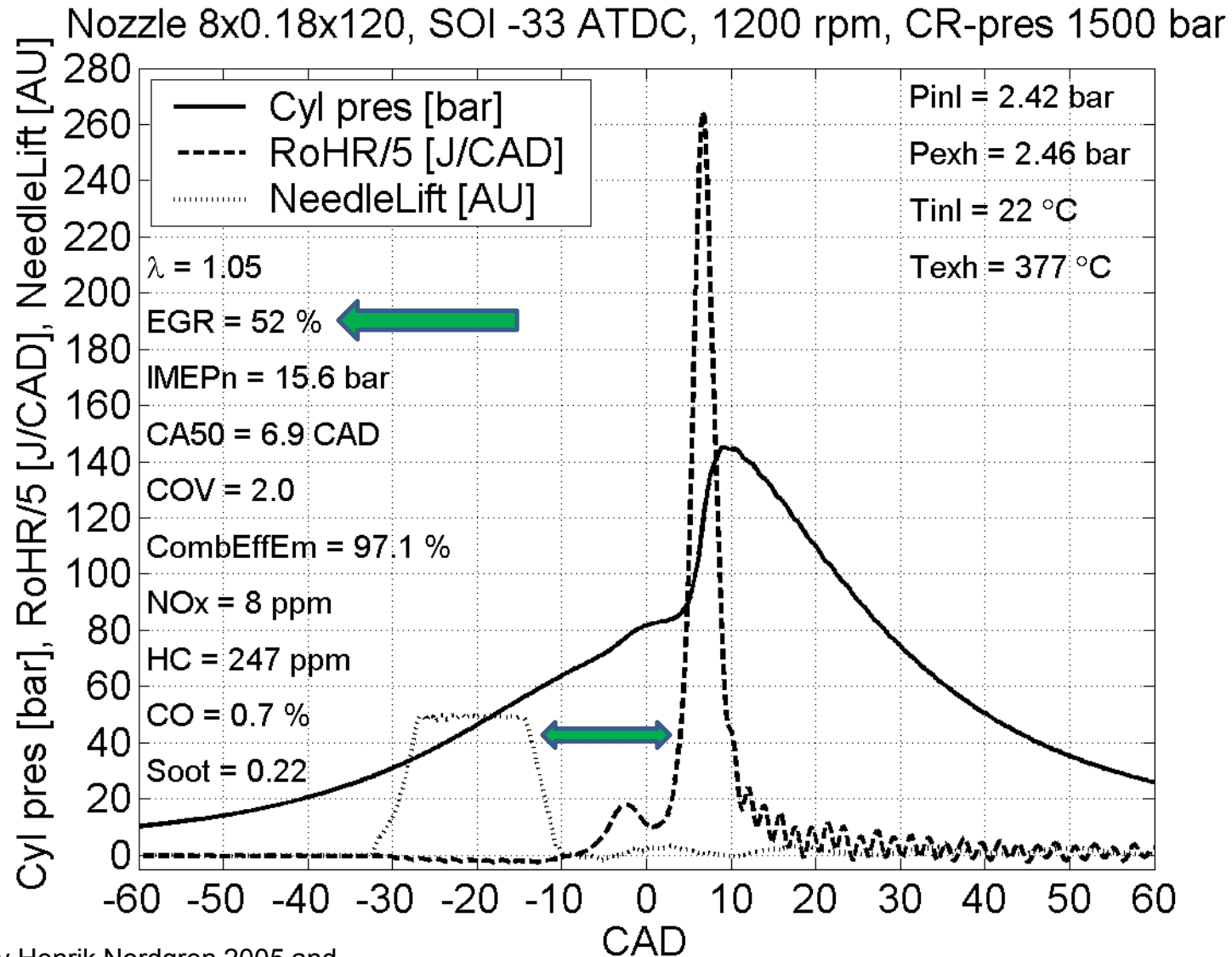


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PPC with low cetane diesel

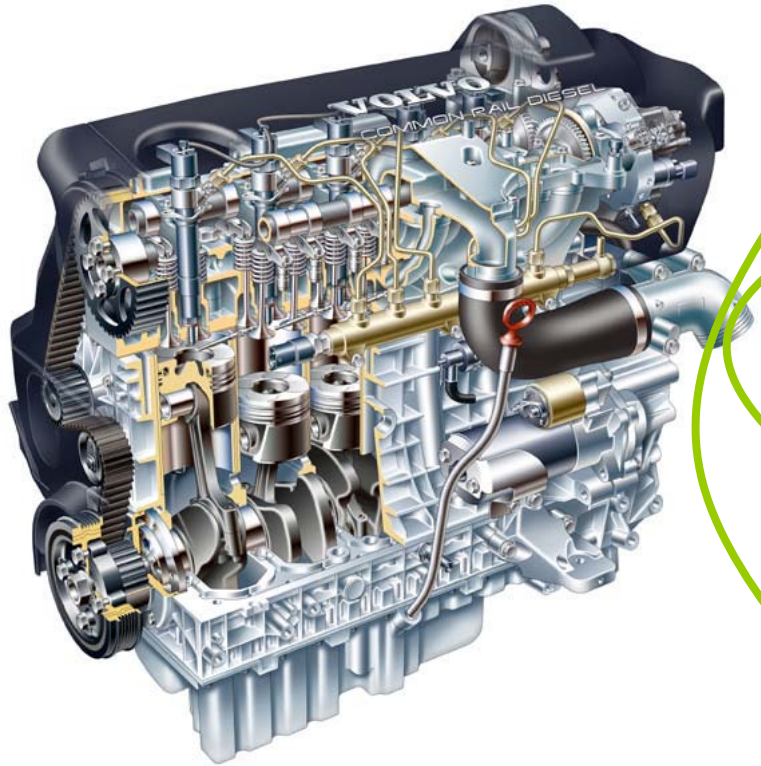


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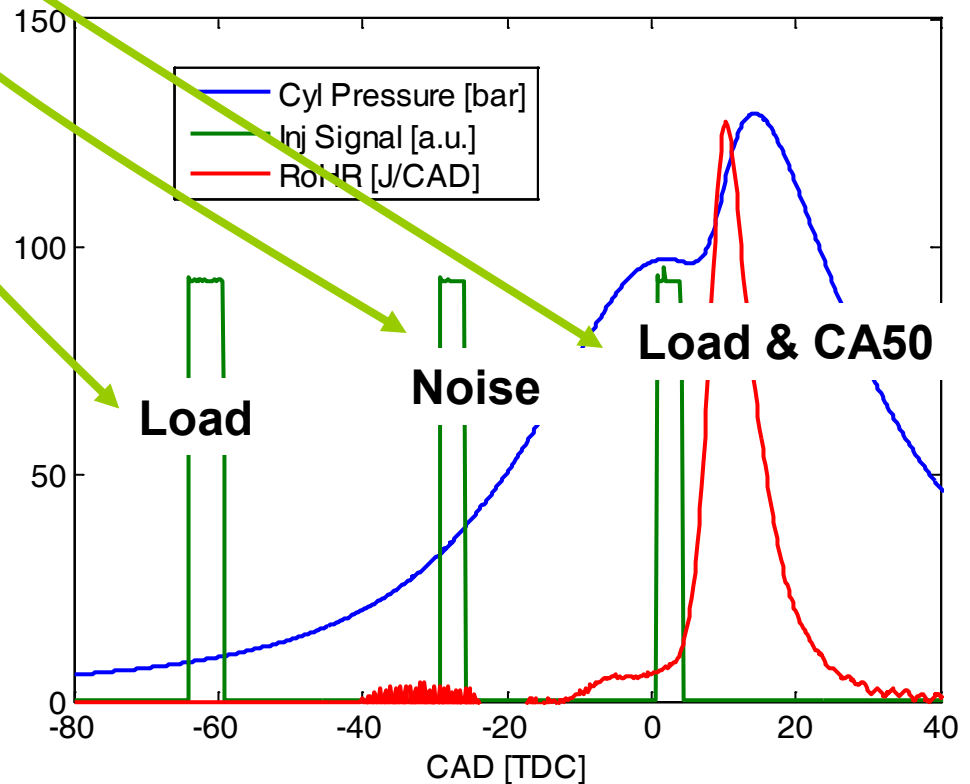


VOLVO D5 with Gasoline

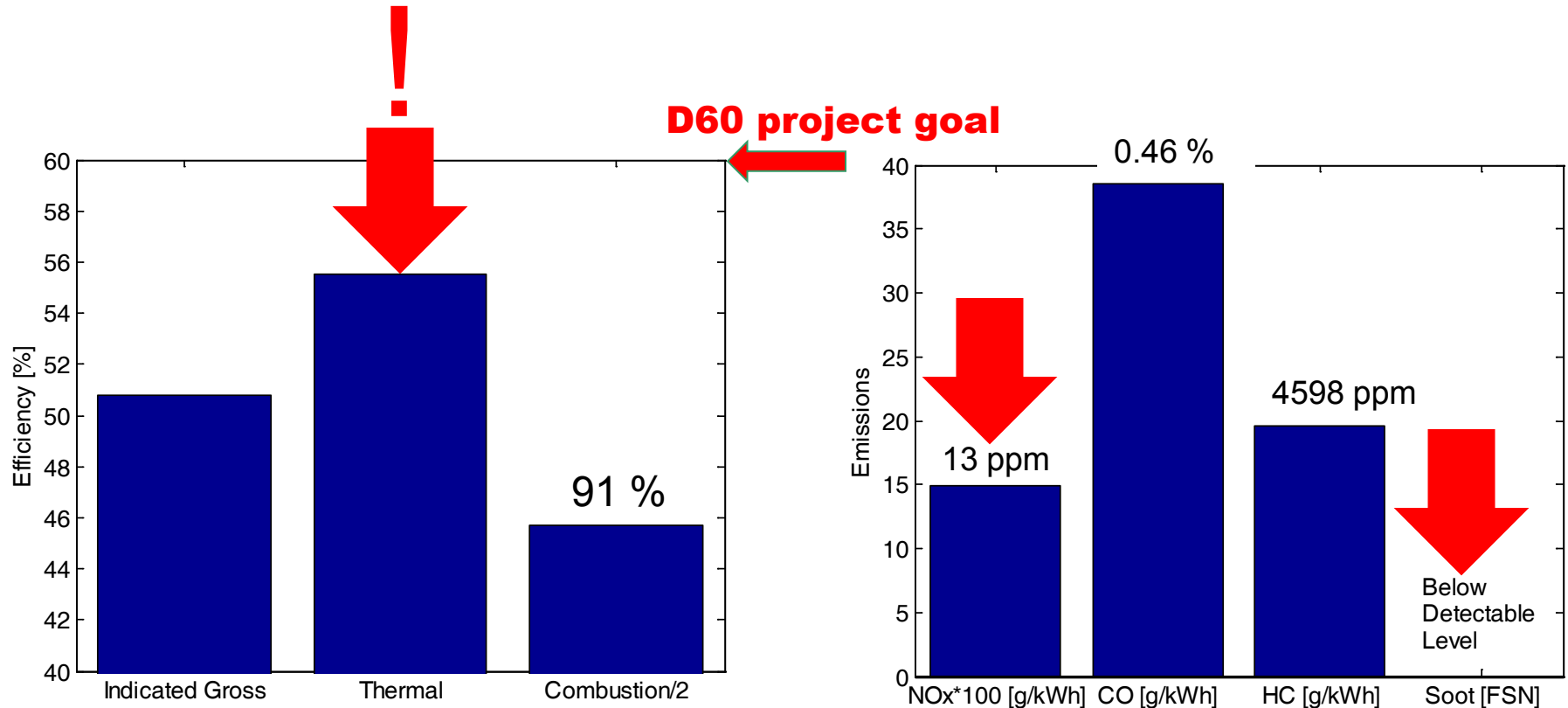


Injection	SOI [TDC]	Fuel MEP [bar]	Percentage [%]
1	-64.00	10.88	41.28
2	-29.20	7.74	29.36
3	0.80	7.74	29.36

N	2000	[rpm]
IMEPg	13.38	[bar]
Pin	2.57	[bar]
Tin	354	[K]
EGR	39	[%]
lambda	1.75	[-]



Efficiencies & Emissions



dPmax	7.20	[bar/CAD]
CA5	3.40	[TDC]
ID	-1.00	[CAD]
CA50	11.35	[TDC]
CA90-10	13.00	[CAD]

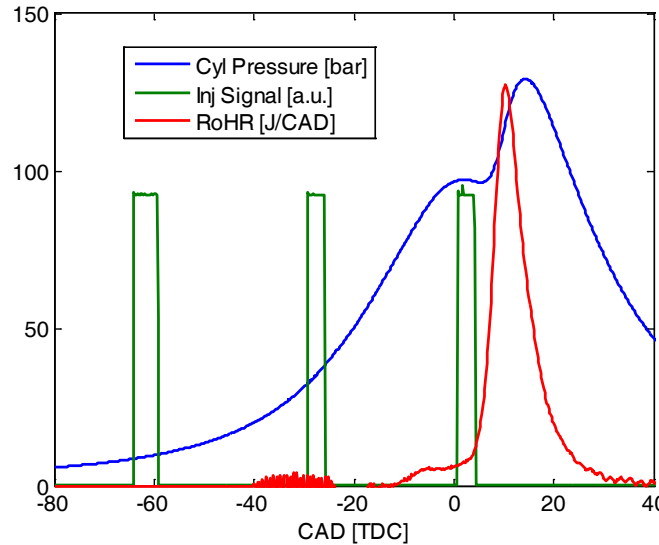


Burn rate and η_T

Optimum Thermodynamic efficiency

Low effective expansion ratio

High heat losses

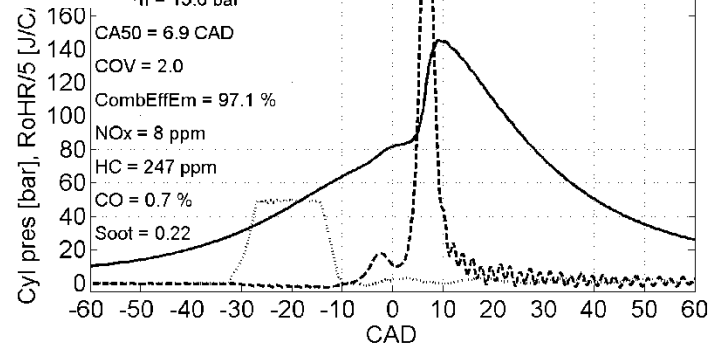


$\phi \times 0.18 \times 120$, SOI -33 ATDC, 1200 rpm, CR-pres 1500 bar

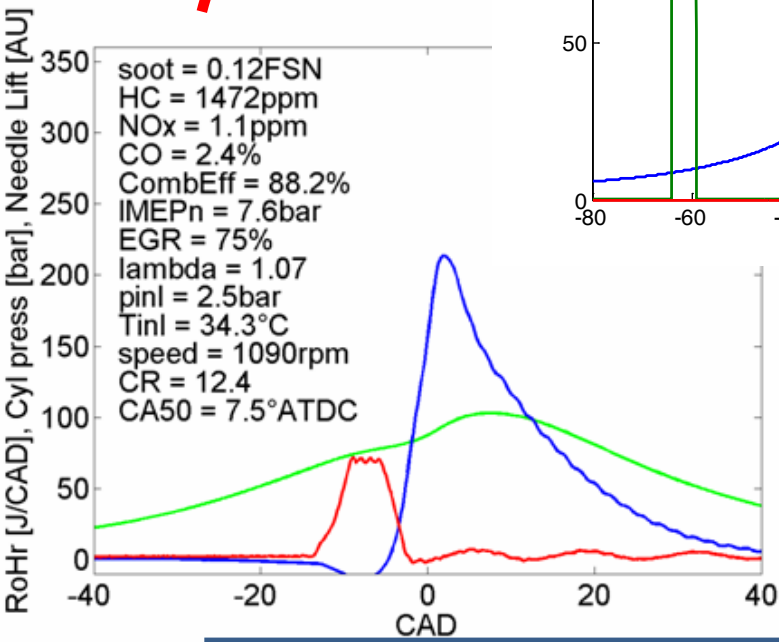
— Cyl pres [bar]
 --- RoHR/5 [J/CAD]
 ... NeedleLift [AU]

$\lambda = 1.05$
 $\eta = 52\%$
 $\eta_{in} = 15.6 \text{ bar}$

$P_{inl} = 2.42 \text{ bar}$
 $P_{exh} = 2.46 \text{ bar}$
 $T_{inl} = 22 \text{ }^\circ\text{C}$
 $T_{exh} = 377 \text{ }^\circ\text{C}$



$soot = 0.12FSN$
 $HC = 1472ppm$
 $NO_x = 1.1ppm$
 $CO = 2.4\%$
 $CombEff = 88.2\%$
 $IMEP_n = 7.6bar$
 $EGR = 75\%$
 $\lambda = 1.07$
 $pinl = 2.5bar$
 $Tinl = 34.3^\circ\text{C}$
 $speed = 1090rpm$
 $CR = 12.4$
 $CA_{50} = 7.5^\circ\text{ATDC}$



Premixedness 22



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Experimental setup, Scania D12



Bosch Common Rail		
Prail _{max}	1600	[bar]
Orifices	8	[-]
Orifice Diameter	0.18	[mm]
Umbrella Angle	120	[deg]
Engine / Dyno Spec		
BMEP _{max}	15	[bar]
V _d	1951	[cm ³]
Swirl ratio	2.9	[-]

Fuel: Gasoline or Ethanol



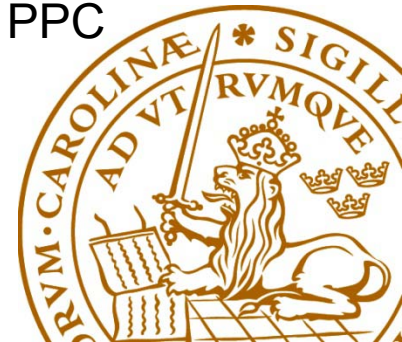
Two Test Series: High & Low Compression Ratio



Low Compression Ratio PPC

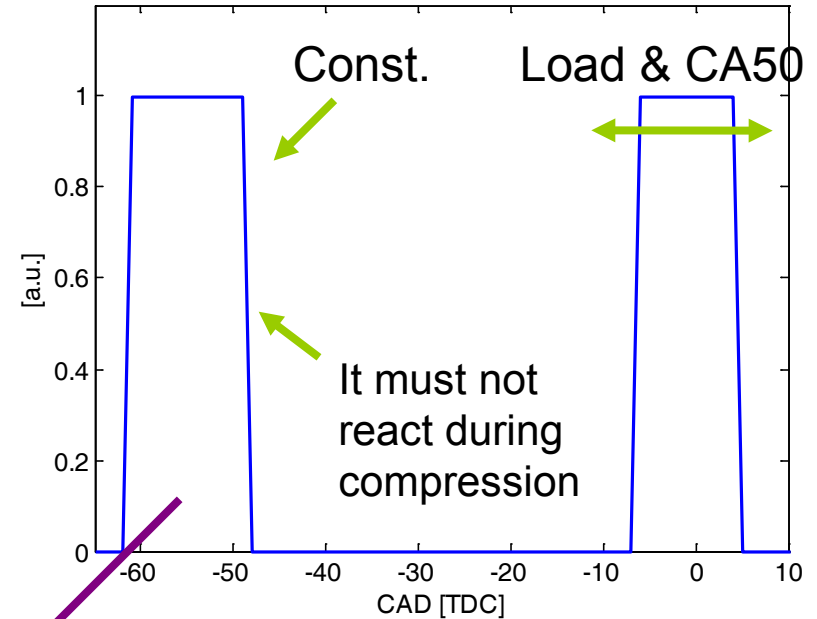


High Compression Ratio PPC



Injection Strategy

It consists of two injections. The first one is placed @ -60 TDC to create a homogeneous mixture while the second around TDC. The stratification created by the second injection triggers the combustion. The first injection must not react during the compression stroke, this is achieved by using EGR.

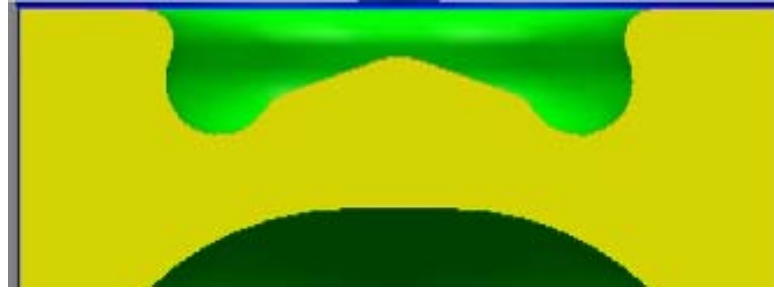


Fuel amount in the pilot is a function of:

- 1.rc
- 2.RON/MON
- 3.EGR



High Compression Ratio PPC



IMEP sweep @ 1300 [rpm]

EGR ~ const throughout the sweep, 40-50 [%]

λ ~ const throughout the sweep, 1.5-1.6 [-]

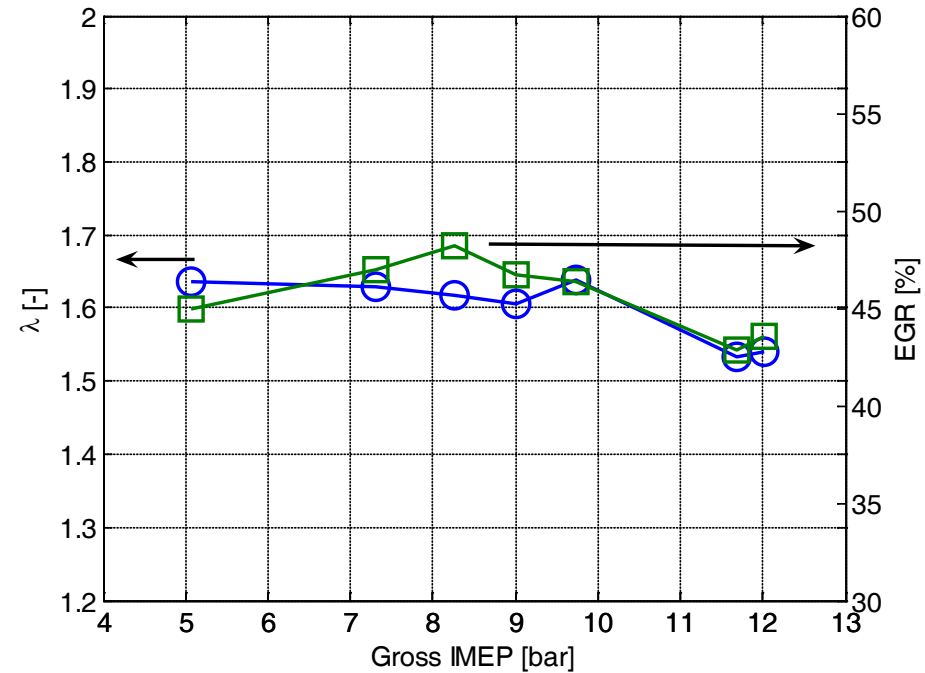
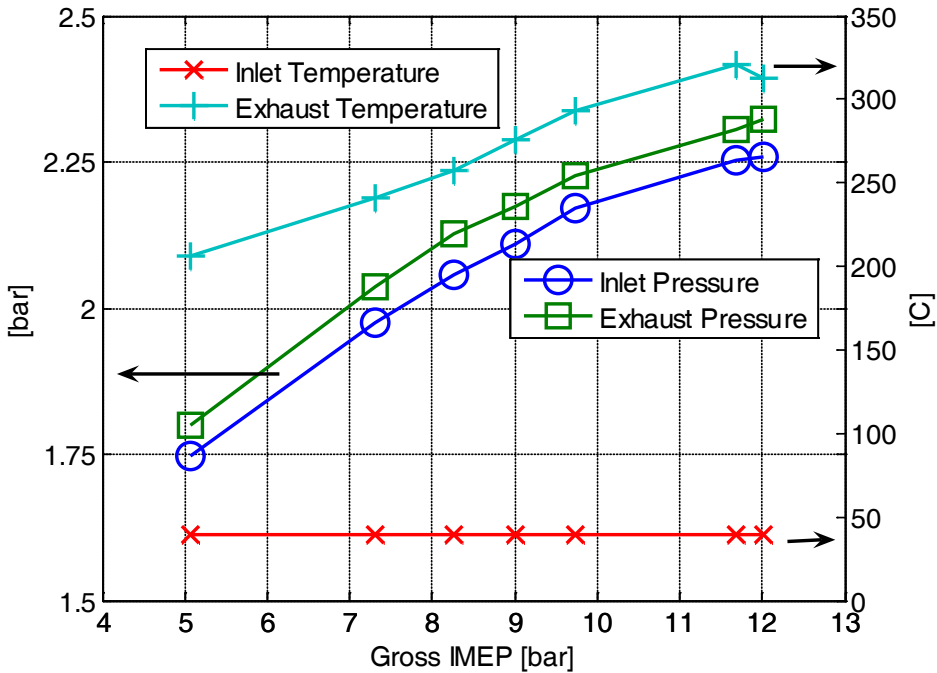
$T_{in} = 308$ [K]



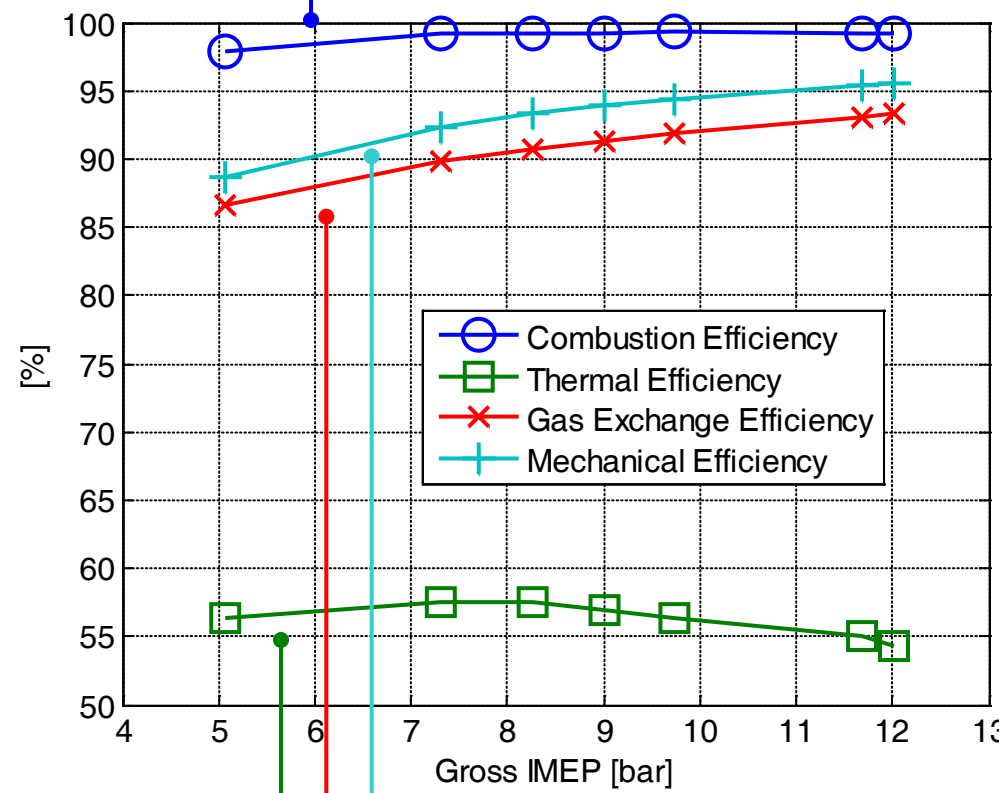
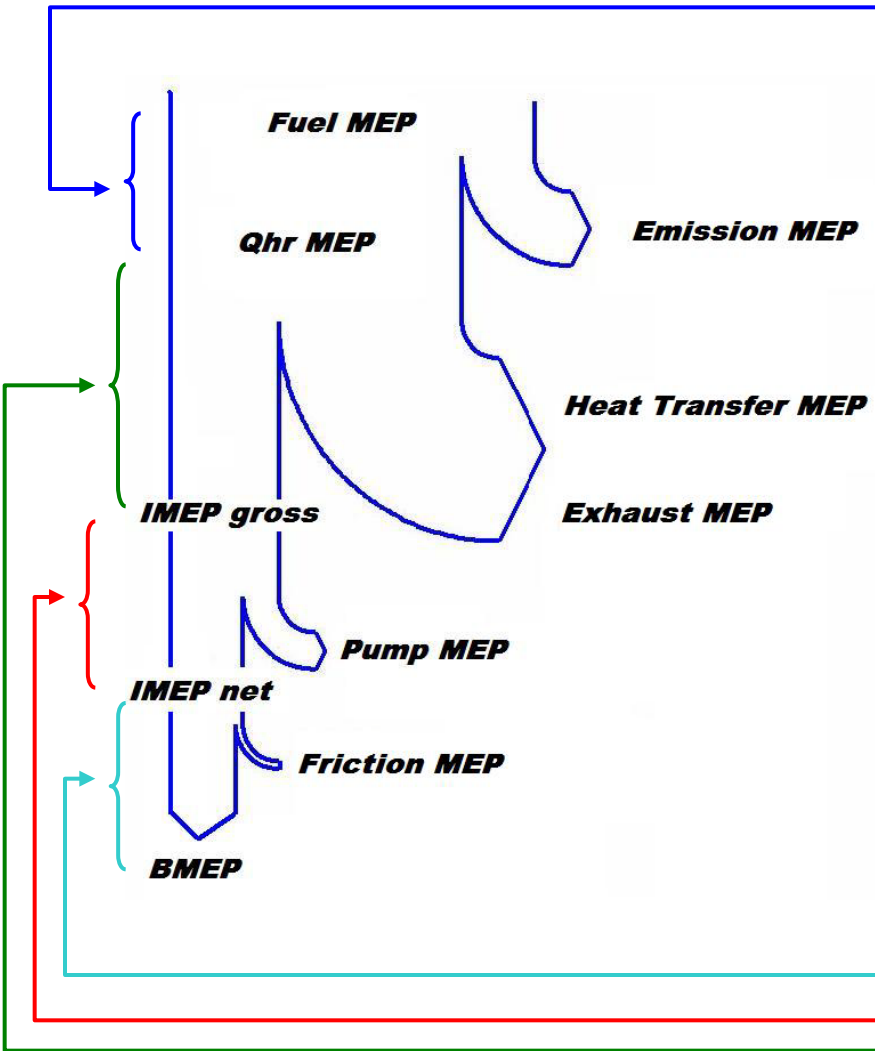
Standard piston bowl, rc: 17:1



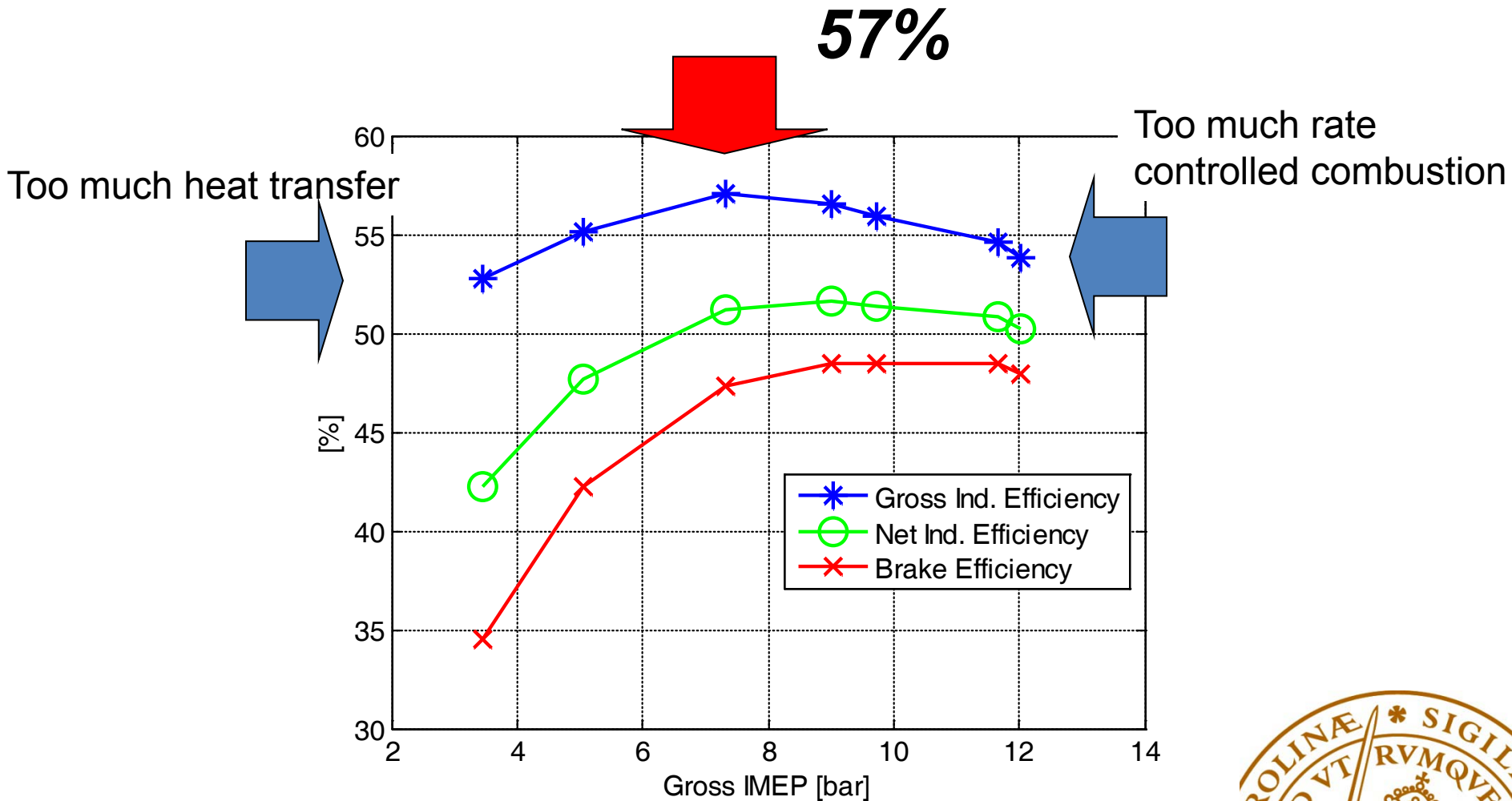
Running Conditions



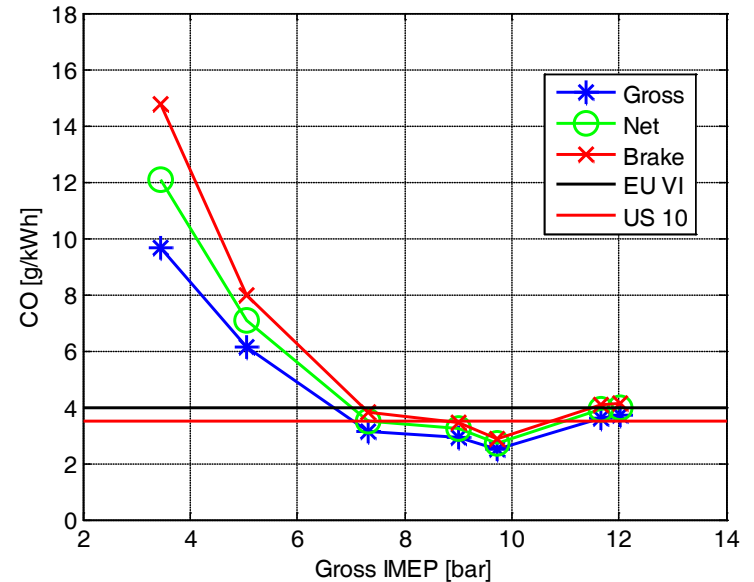
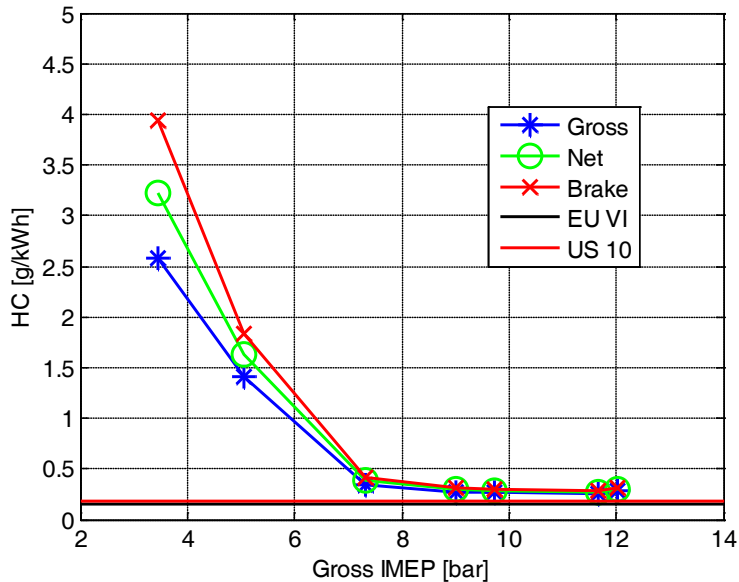
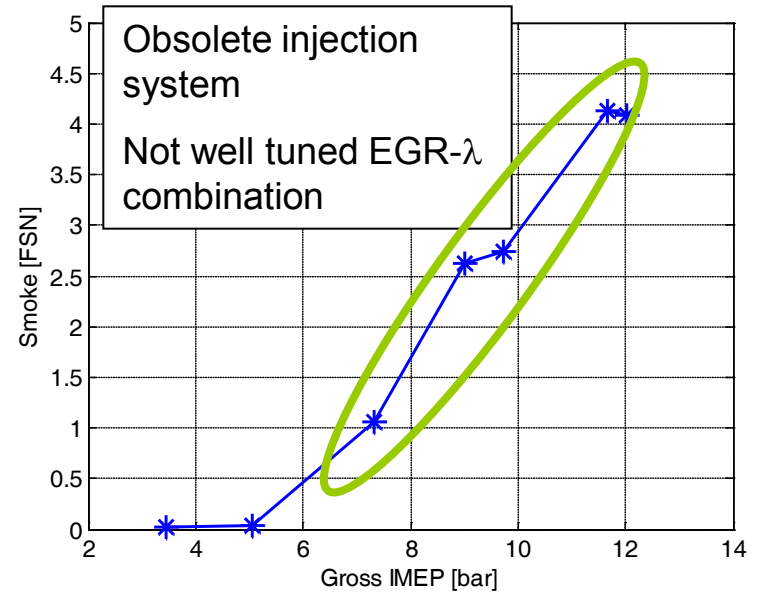
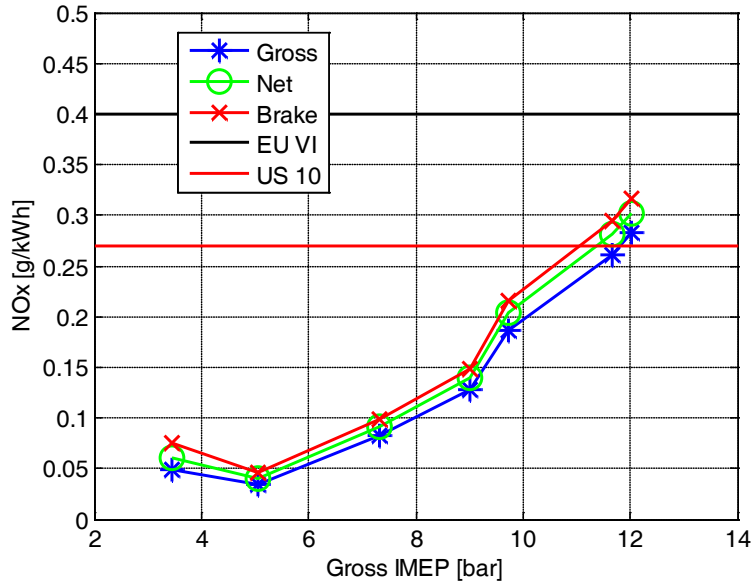
Efficiencies



Efficiency



Emissions

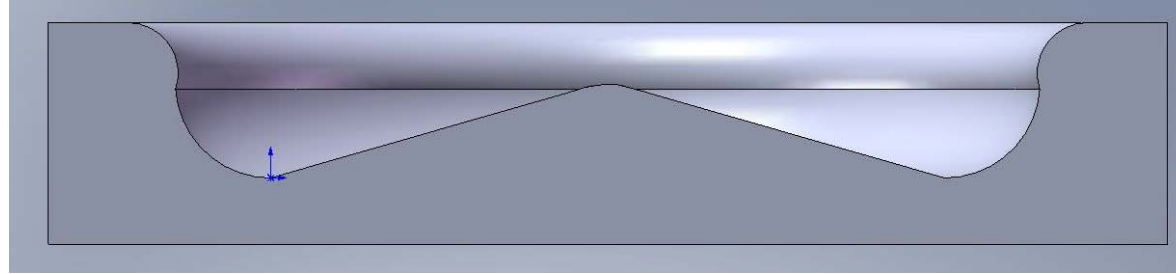


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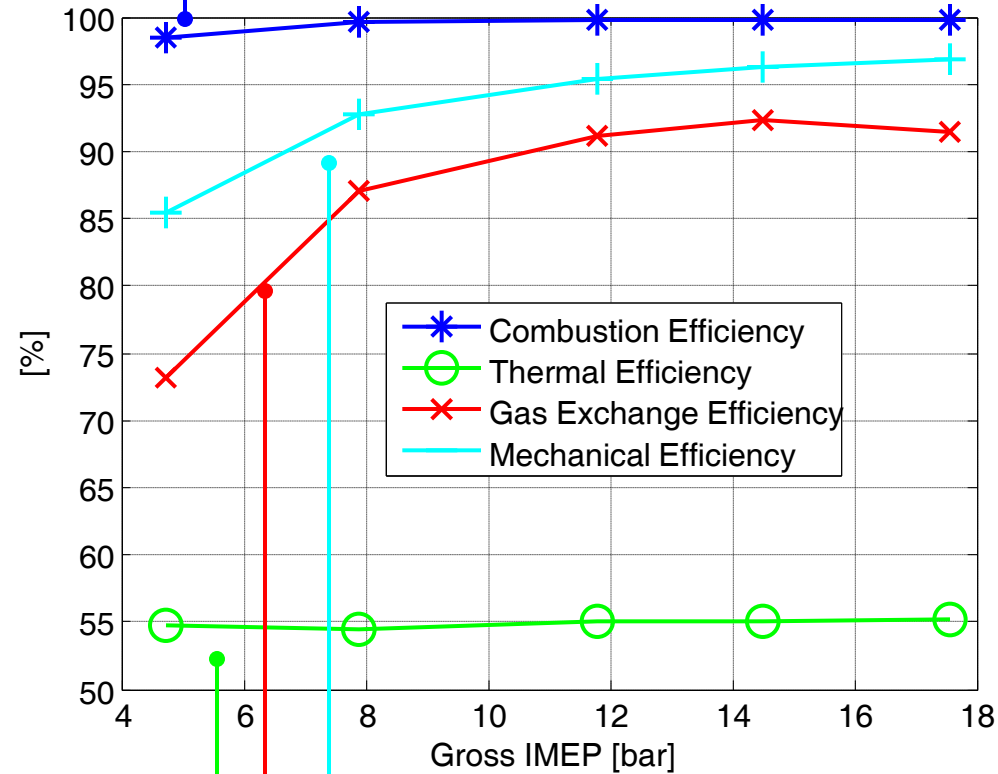
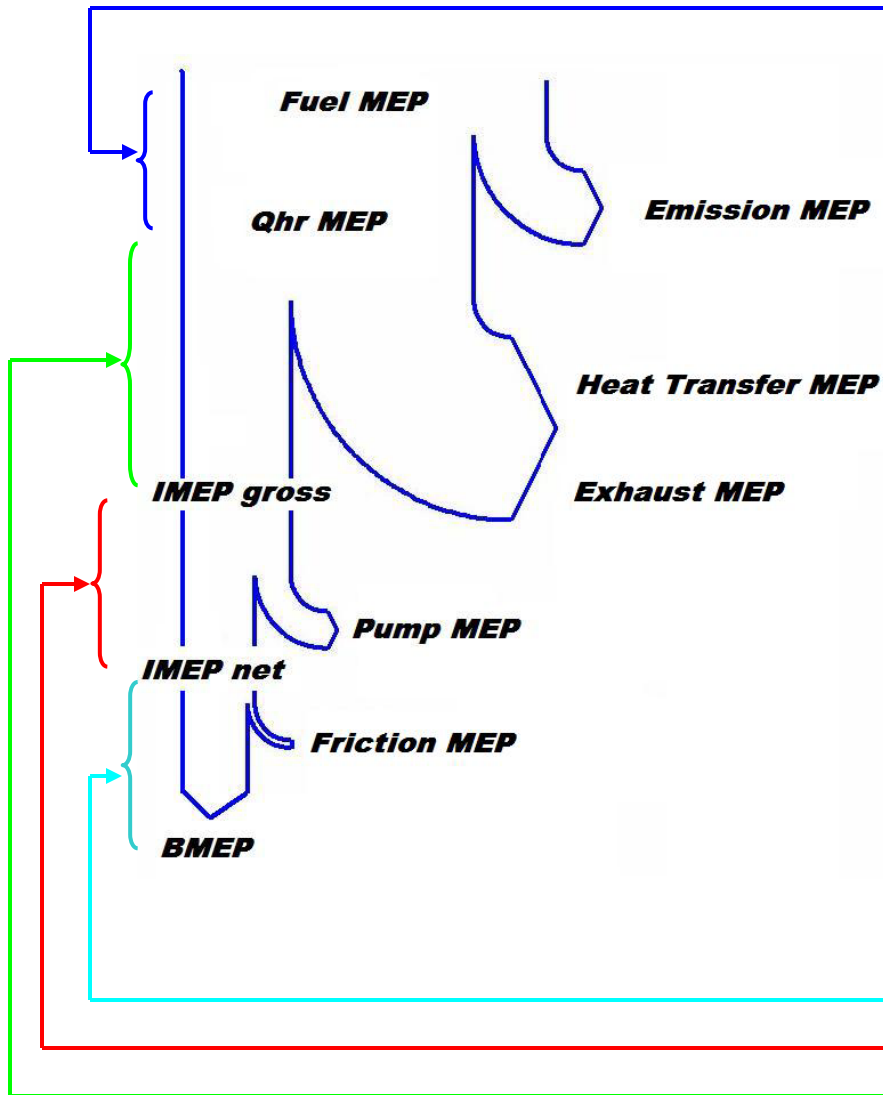
$T_{in} = 308$ [K]



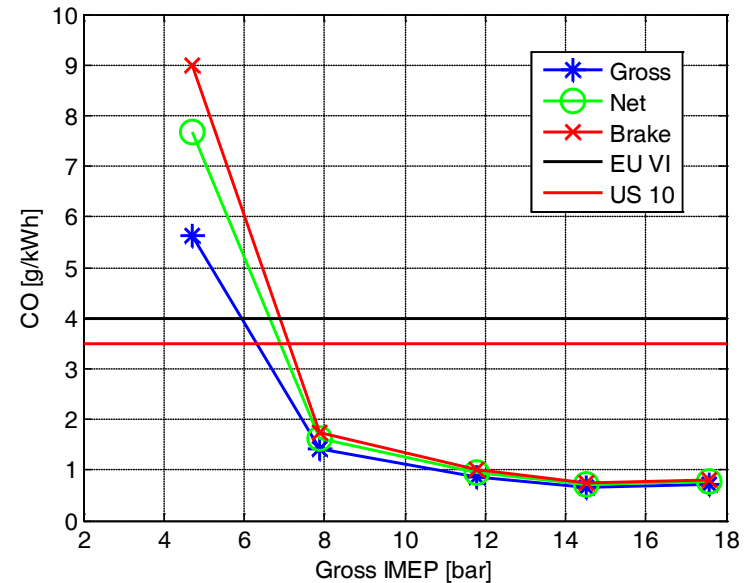
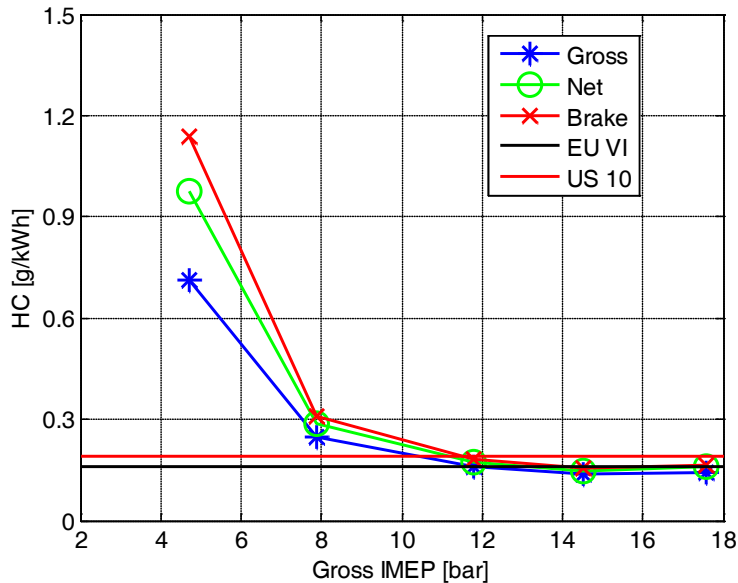
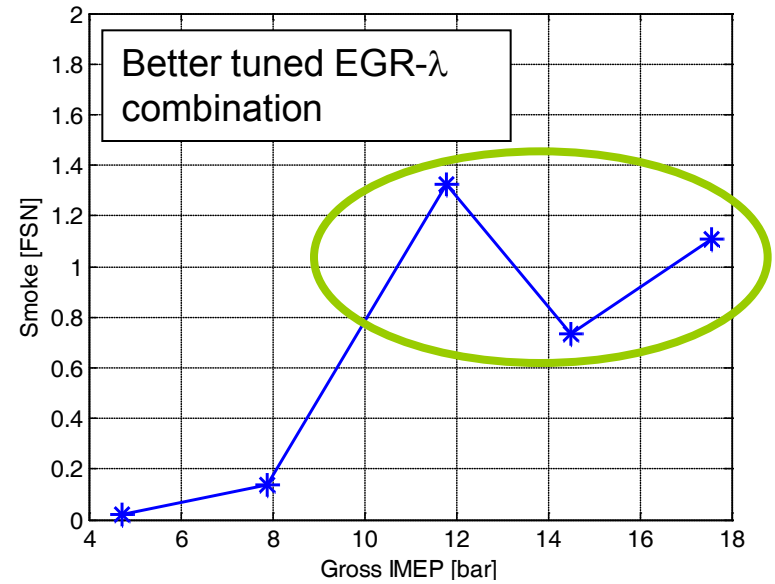
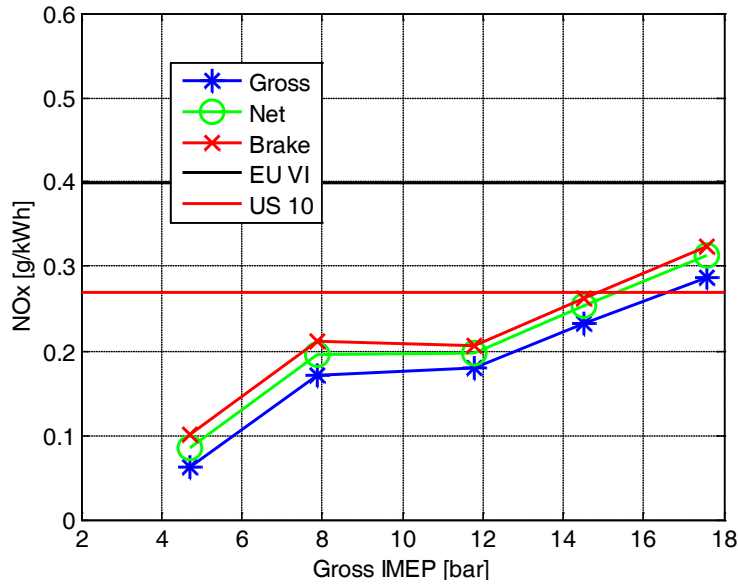
Custom piston bowl, rc: 14.3:1



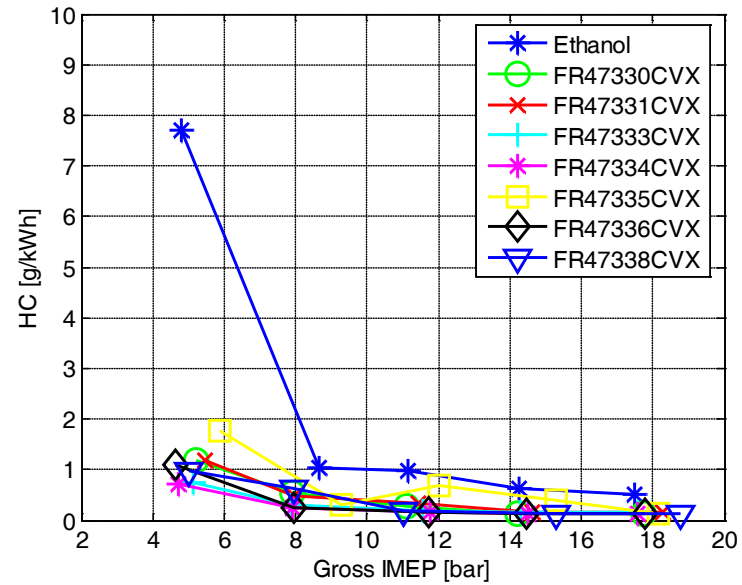
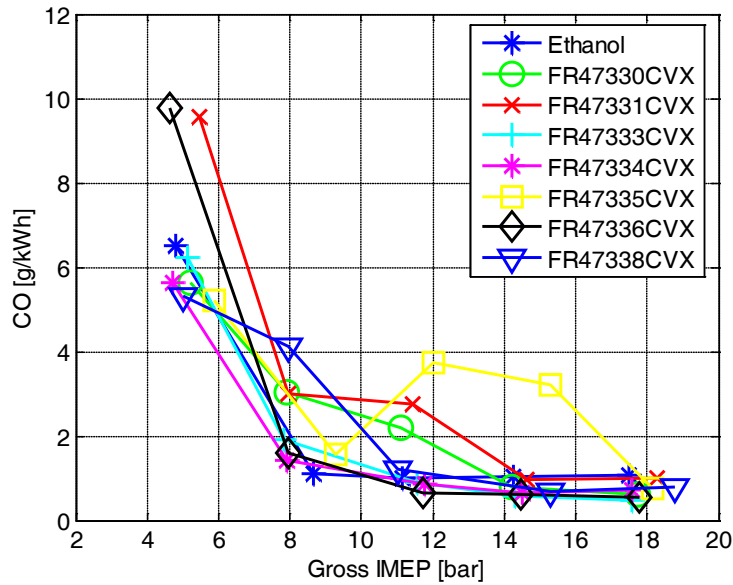
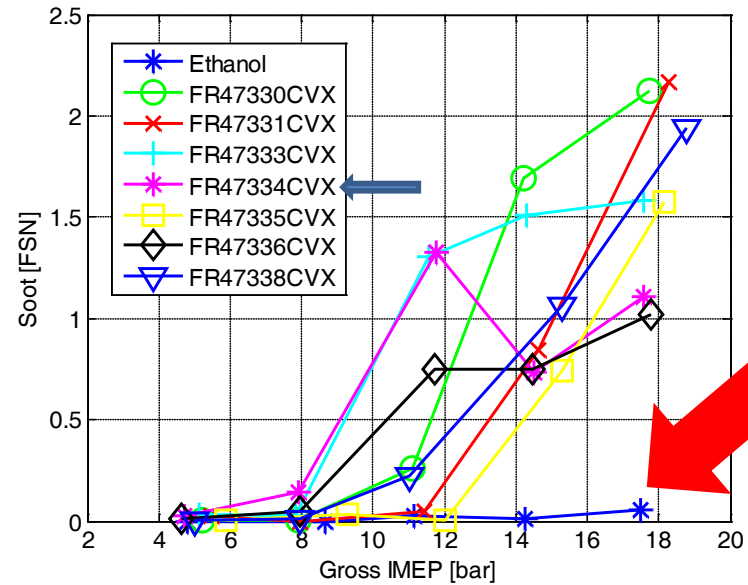
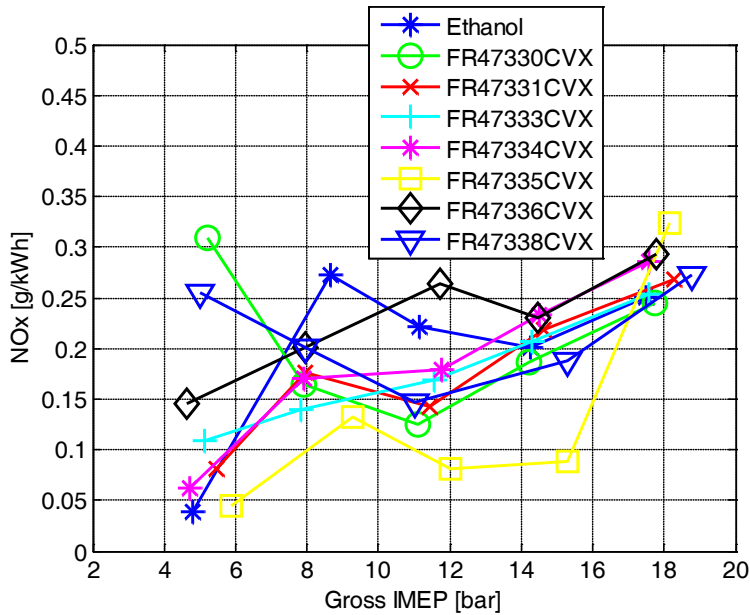
Efficiencies



Emissions



Emissions – different fuels

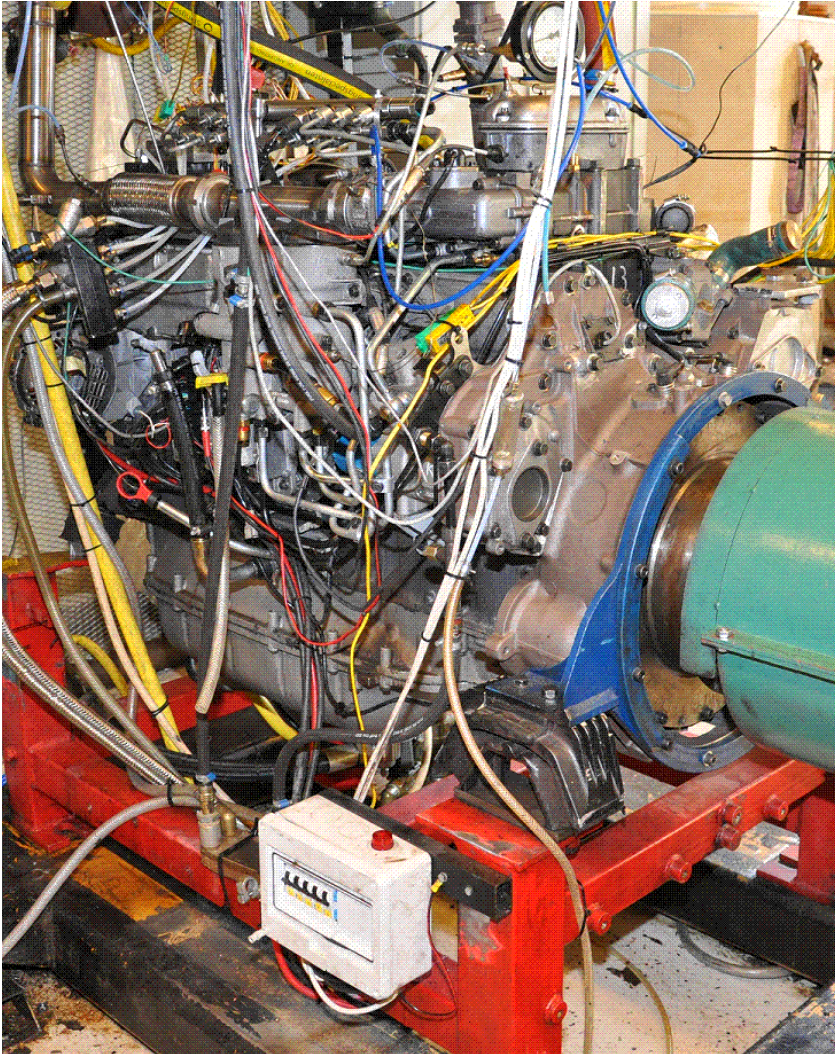


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Experimental Apparatus, Scania D13



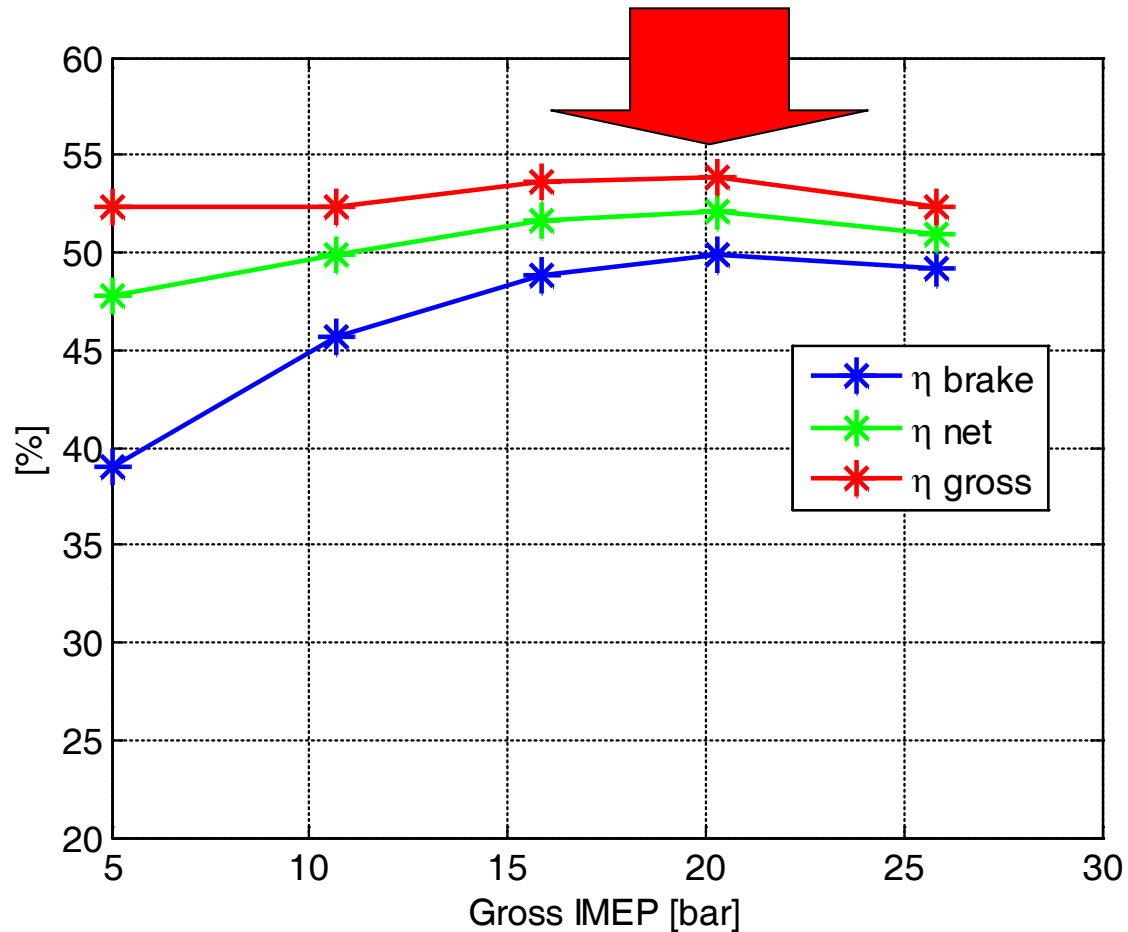
XPI Common Rail		
Orifices	8	[-]
Orifice Diameter	0.19	[mm]
Umbrella Angle	148	[deg]
Engine / Dyno Spec		
BMEPmax	25	[bar]
Vd	2124	[cm ³]
Swirl ratio	2.095	[-]



Standard piston bowl, rc: 17.3:1

Efficiency

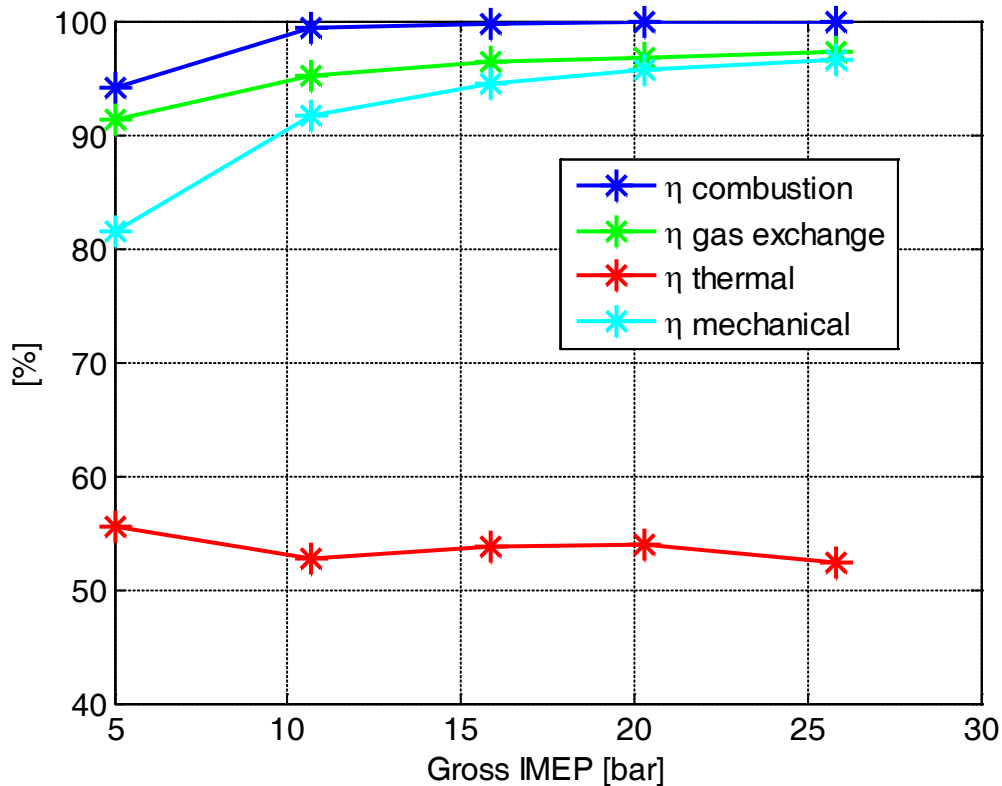
50% brake efficiency seems viable!!!



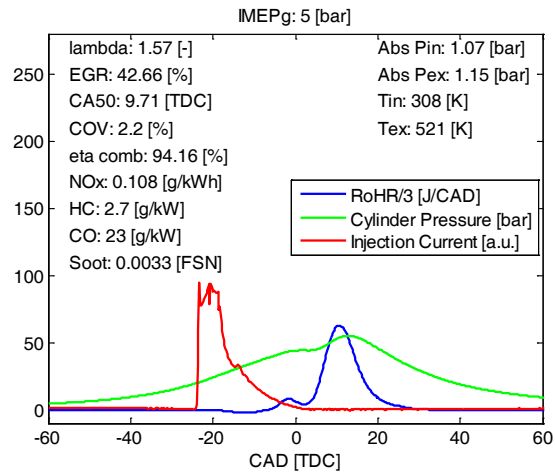
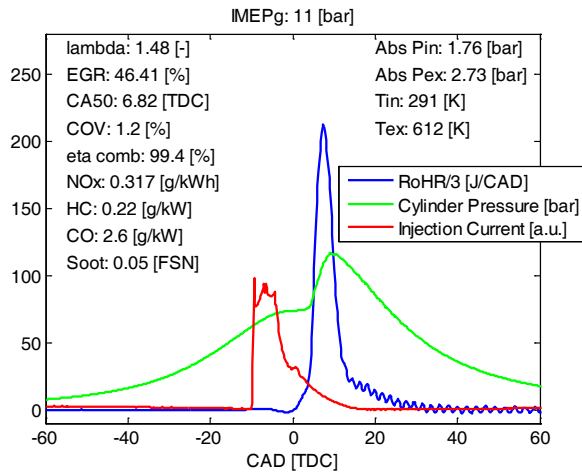
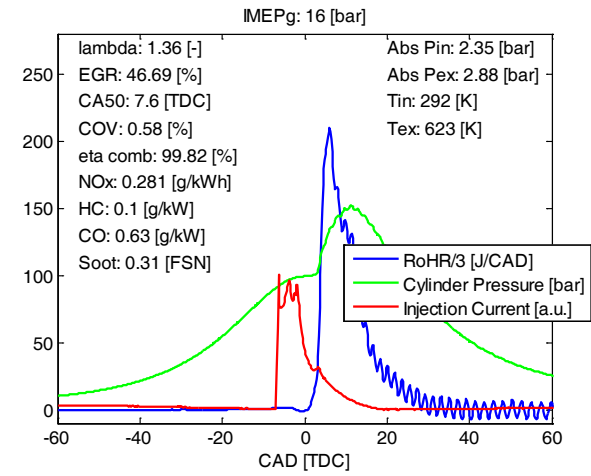
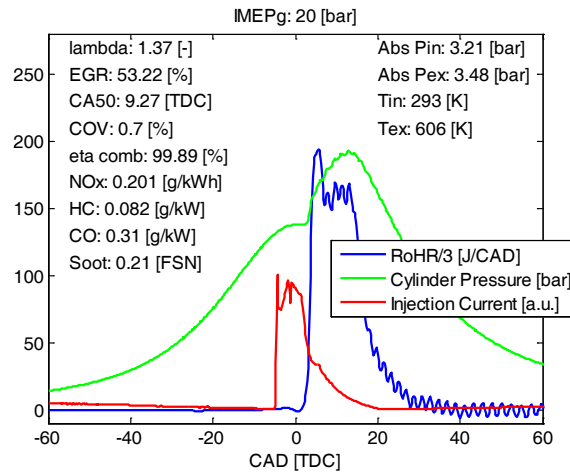
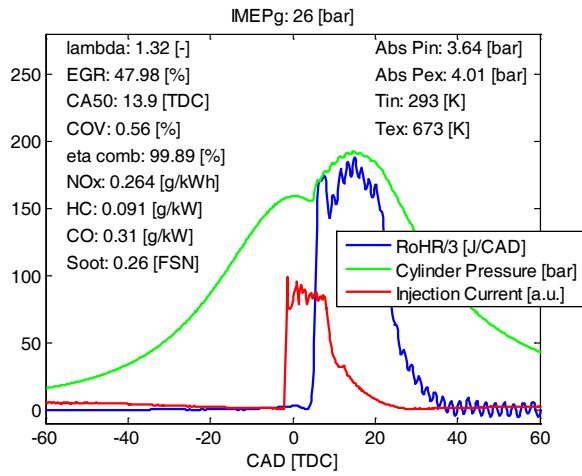
Efficiency

50% brake efficiency \rightarrow maximization of all intermediate efficiencies

$$\eta_{Brake} = \eta_{Combustion} \cdot \eta_{Thermodynamic} \cdot \eta_{GasExchange} \cdot \eta_{Mechanical}$$

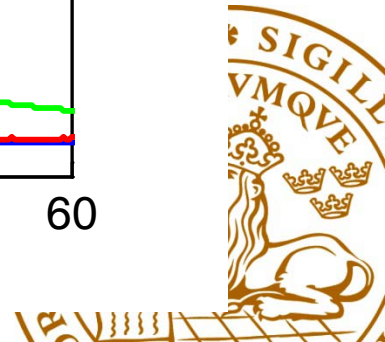
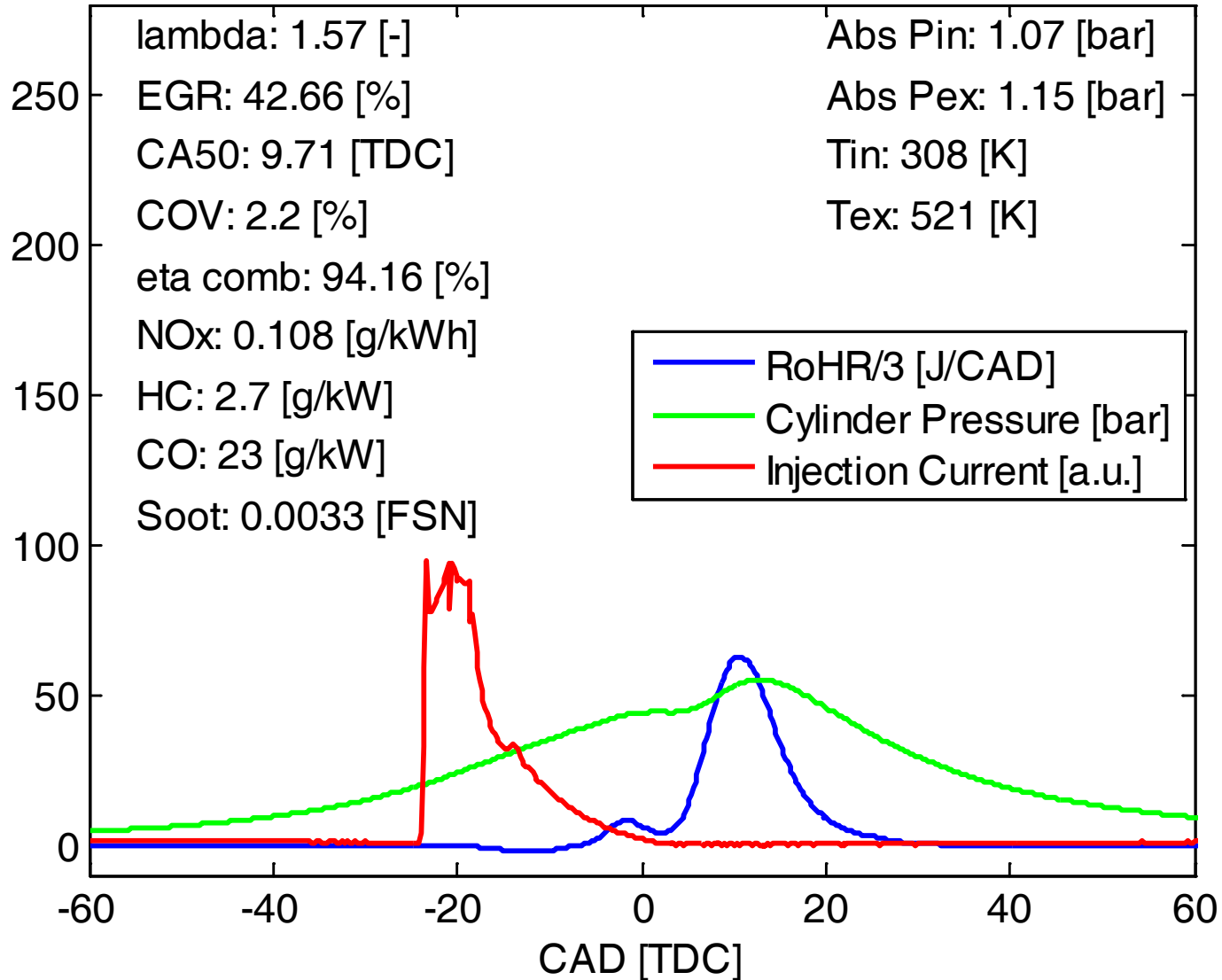


RoHR, Cylinder Pressure & Injection Signal

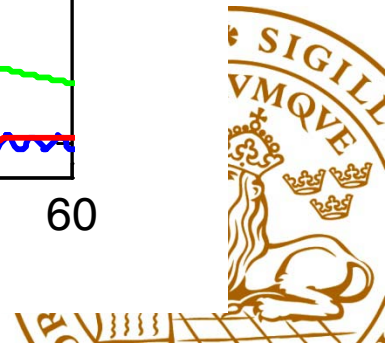
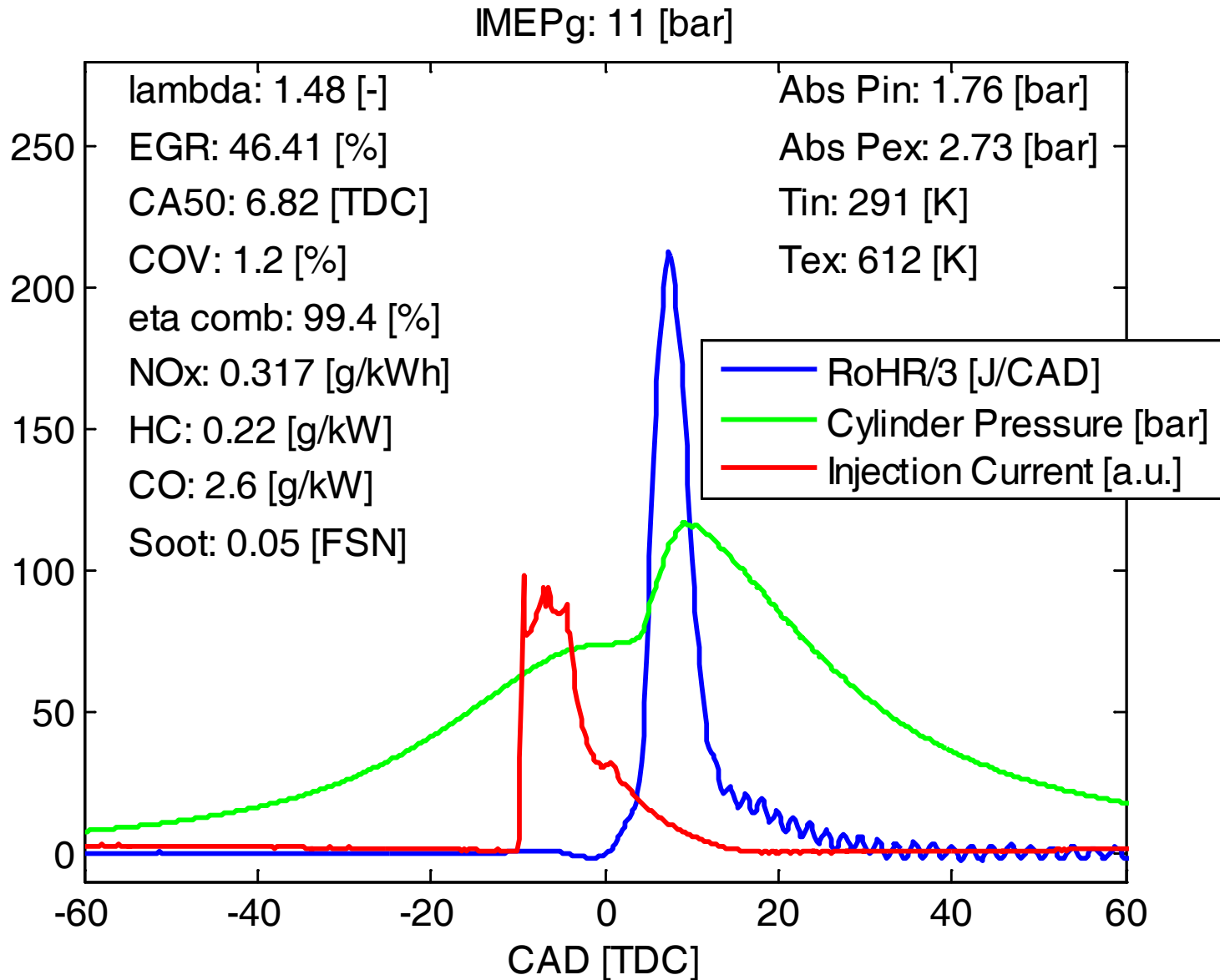


RoHR, Cylinder Pressure & Injection Signal

IMEPg: 5 [bar]

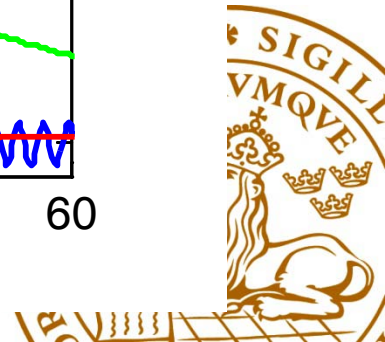
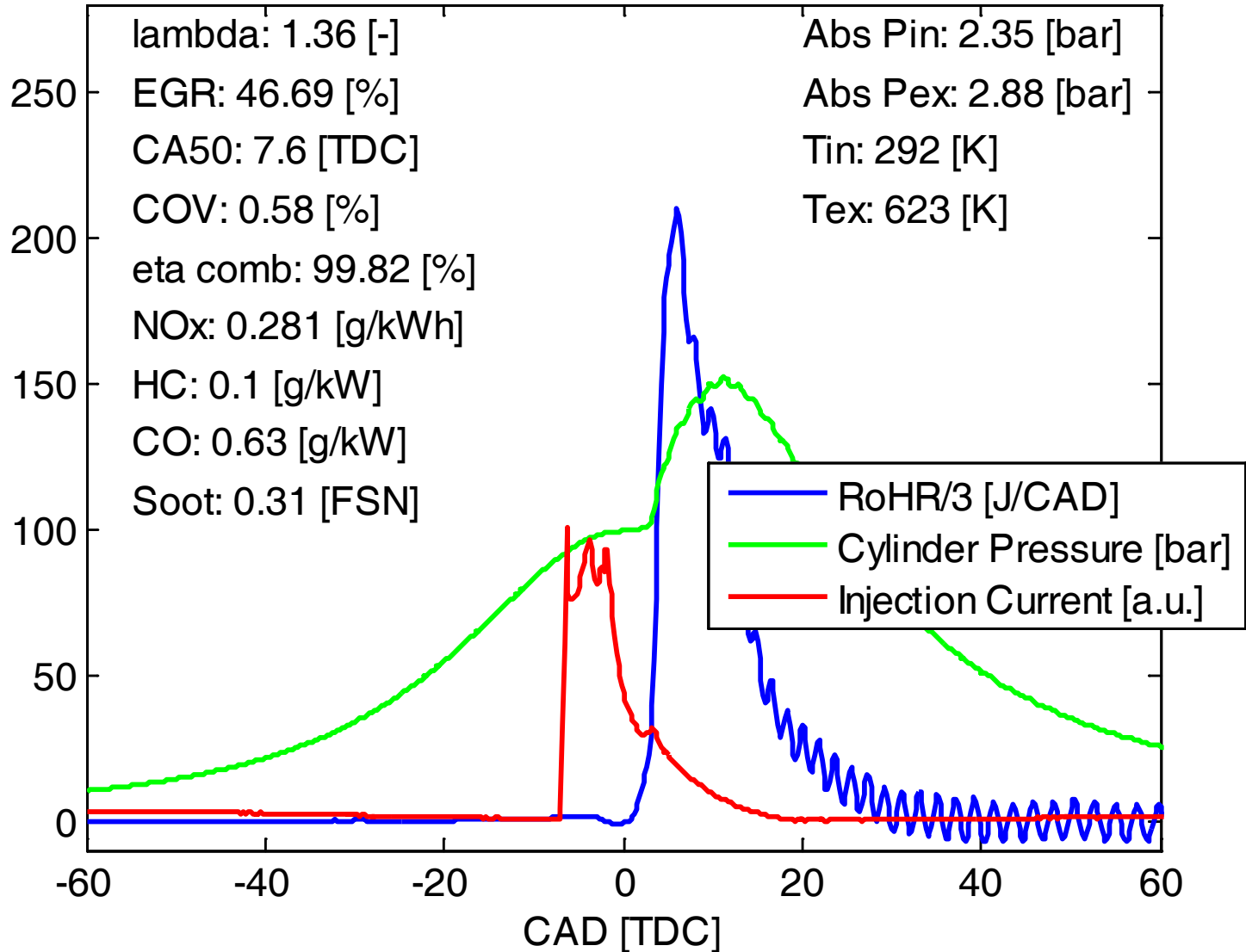


RoHR, Cylinder Pressure & Injection Signal

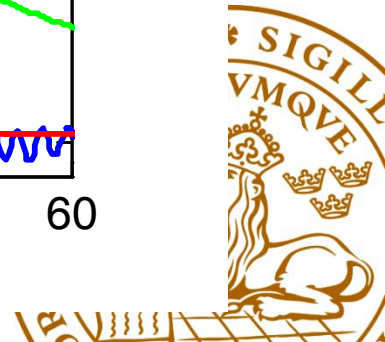
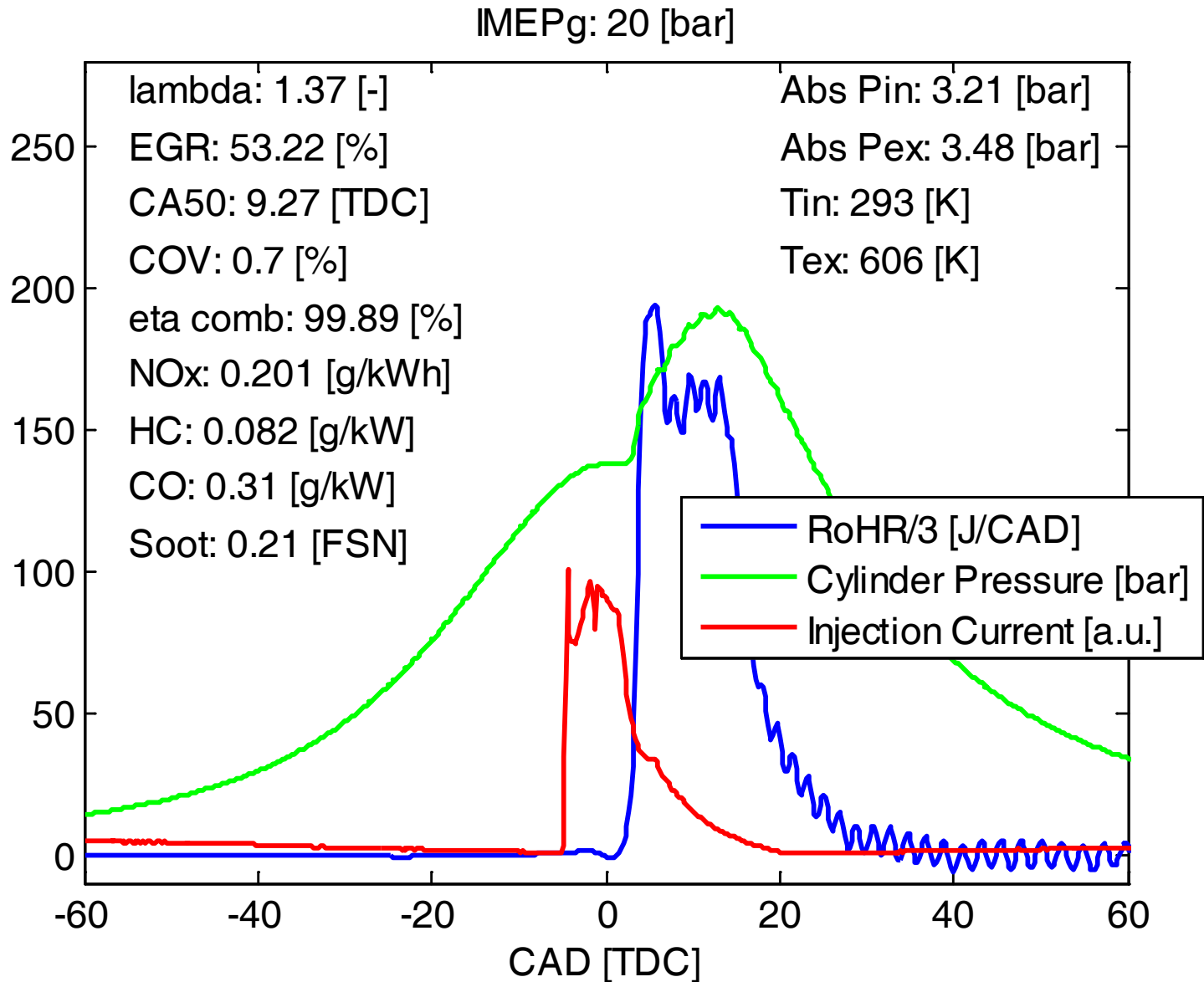


RoHR, Cylinder Pressure & Injection Signal

IMEPg: 16 [bar]

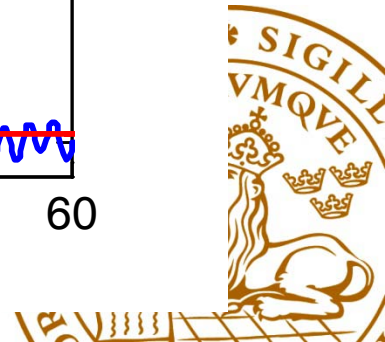
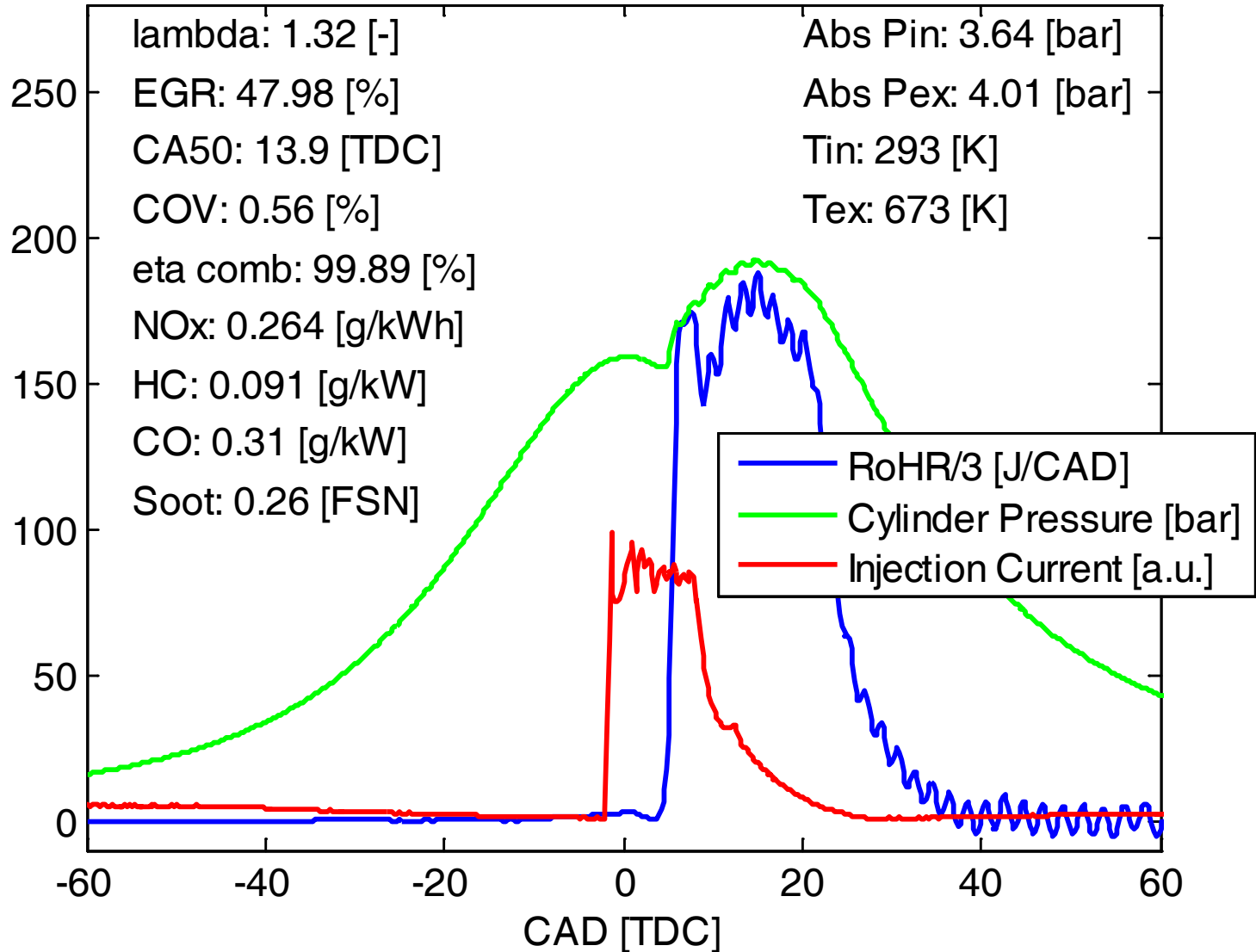


RoHR, Cylinder Pressure & Injection Signal

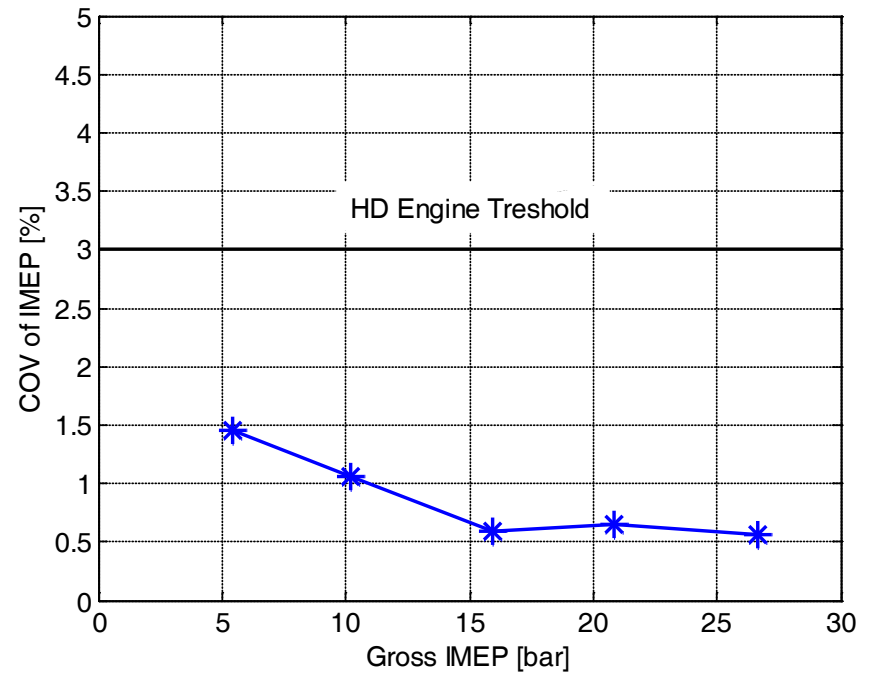
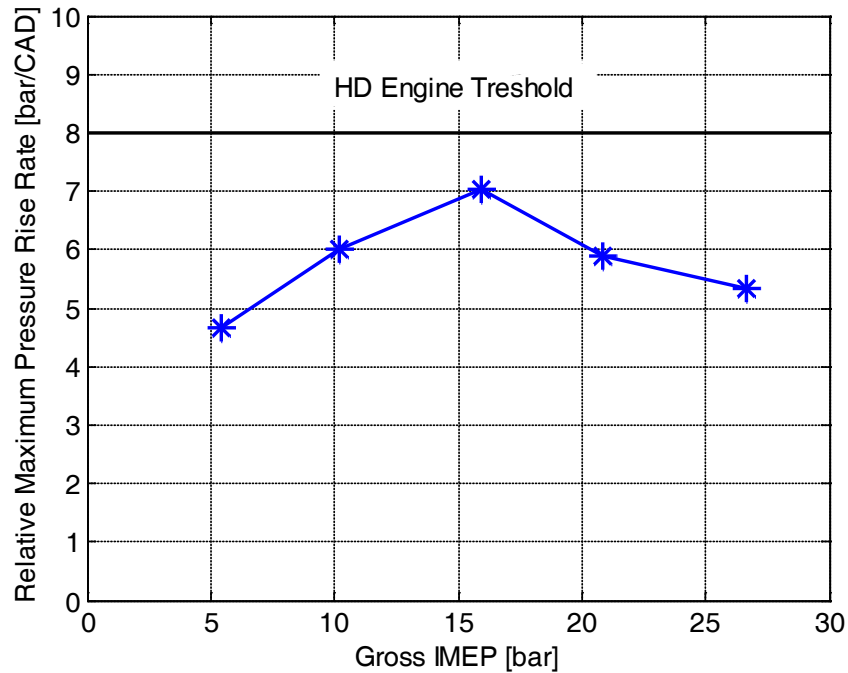


RoHR, Cylinder Pressure & Injection Signal

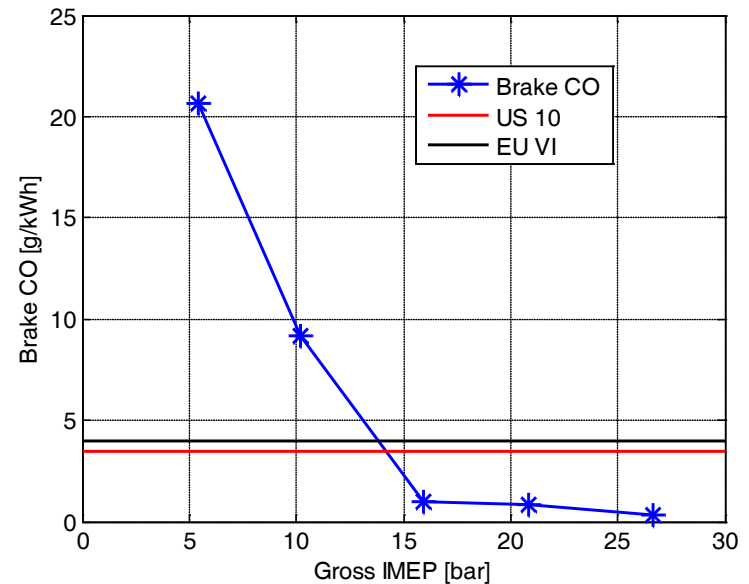
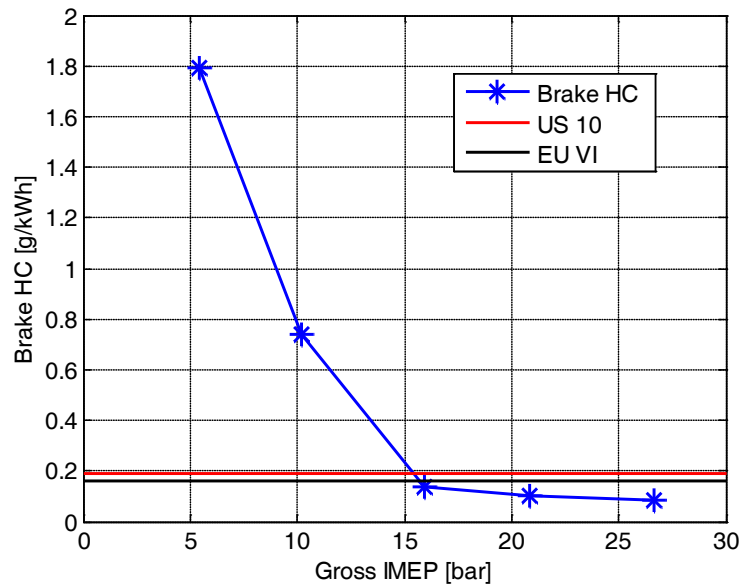
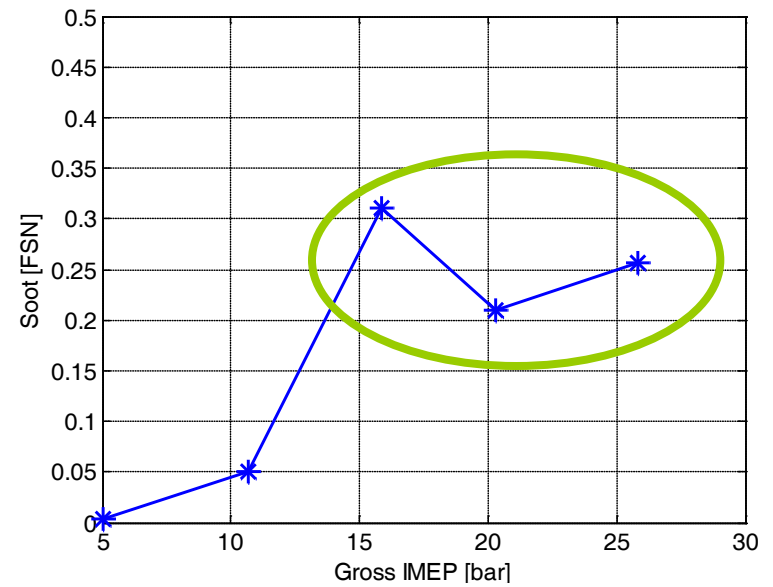
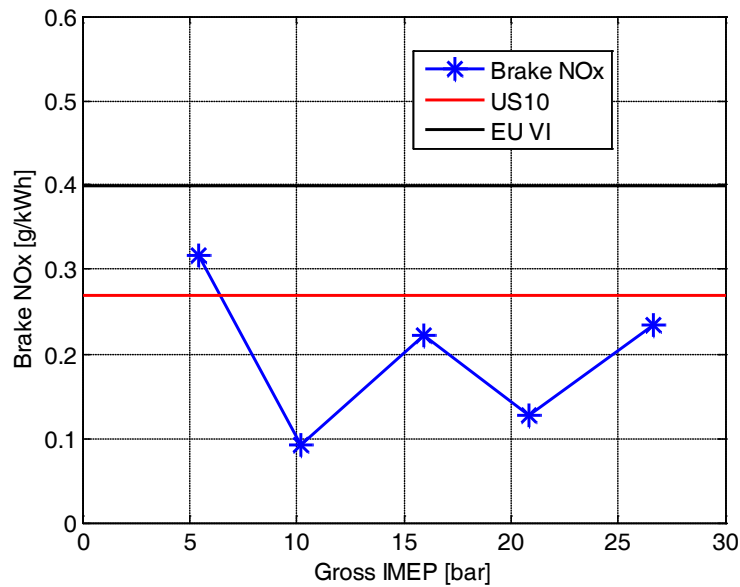
IMEPg: 26 [bar]



Combustion Noise & Stability



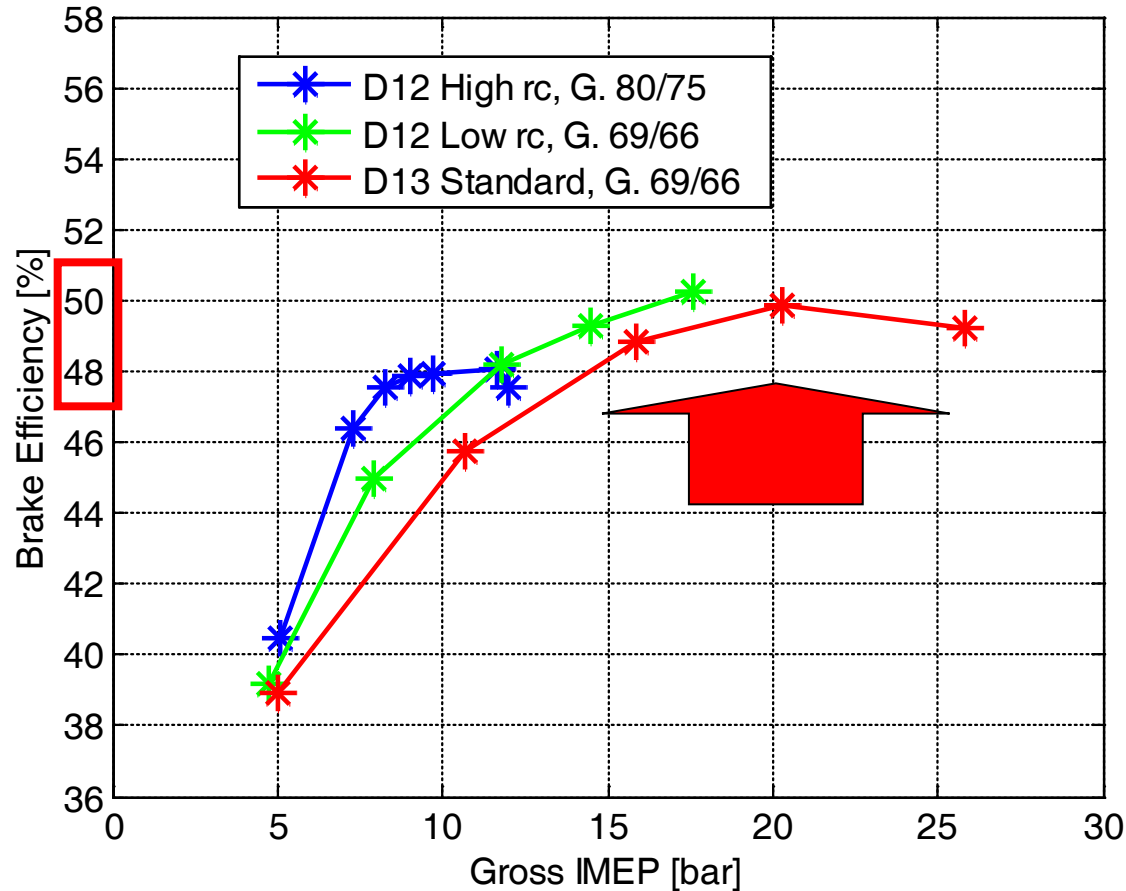
Emissions



Summary



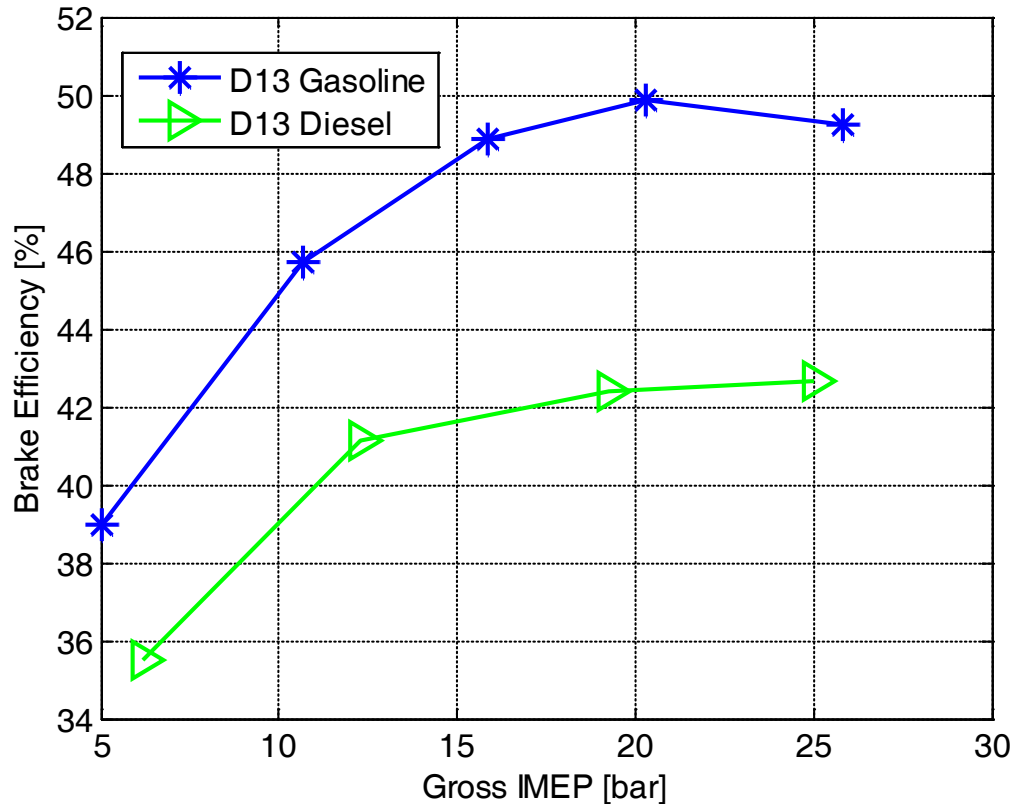
Brake Efficiency



Brake efficiency in the range of 48-50% seems to be viable between 12.5 and 26 bar gross IMEP.



D13 Running on Diesel & Gasoline

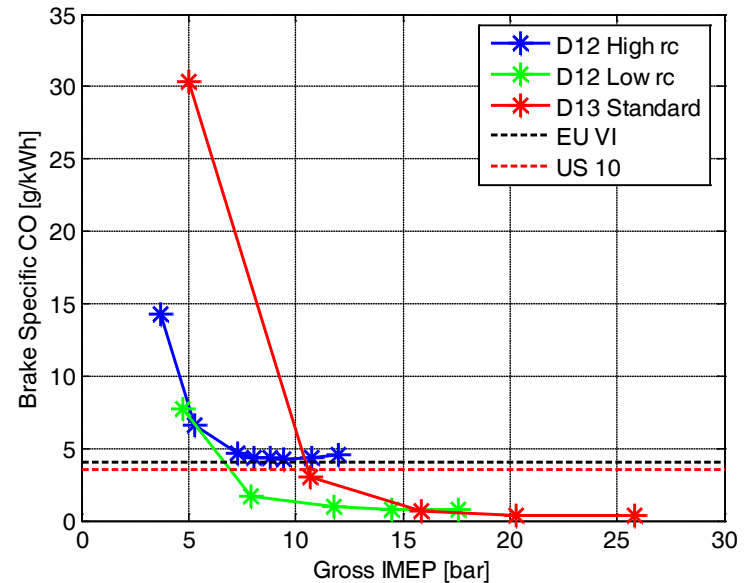
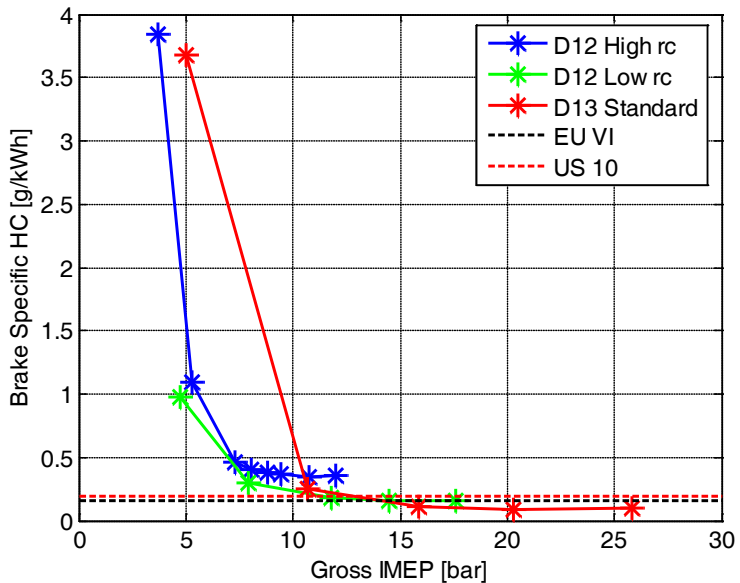
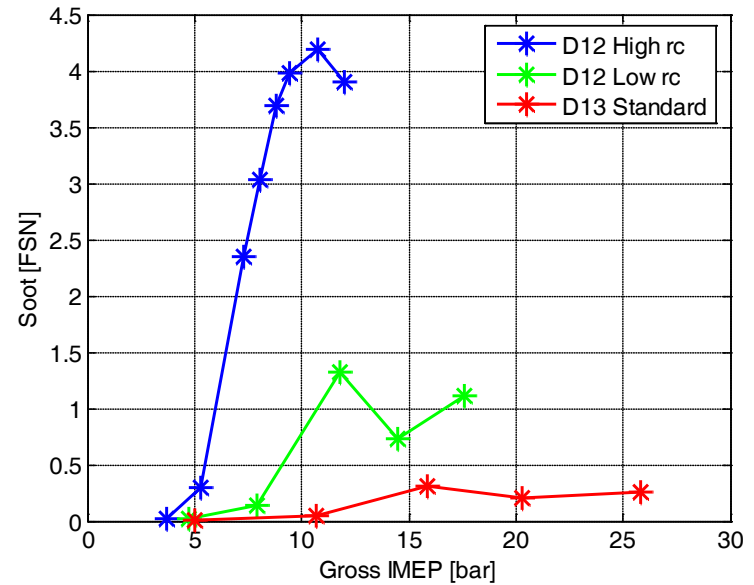
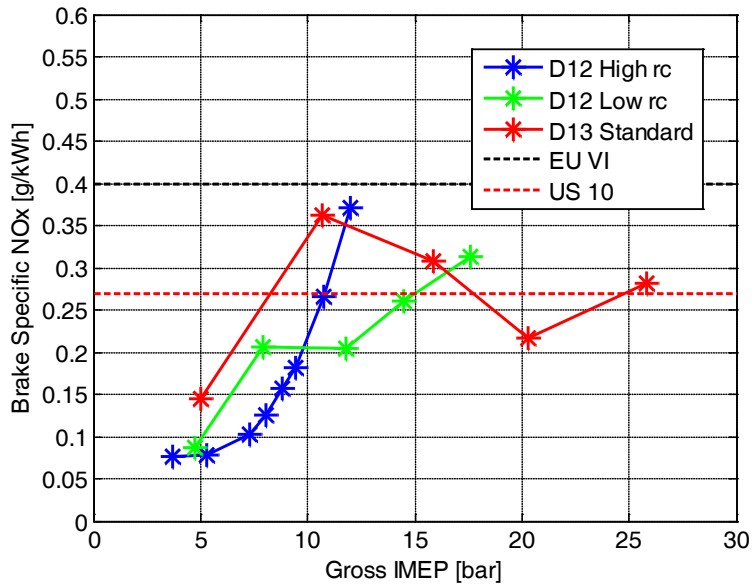


D13 Diesel was calibrated by Scania and the calibration was done to meet EU V legislation.

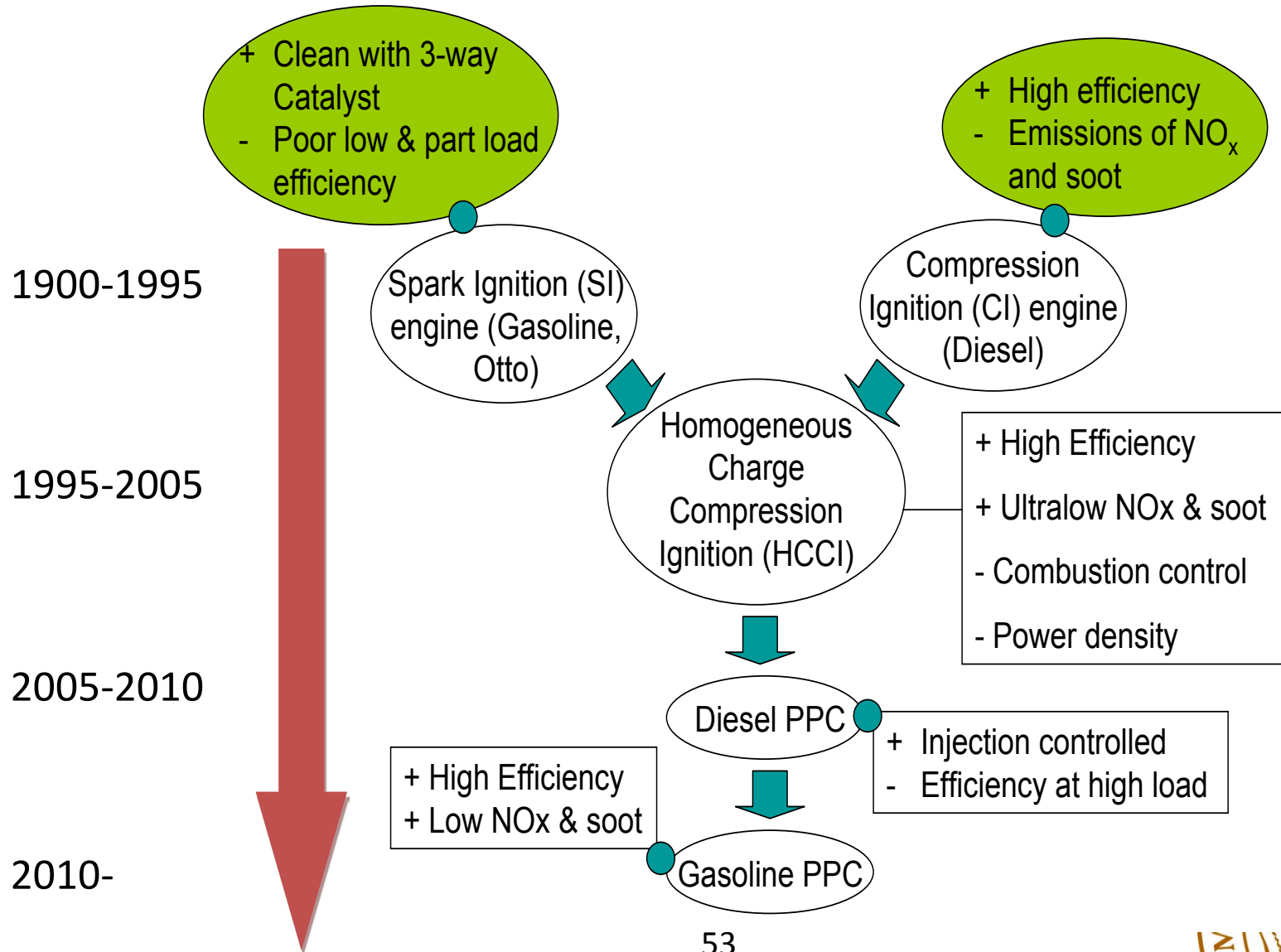
Average improvement of 16.6% points @ high load!!!



Brake Emissions



Engine combustion - direction



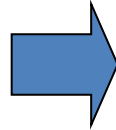
The End

Thank you

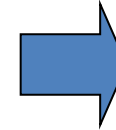


Path to High Efficiency Gasoline Engine

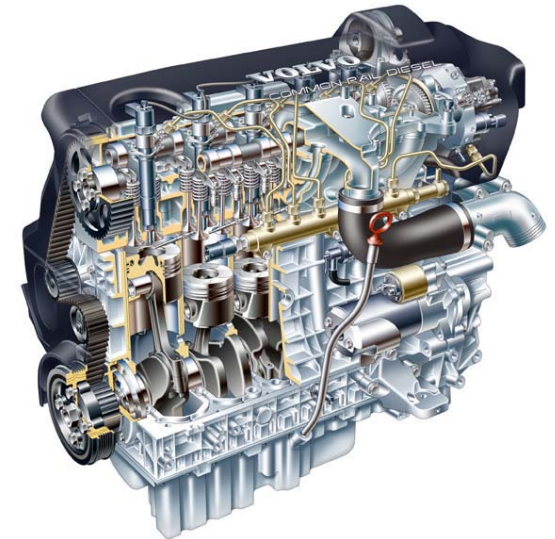
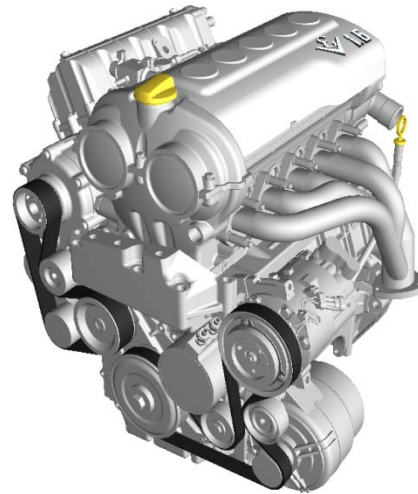
SI



HCCI



PPC



Prof. Bengt Johansson

Division of Combustion Engines
Department of Energy Sciences

Lund University

Outline

- Partially premixed combustion, PPC
 - Summary of
 - 56% thermal efficiency in car size engine
 - 57% thermal efficiency in truck size engine
 - Why 55% thermal efficiency is better than 57%
 - Fuel effects in Scania D12 engine
 - How to reach 26 bar IMEP with US10
NO_x, PM, HC and CO engine out, Scania D13
 - Fuel effects in Scania D13 engine



Fuel Matrix

		RON	MON	C	H/C	O/C	LHV [MJ/kg]	A/F stoich
Group 1	FR47335CVX	99.0	96.9	7.04	2.28	0.00	44.30	15.10
	FR47332CVX	97.7	87.5	6.61	2.06	0.07	39.70	13.44
	FR47337CVX	96.5	86.1	7.53	1.53	0.00	42.10	14.03
Group 2	FR47338CVX	88.6	79.5	7.21	1.88	0.00	43.50	14.53
	FR47330CVX	87.1	80.5	7.20	1.92	0.00	43.50	14.60
	FR47331CVX	92.9	84.7	6.90	1.99	0.03	41.60	14.02
Group 3	FR47336CVX	70.3	65.9	7.10	2.08	0.00	43.80	14.83
	FR47334CVX	69.4	66.1	7.11	1.98	0.00	43.80	14.68
	FR47333CVX	80.0	75.0	7.16	1.97	0.00	43.70	14.65
Group 4	PRF20	20	20	7.2	2.28	0	44.51	15.07
	MK1	n.a.	20	16	1.87	0	43.15	14.9

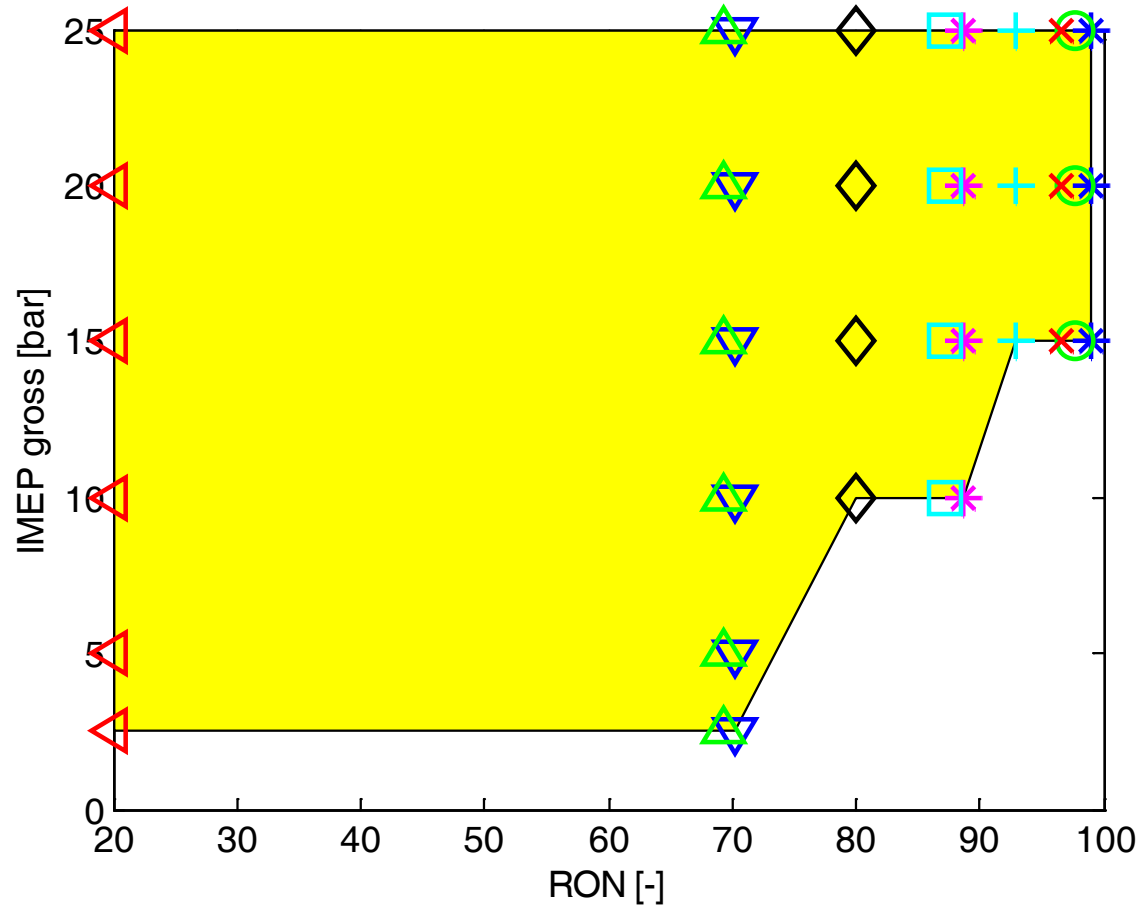


Results

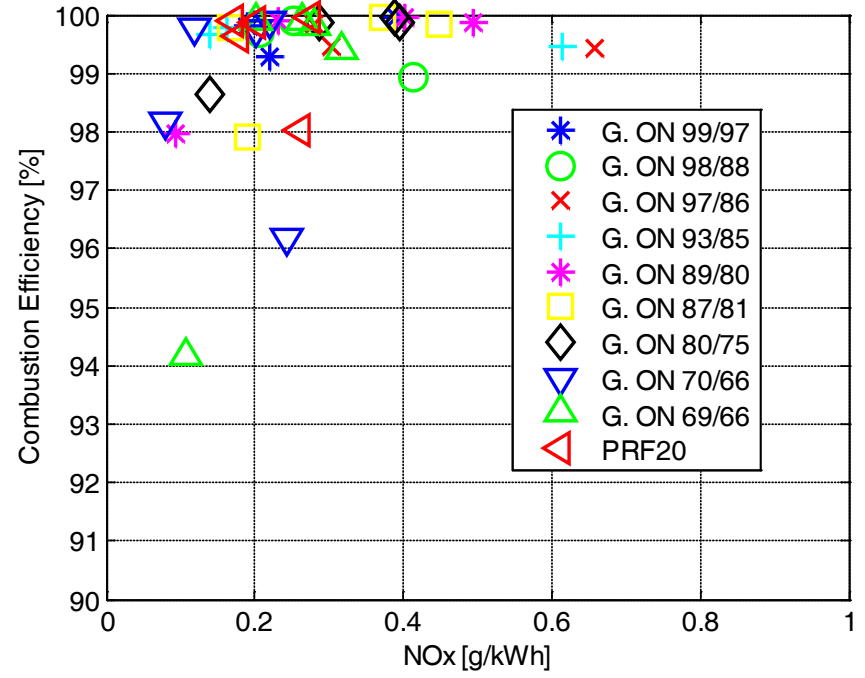
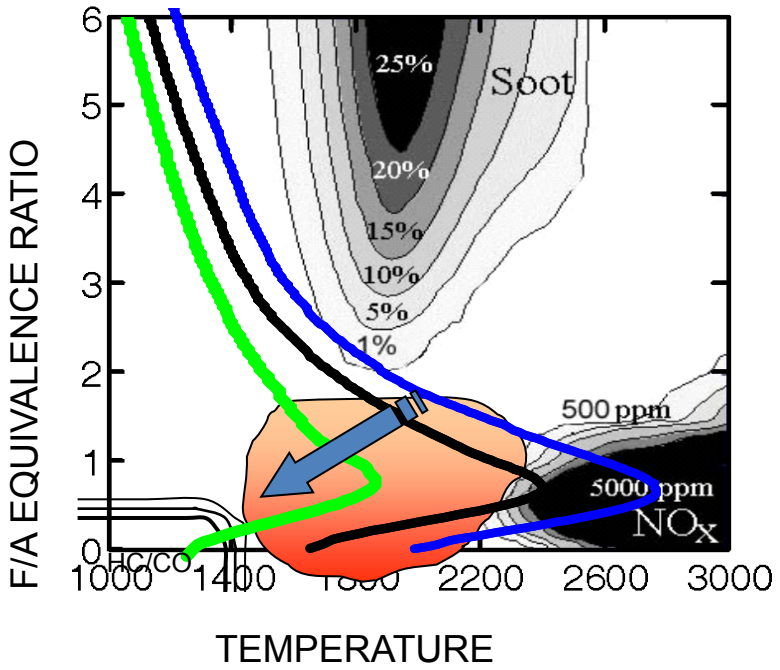


Tested Load Area

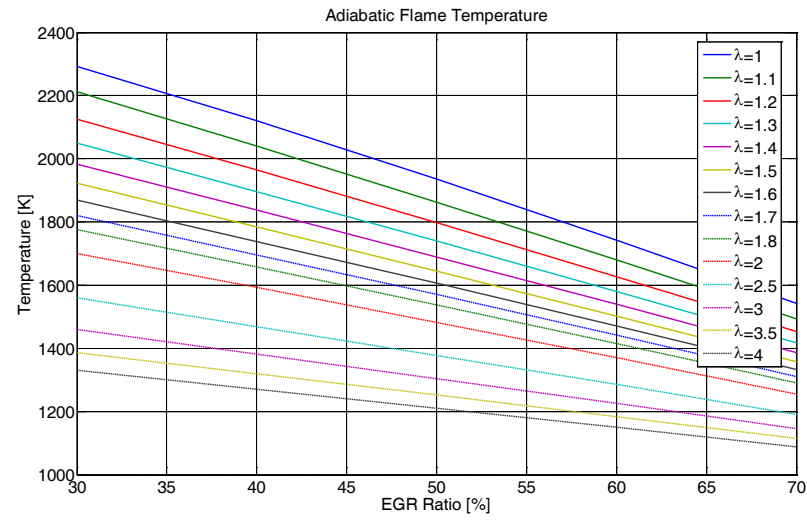
Stable operational load vs. fuel type



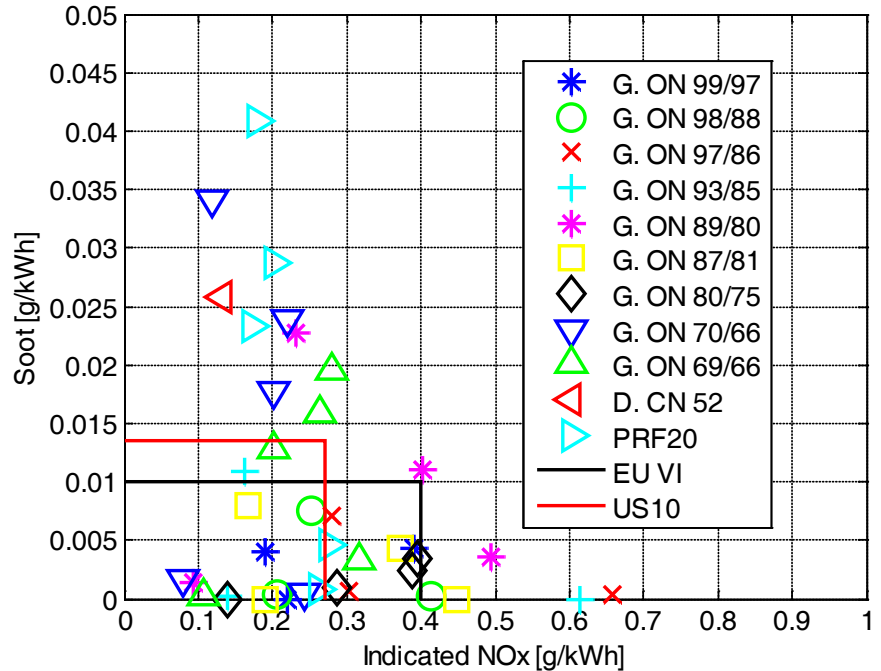
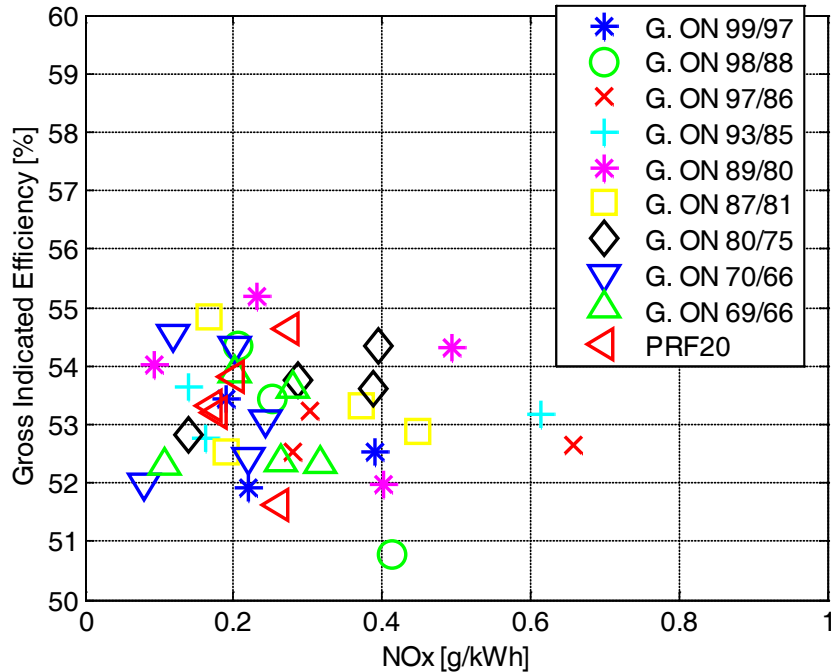
NOx - η_{comb} Trade - Off Solution



It is possible to achieve low NOx and still keep high combustion efficiency in the whole load range!



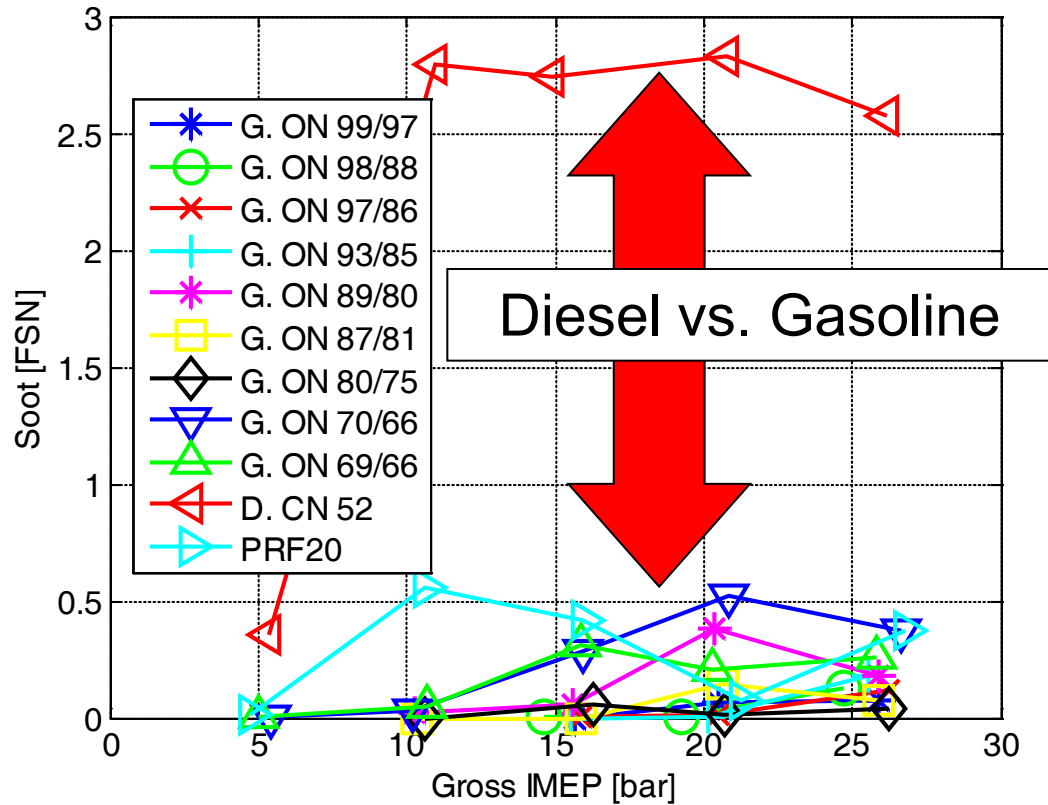
Efficiency & Emissions



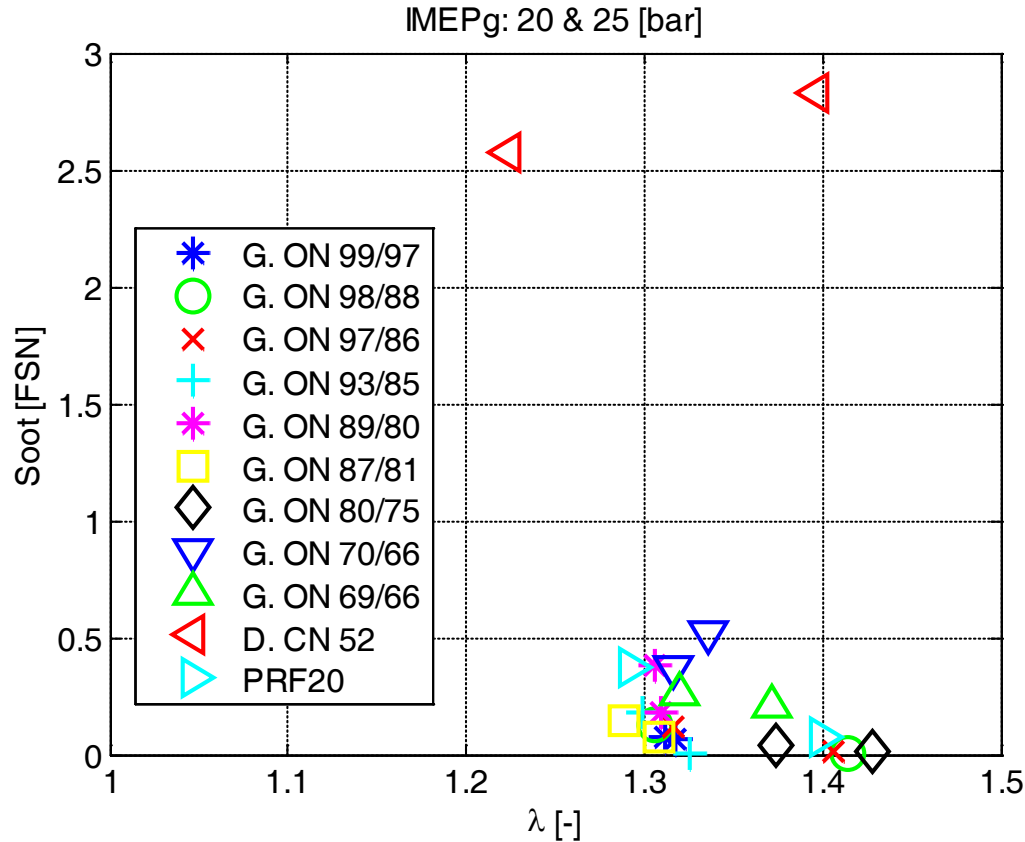
In certain operating range, some fuels are capable to comply EU VI & US10 legislations and still keep high efficiency without compromising the efficiency!



Soot Emissions



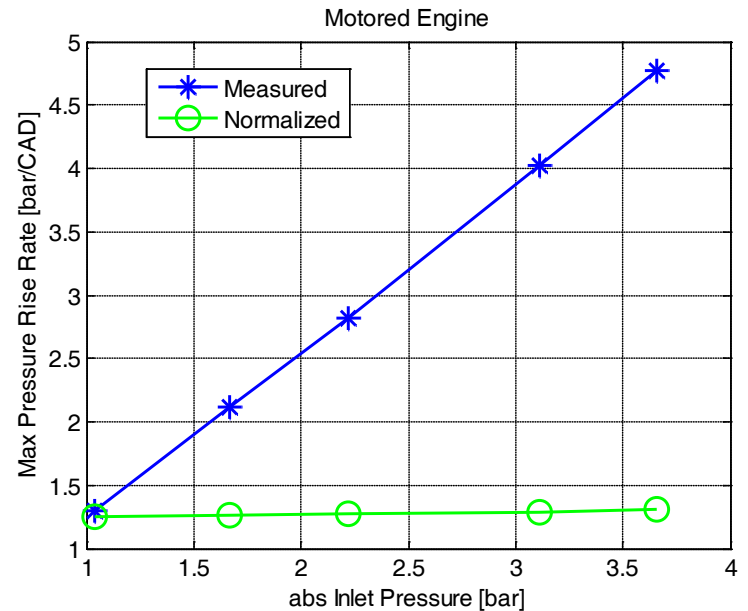
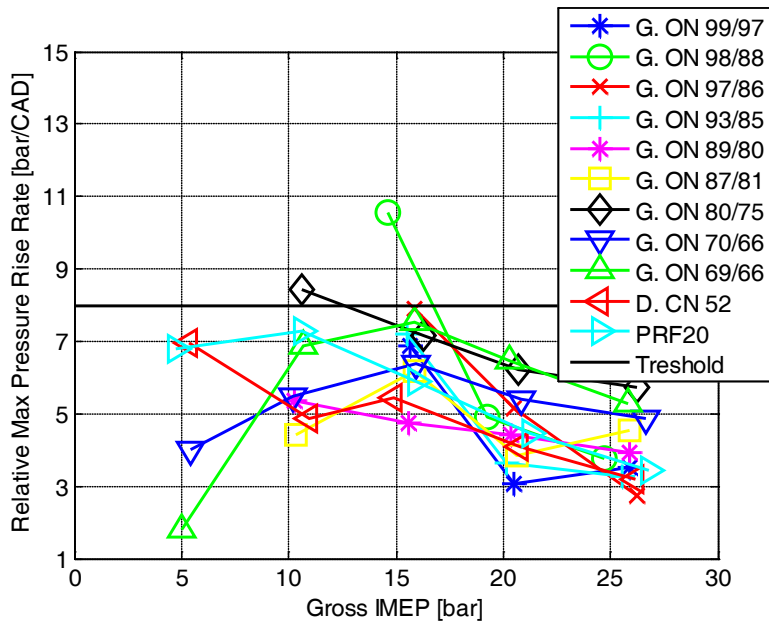
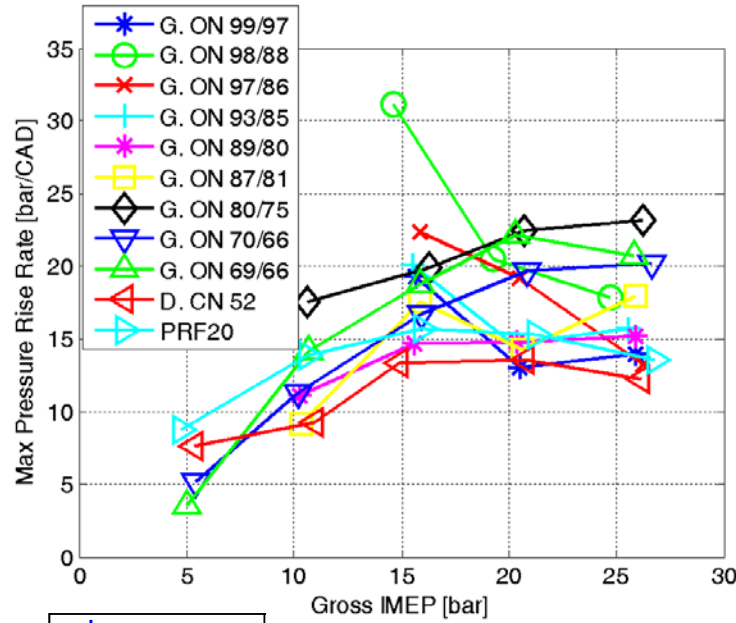
Higher Power Density



Low soot even @ λ 1.3 \rightarrow higher power density without producing smoke!



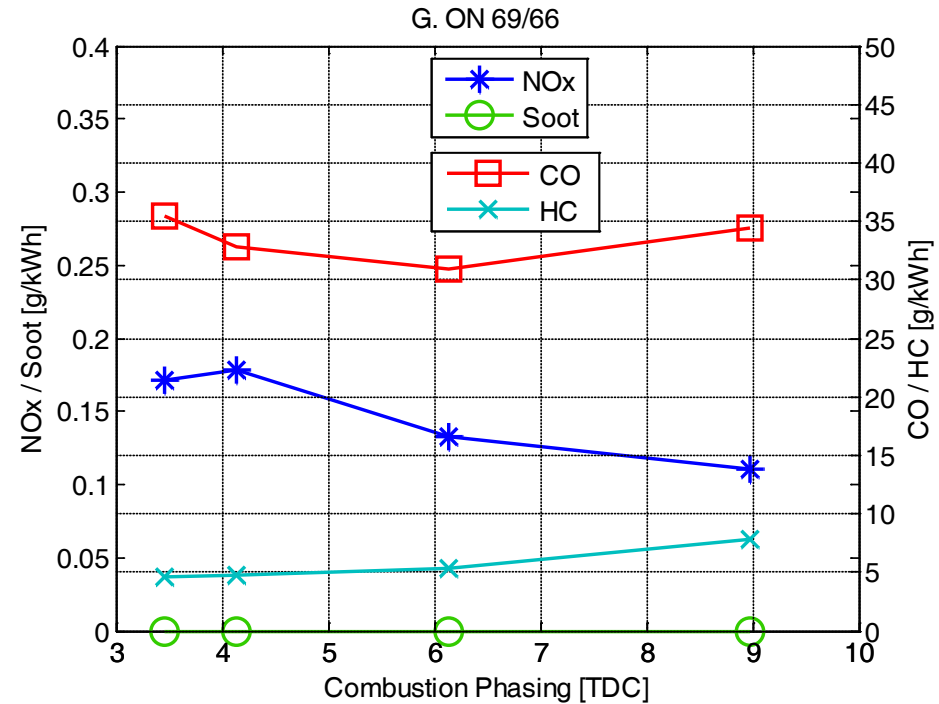
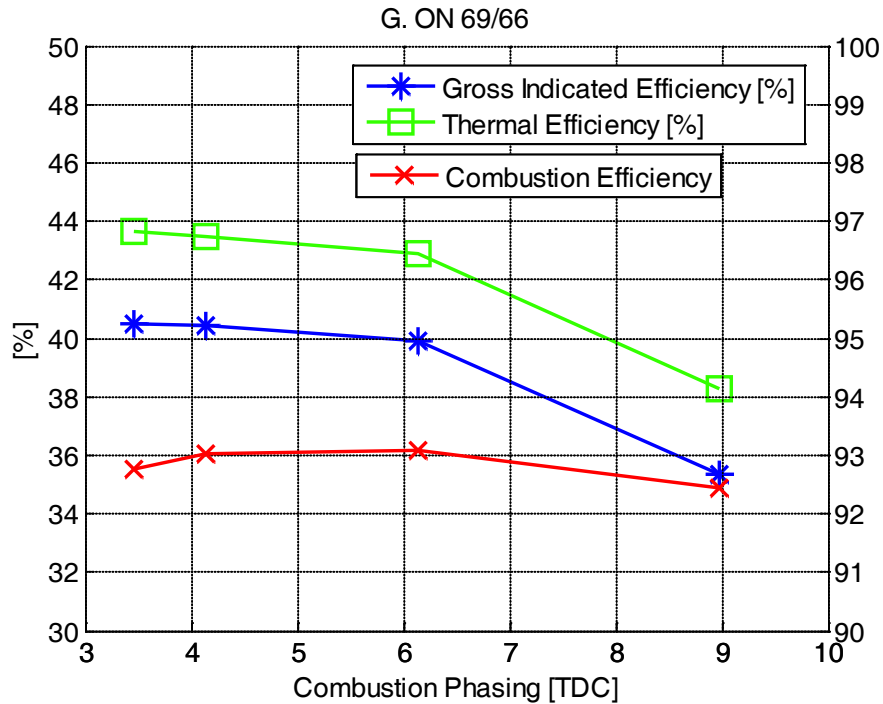
Acoustic Noise



Idle



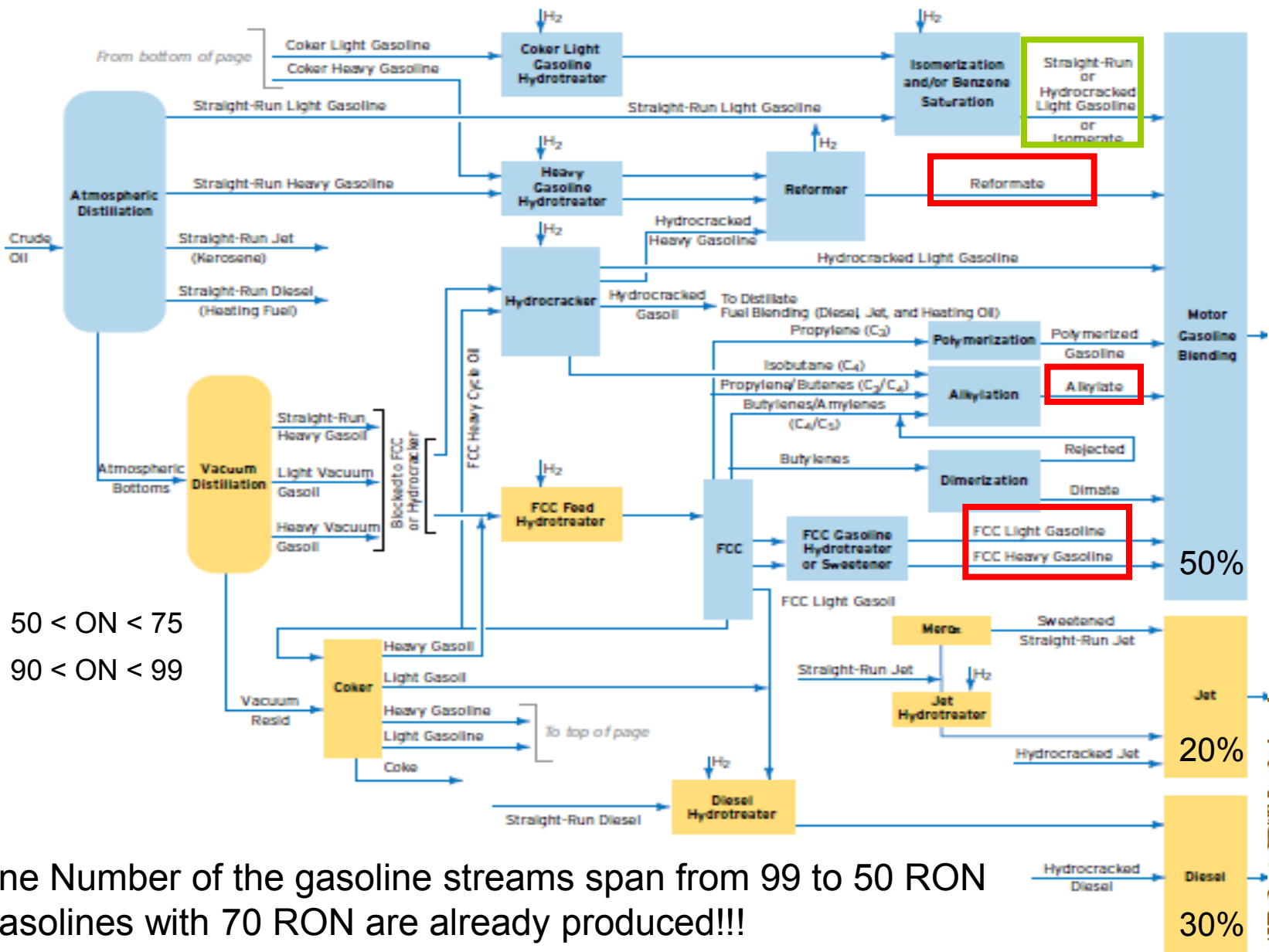
Efficiencies & Emissions



Viability of Low ON Gasolines for PPC?



Oil Refineries Production Layout



 50 < ON < 75
 90 < ON < 99

Octane Number of the gasoline streams span from 99 to 50 RON
 → Gasolines with 70 RON are already produced!!!



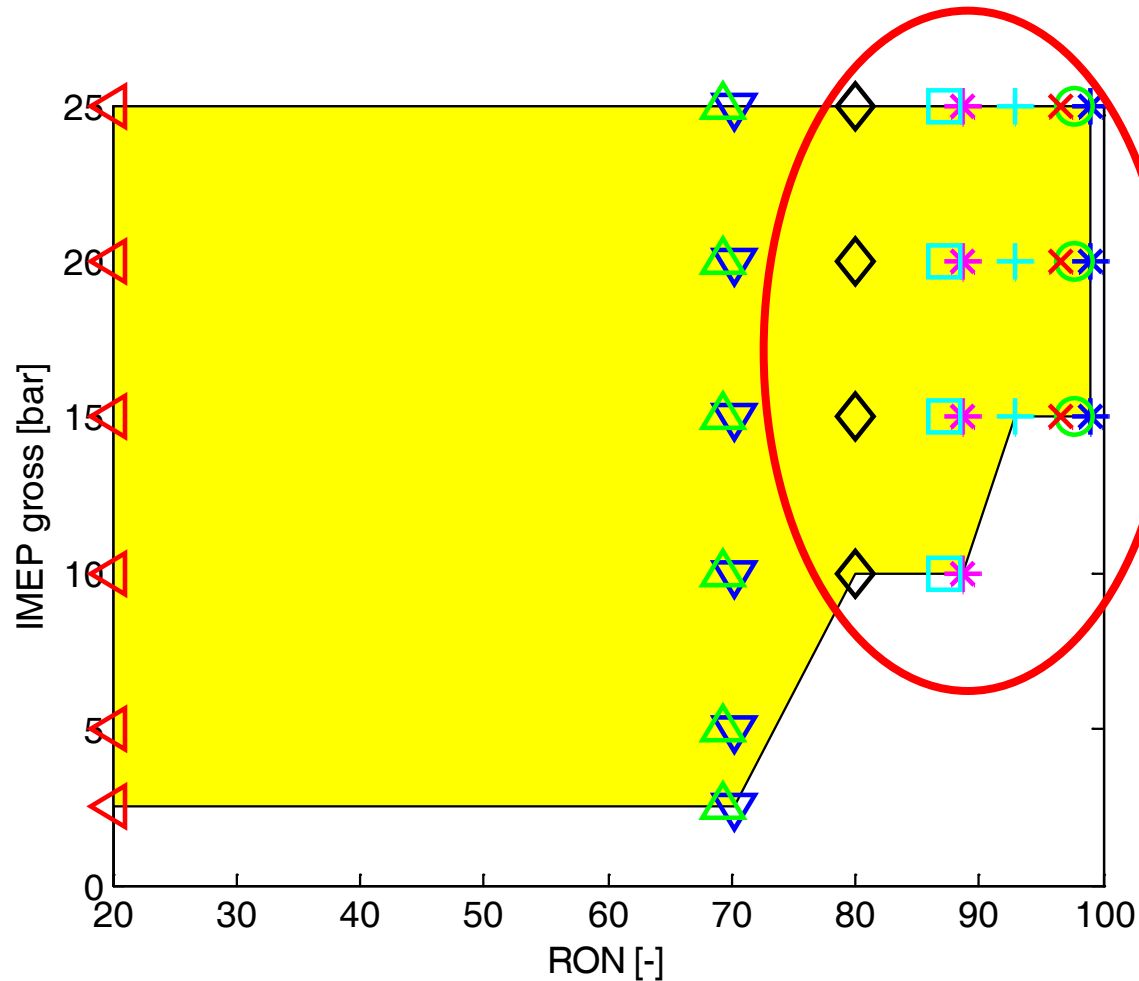
Oil Refineries Perspectives



Oil refineries are a very stiff system and their kerosene, diesel and gasoline production can not be easily varied without major investments → we need to build highly efficient vehicles with the available fuels...



High ON Gasolines in Scania D13



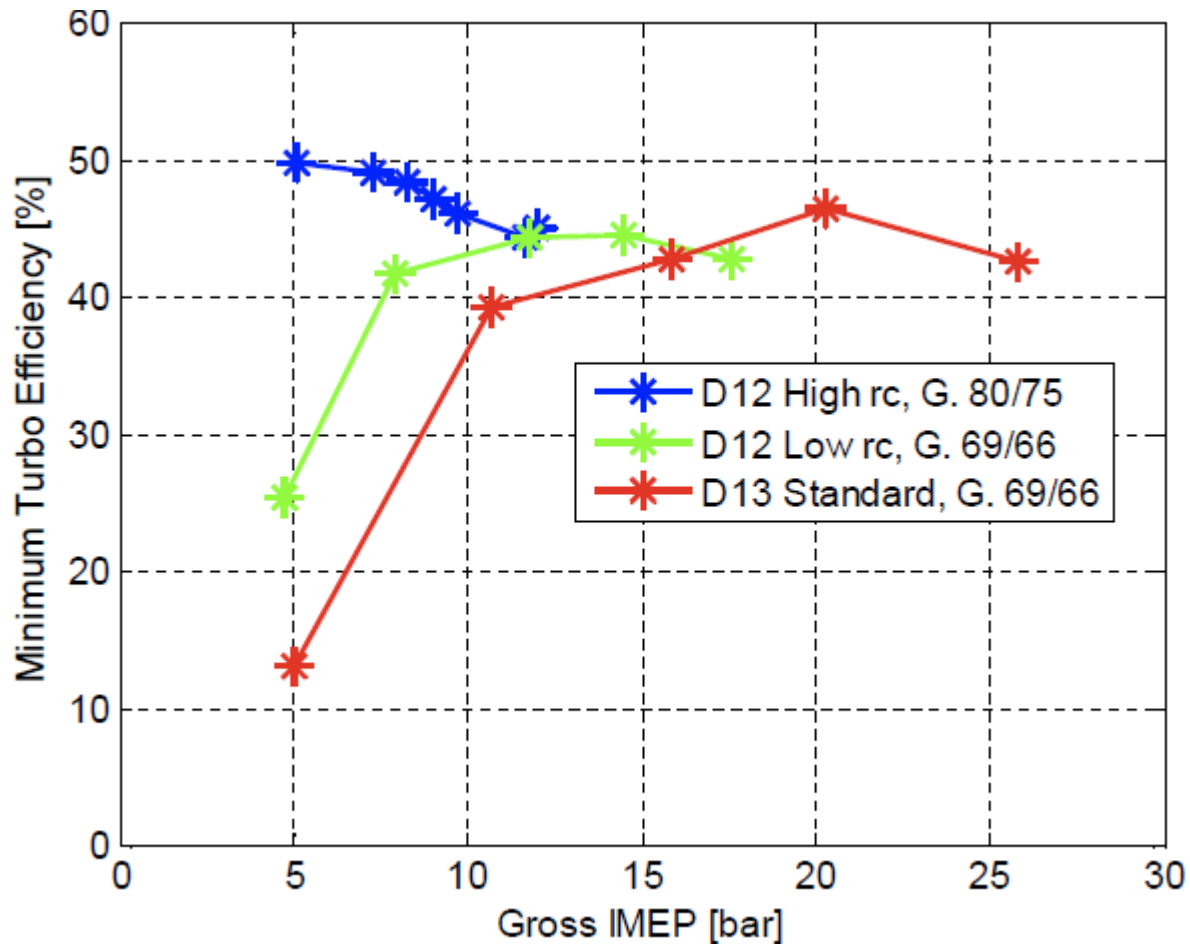
What to do with these fuels?!

Still to be used in SI engines?!



Minimum Turbo Efficiency

$$W_{compressor_ideal} = \eta_{compressor} \cdot \eta_{turbine} \cdot \eta_{mechanical} \cdot W_{turbine_ideal}$$



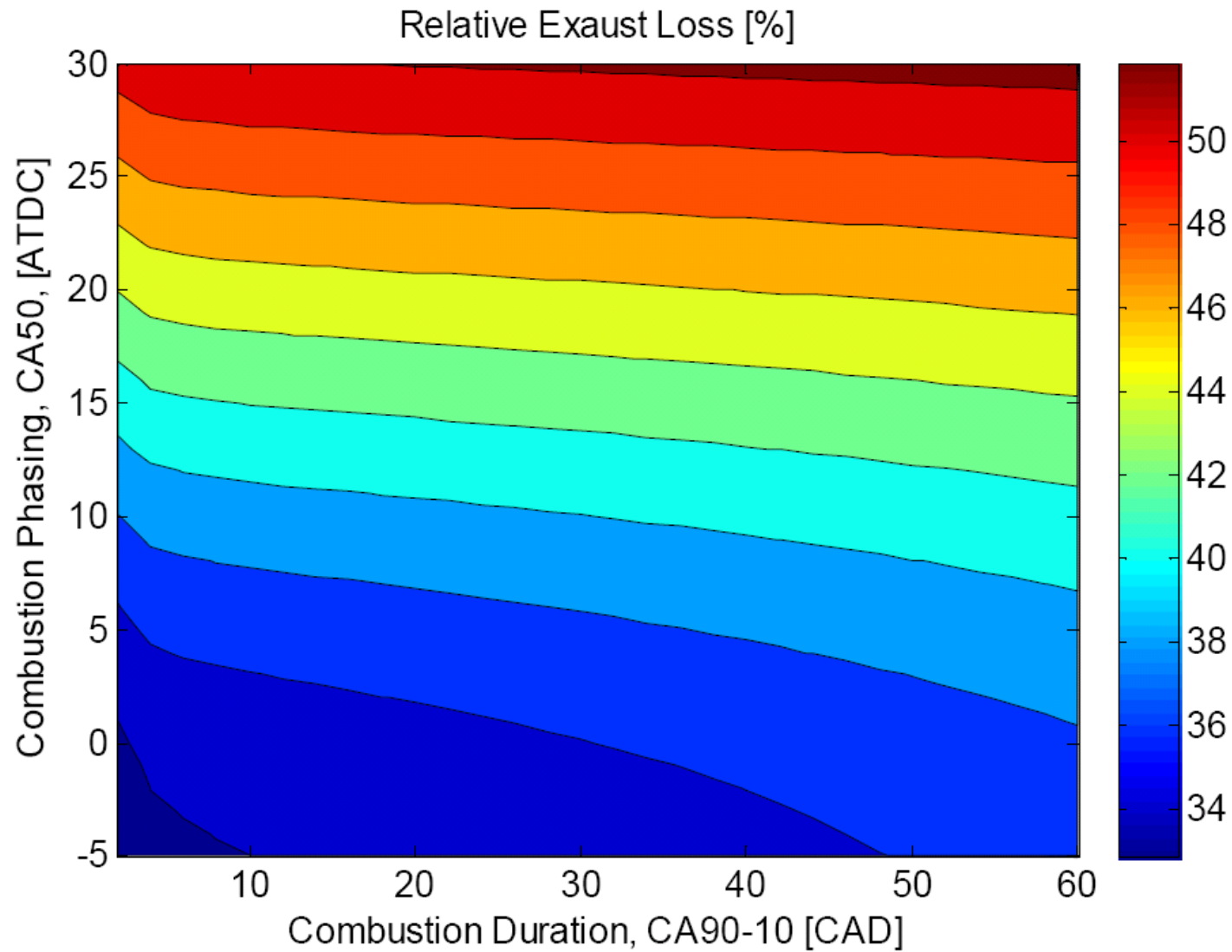
Ideal burn rate?

Conditions:

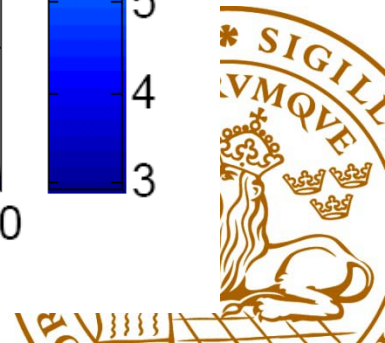
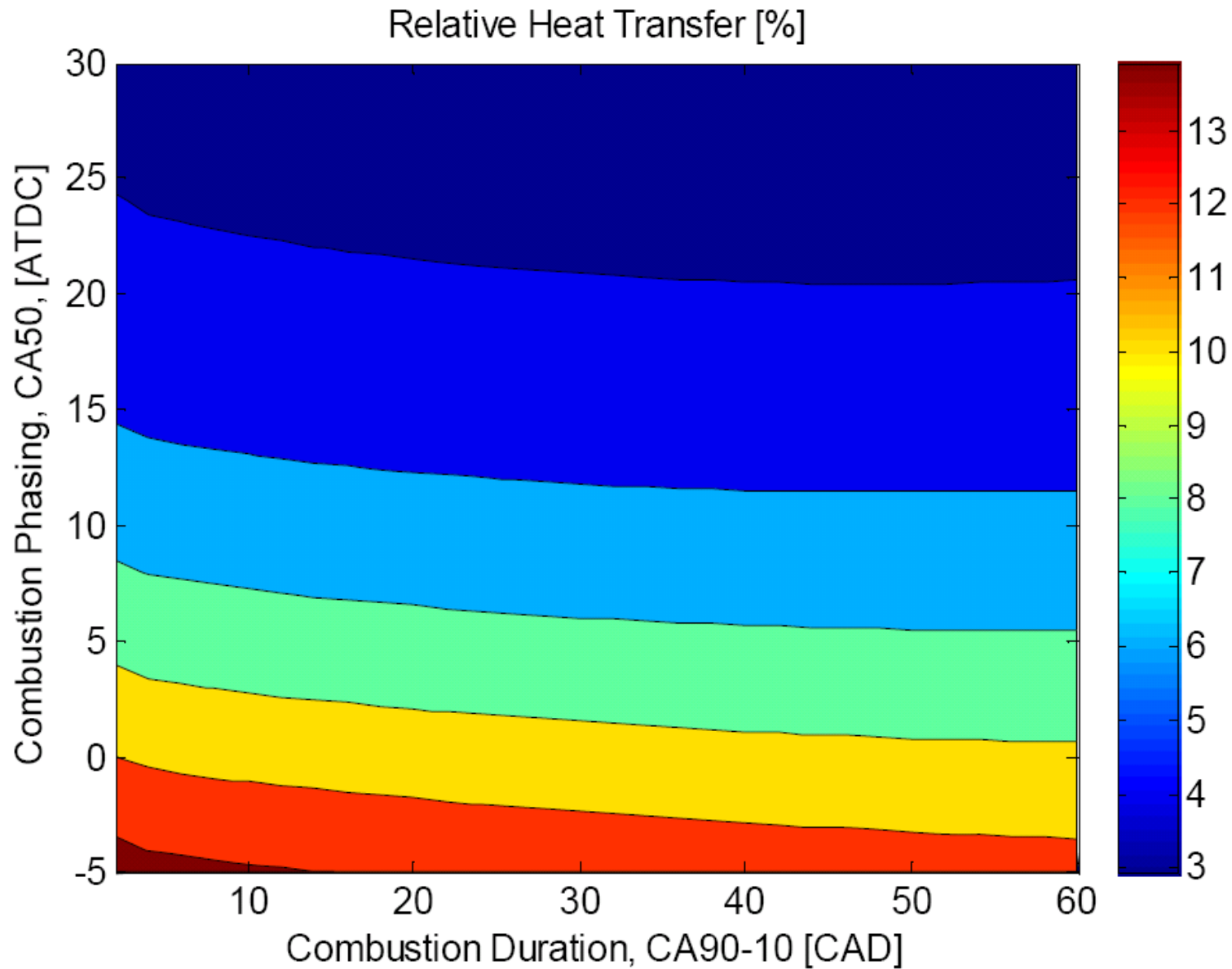
1. CA50: 8 [ATDC].
2. CA90-10: 15 [CAD].
3. Engine geometry: custom Scania D13.
4. Inlet temperature: 303 [K].
5. Reference temperature: 298 [K].
6. Engine speed: 1250 [rpm].
7. Differential pressure exhaust minus inlet: 0.25 [bar].
8. Cylinder wall temperature: 450 [K].
9. **Heat transferred modeled with the Woschni equation** and tuned to match the experimental results
10. **The rate of heat release has been approximated with a Wiebe function.**
11. EGR is added in order to have 1.35 as λ . If the inlet pressure was not enough to have λ without EGR higher than 1.35, EGR was set to zero.
12. The combustion efficiency was assumed to be 100%.
13. Lower heating value 43.8 MJ/kg, stoichiometric air fuel ratio 14.68.



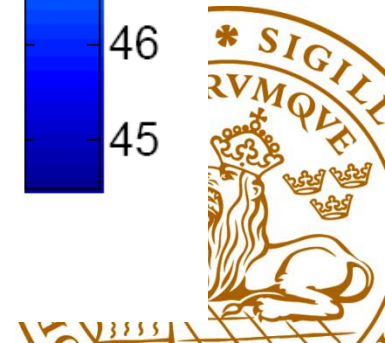
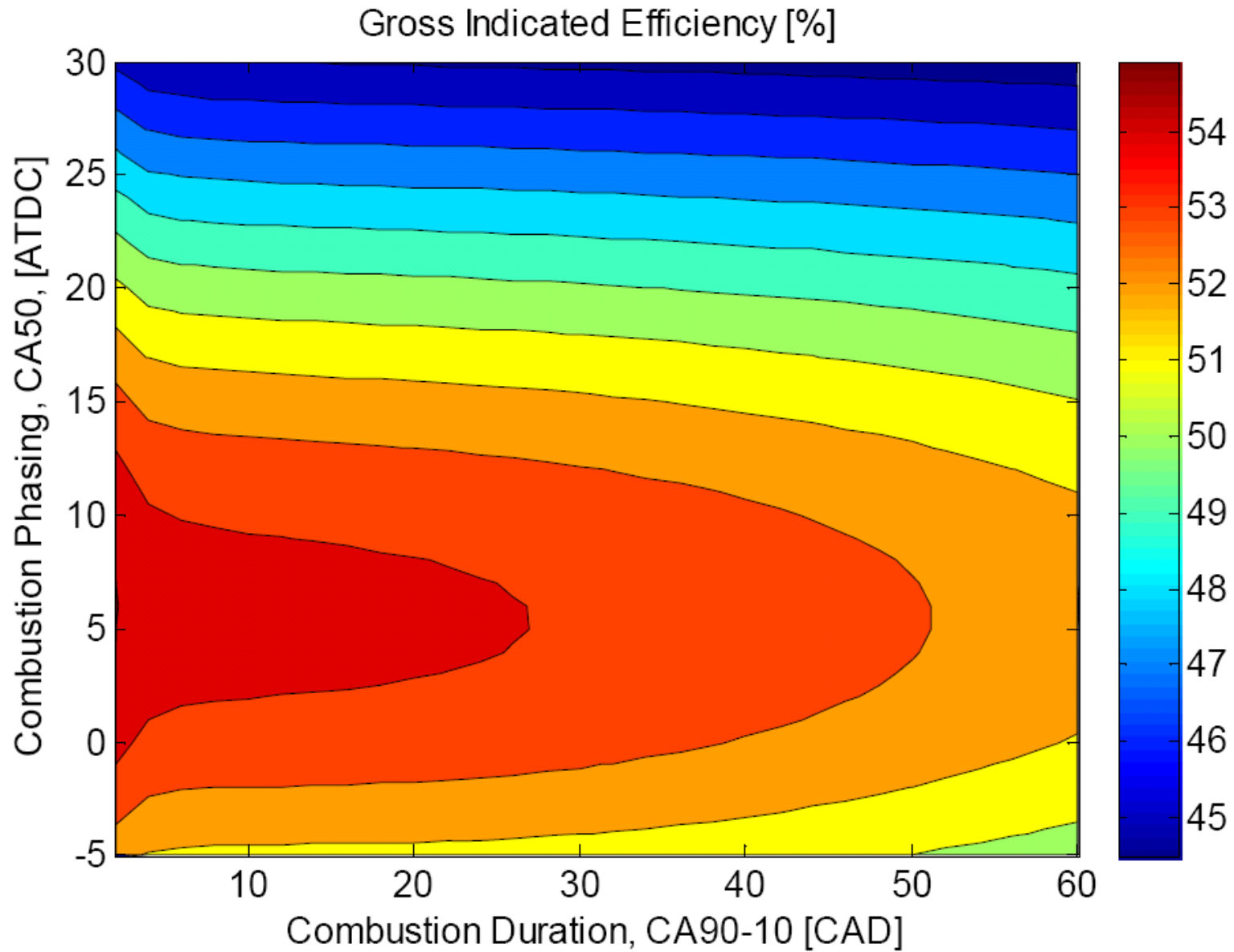
Exhaust Loss



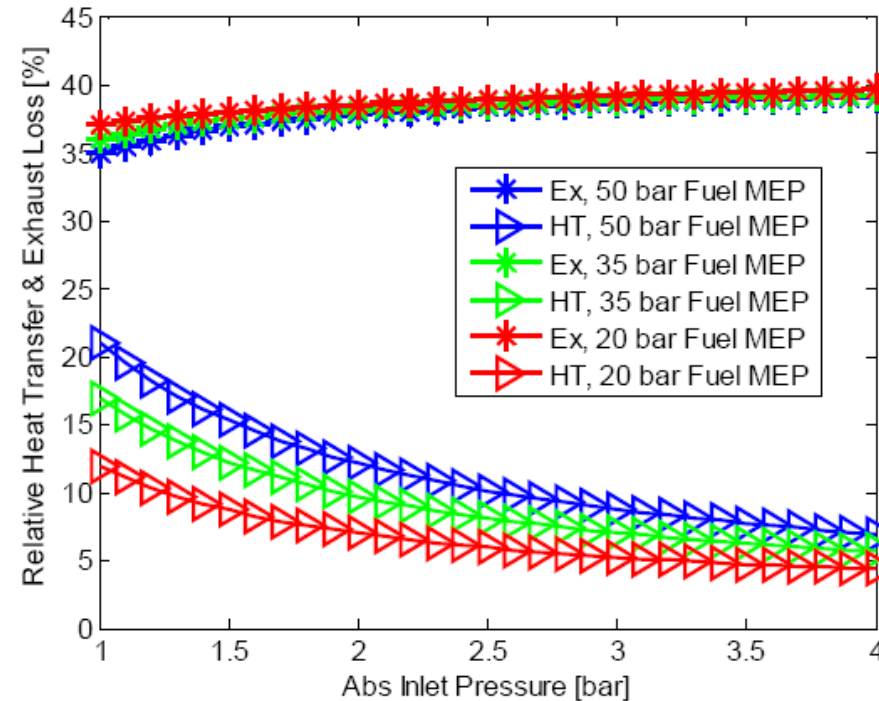
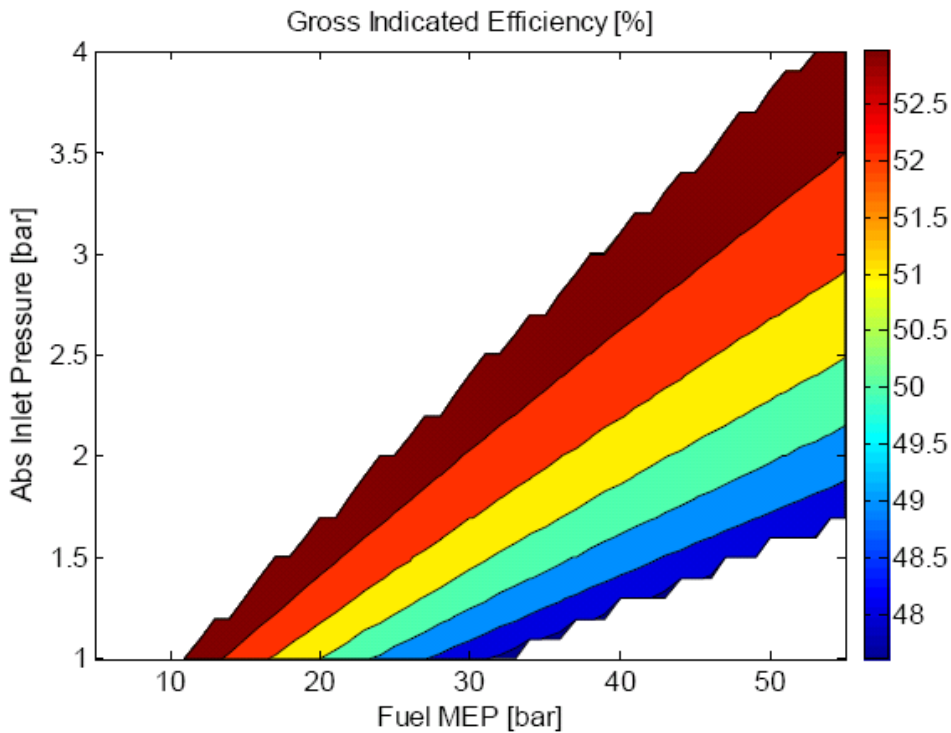
Heat transfer loss



The rest (useful work)



Boosting reduce heat losses



A-B-C of Fuel Consumption

- A. Car size
- B. Engine size
- C. Engine efficiency in right operating conditions



Porsche 911 performance with 100+ mpg?

- Two persons
- 100 liter of storage capacity



Porsche 911 data

$M=1550$ kg
 $C_r=0.012$
 $A_v=1.96$ m²
 $C_d=0.33$

$V_d=3.8$ liter
 $P=355$ PS (hp)
 $T=400$ Nm

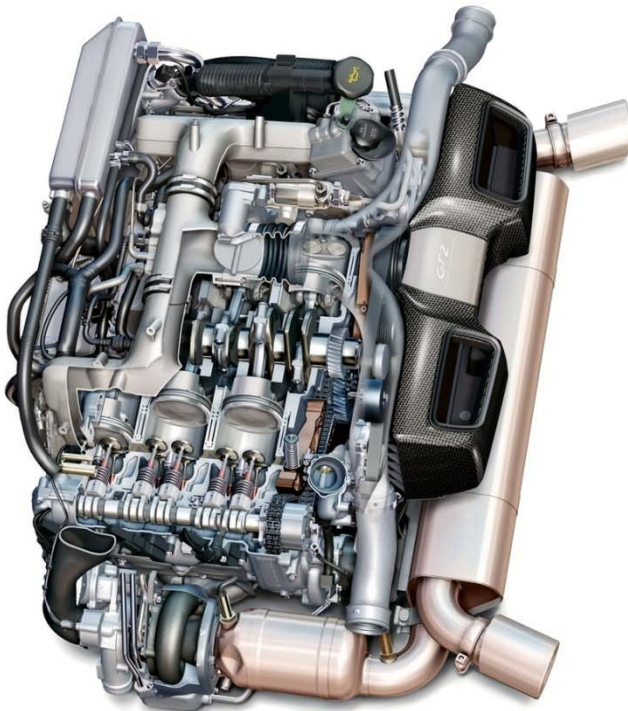


Performance

0-60: 4.6 s

$V_{max}=300$ km/h (186.5 mph)

Fuel consump.= 12.0 l/100 km (19.6 mpg)



Power needed @300 km/h (186.5 mph)

$$P = (C_R mg + 0.5 \rho_a C_D A_v v^2) v =$$
$$\left(0.012 \times 1550 \times 9.81 + 0.5 \times 1.2 \times 0.33 \times 1.96 \times \left(\frac{300}{3.6} \right)^2 \right) \times \left(\frac{300}{3.6} \right)$$
$$= 239.8 \text{ kW} = 326.1 \text{ hp}$$



The "Cigar"



Two person capacity is often enough

UK National Office of Statistics:
"The average car occupancy is 1.6 people per car and for commuting it's 1.2"



A carpool in California is a car with ONE person if the car is fuel efficient...



The "Cigar"

Existing large model use large BMW 1200 cc MC engine. With turbo a top speed of 315 km/h and fuel consumption of 3.5 l/100 km (67 mpg)

<http://www.peraves.ch/>



Power needed @300 km/h (186.5 mph)

Cigar design specifications

$$C_d=0.1$$

$$A_v=0.5-1 \text{ m}^2$$

$$m= 250 \text{ kg}$$

$$C_r=0.012 \text{ (two wheels)}$$

$$P = \left(C_R mg + 0.5 \rho_a C_D A_v v^2 \right) v =$$
$$\left(0.012 \times 250 \times 9.81 + 0.5 \times 1.2 \times 0.10 \times 1.0 \times \left(\frac{300}{3.6} \right)^2 \right) \times \left(\frac{300}{3.6} \right)$$
$$= 37.2 \text{ kW} = 49.7 \text{ hp}$$



Power needed at 50 and 100 km/h (31- 62 mph)

Porsche 911 vs. cigar

Speed (km/h)	911	Cigar	Unit	Ratio
50	3.57	0.57	kW	6.28
100	13.4	2.1	kW	6.36
300	239.8	37.2	kW	6.45
50	4.86	0.77	hp	6.28
100	18.2	2.9	hp	6.36
300	326.1	49.7	hp	6.45

Acceleration proportional to power/mass ratio:

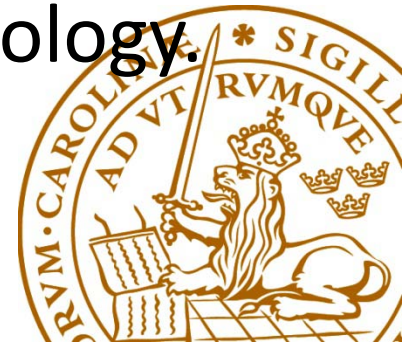
Cigar: $250/49.7=5.03$ kg/hp

911: $1550/355=4.37$ kg/hp



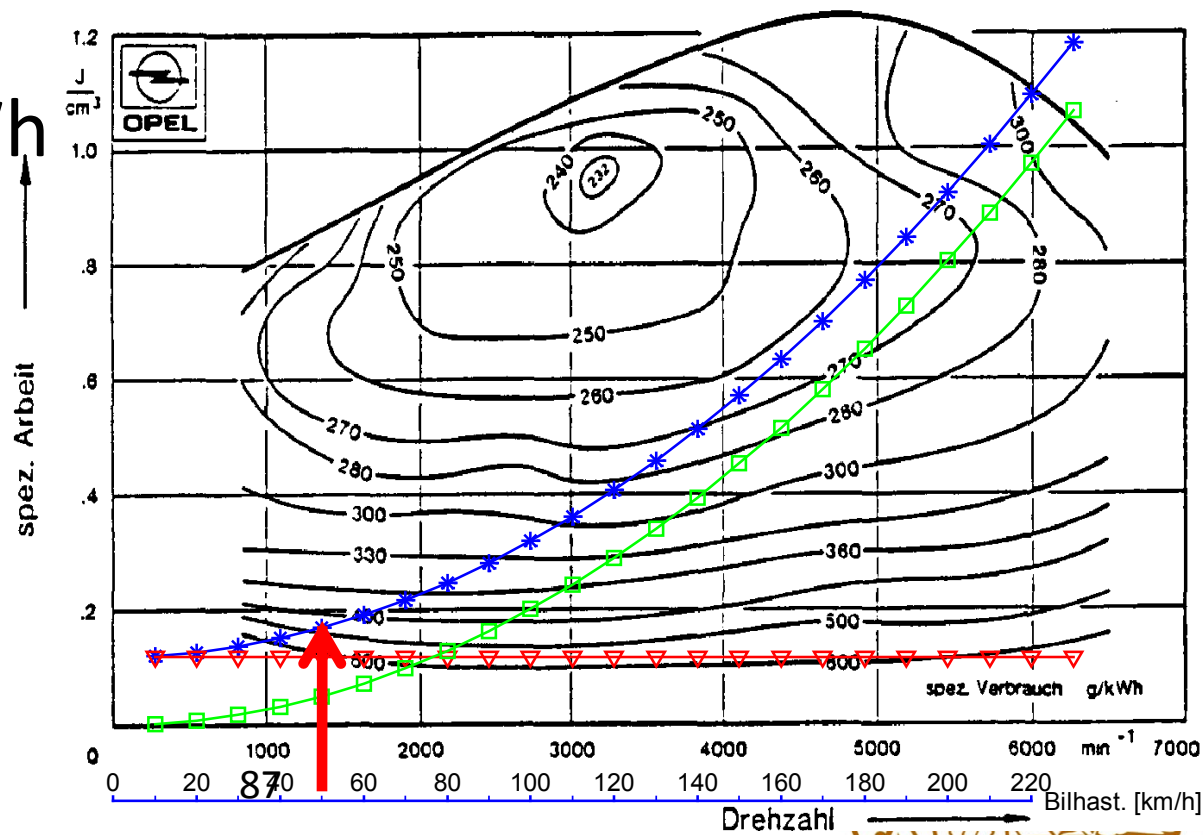
A. Car size

- With more correct car size the engine size can be reduced a factor of 6 i.e. single cylinder version of 911 engine with 633 cc displacement is enough
- Porsche 911 has a fuel consumption of 12 l/100 km (19.6 mpg)
- Cigar would have $12/6=2$ l/100 km (117.6 mpg) without any need of new engine technology.
(Scaling both engine and car size)



B. Engine size

- A Porsche 911 does not operate at optimum load points in normal driving.
- At 50 km/h the estimated load is only 2 bar BMEP or less
- $B_{sfc} = 400 \text{ g/kWh}$
($\eta_b = 21 \%$)



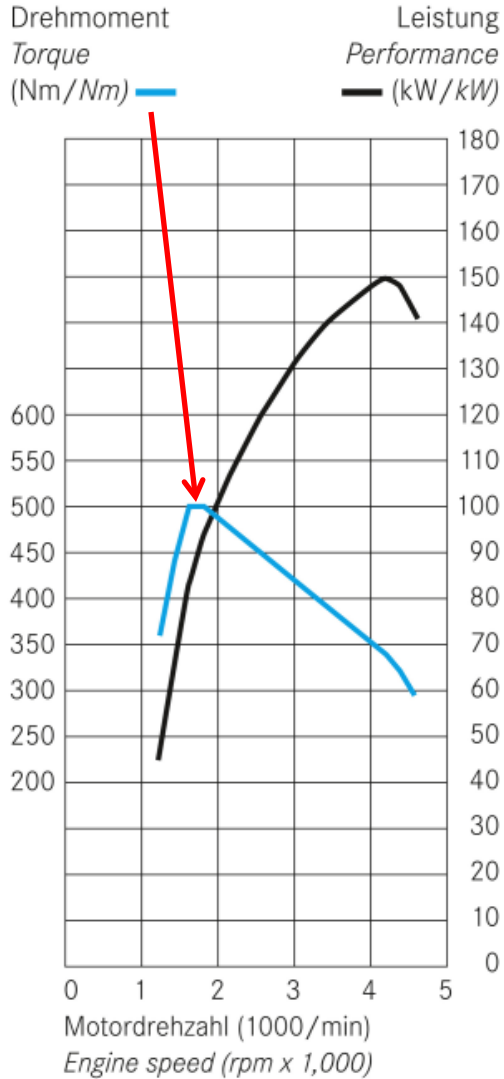
Engine downsizing

Three options

1. Turbo or supercharge a small engine
2. Cylinder deactivation of large engine
3. Variable displacement i.e. variable engine size



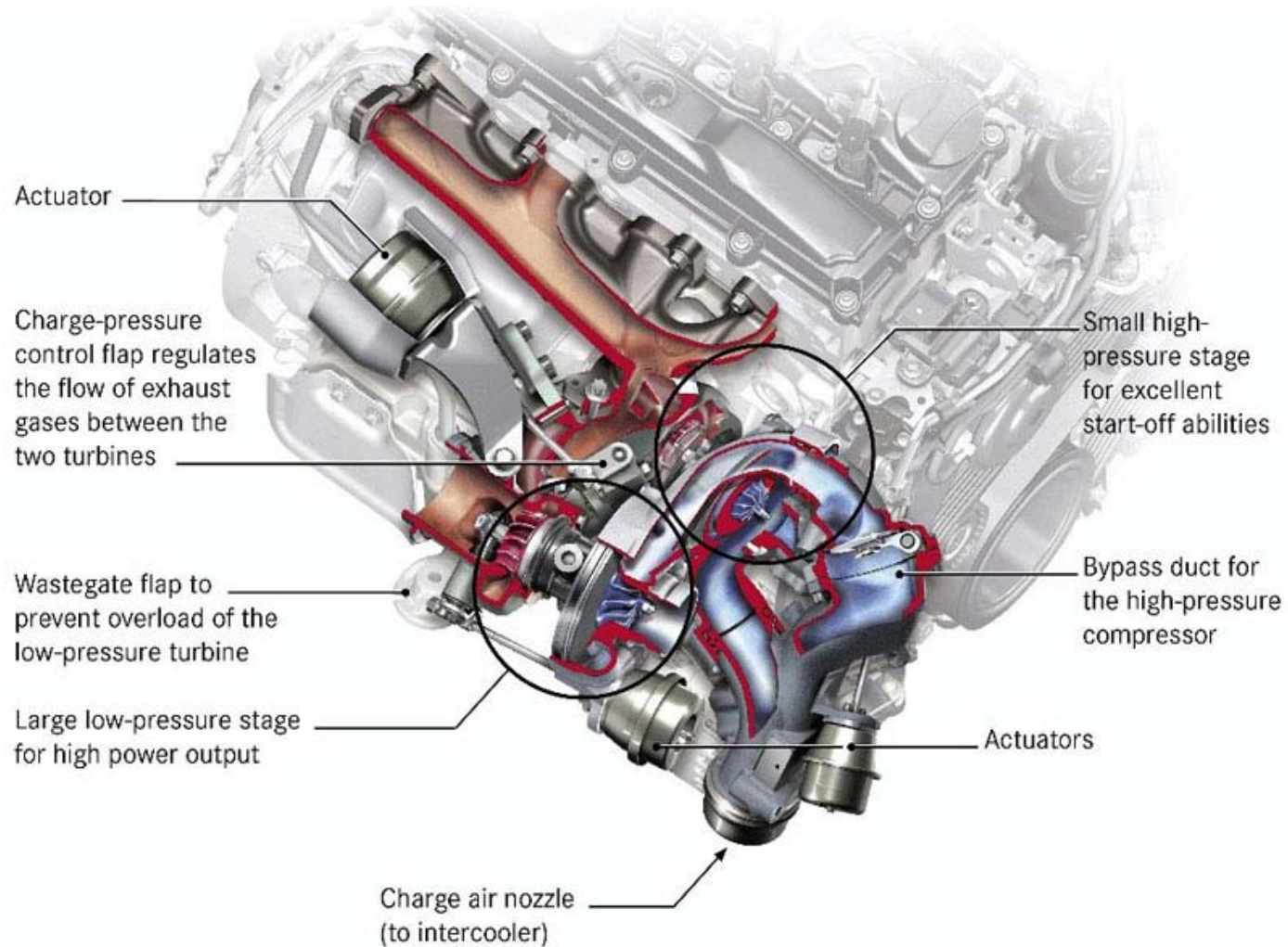
B.1. Mercedes CDI 250, 2.1 liter



Vd=2143 cc
Torque= 500 Nm (369 lb-ft)



Two stage turbo



Engine downsizing- MB 250 CDI

Displacement of 2.1 liter giving 224 hp and 500 Nm of torque :
30 bar BMEP is now full load **NOT** 10 or 20 bar

Fuel consumption;

C-class 5.1 l/100 km (46.1 mpg),

E-class 5.3 l/100 km (44.4 mpg),

S-class 5.9 l/100 km (39.9 mpg)

CO2:

C-class 139 g/km

E-class 143 g/km

S-class 155 g/km



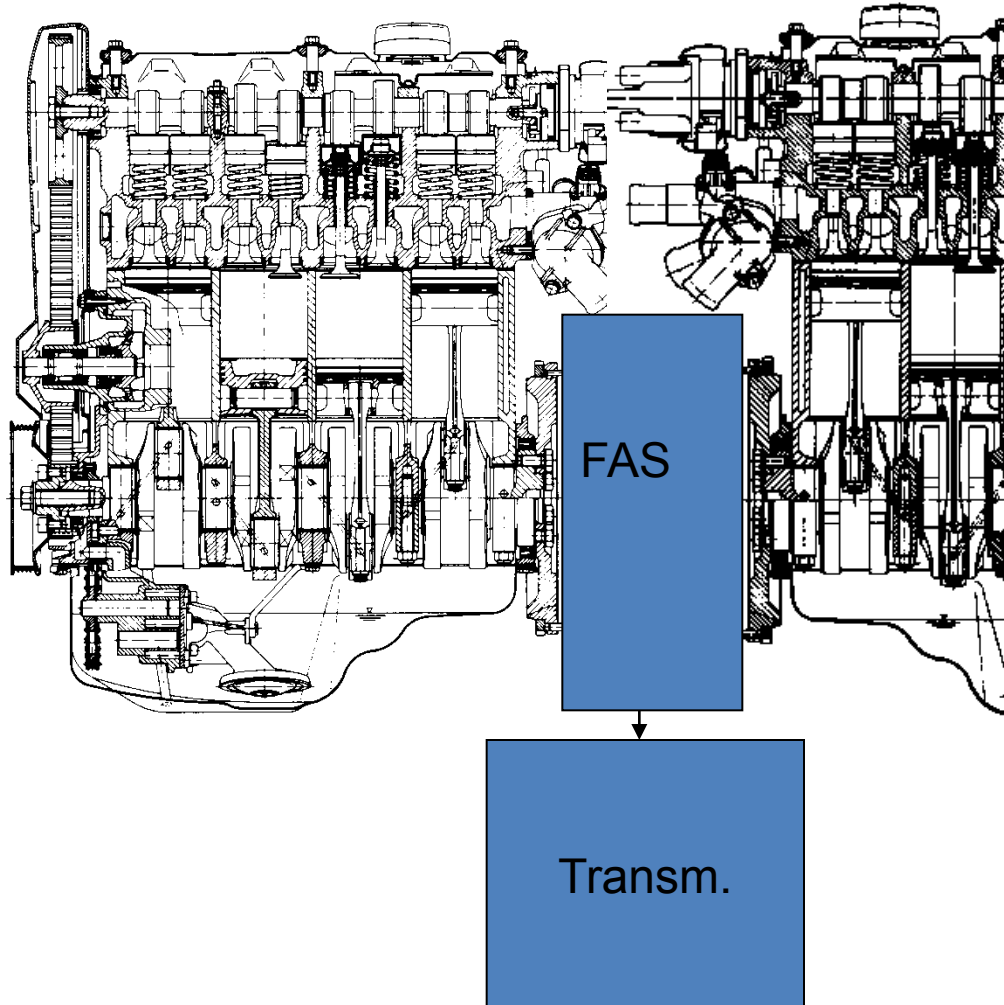
B2: Dual engine concept

- Use one small and one large engine
- As an example:
 - One 2 cylinder 1 liter engine
 - One 4 cylinder 2 liter engine
- This gives us 1, 2 or 3 liter to choose from



Layout 4 + 2 cyl

Fiat 2-cylinder
production engine



Operation

- 2-cyl at low loads
- 4-cyl operation at higher load operation (Autobahn)
- 6-cyl operation at highest loads
- 6-cyl + FAS at transients (with FAS start of 4-cyl)
- FAS for regenerative braking
- FAS for lowest speed operation (< 5 km/h)
- Manual selection should be possible



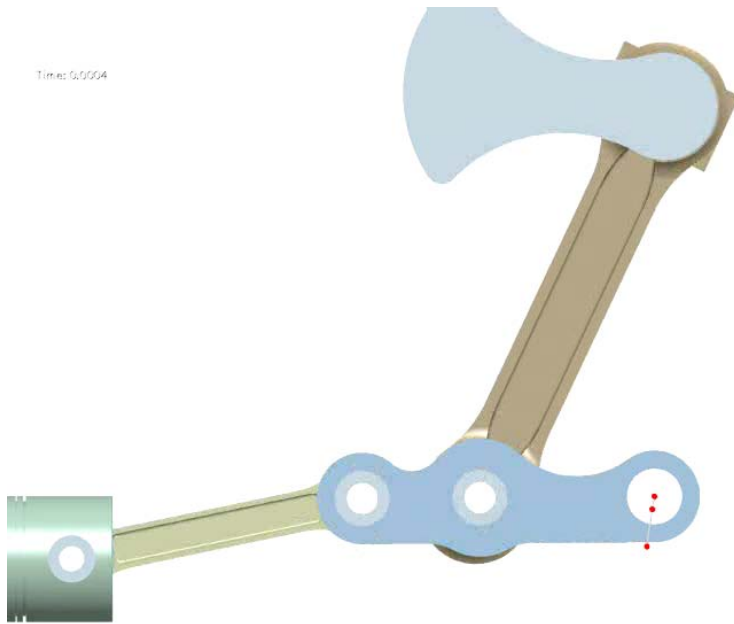
B3: Variable displacement engine

- If we can change displacement, V_d , engine load, P , can be controlled without reducing BMEP!

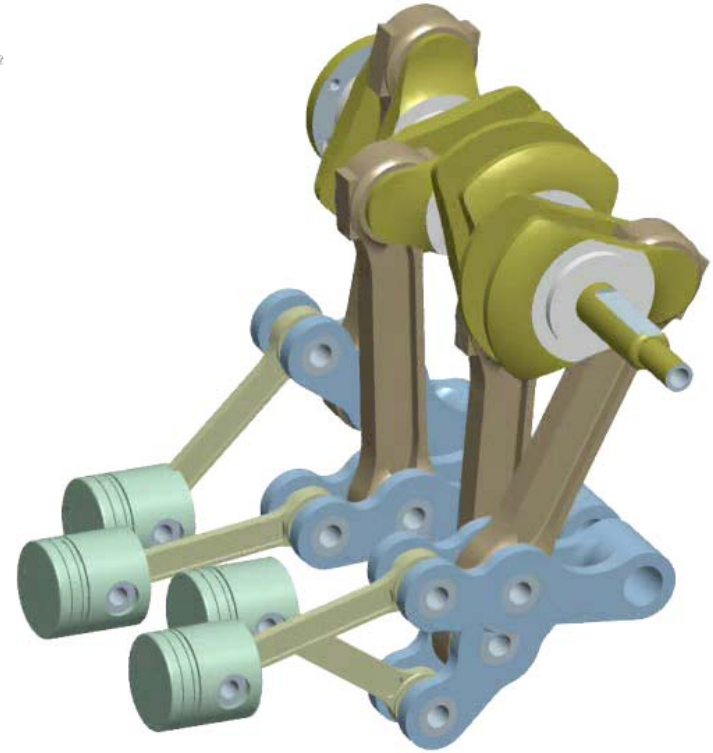
$$P = bmep V_d \frac{N}{n_t}$$



Atkinson Cycle



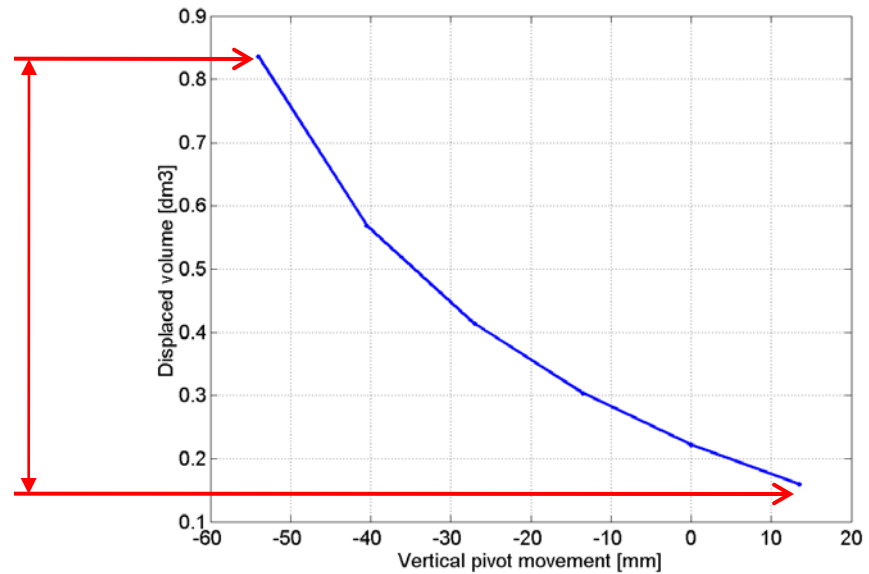
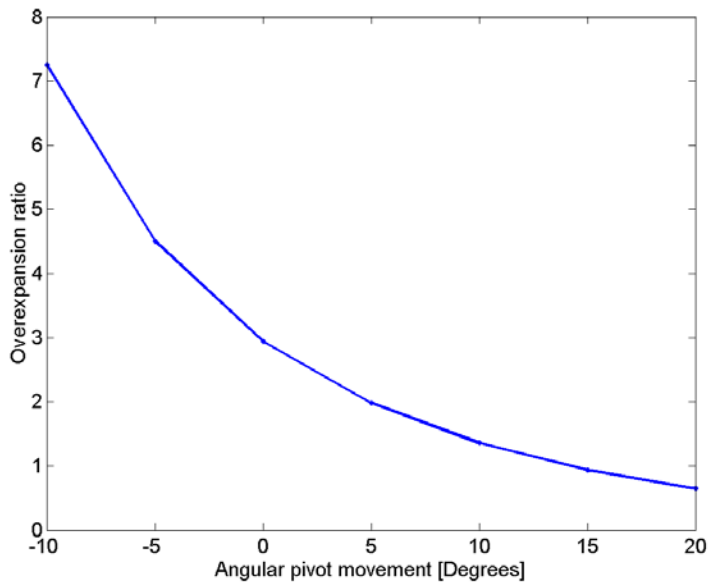
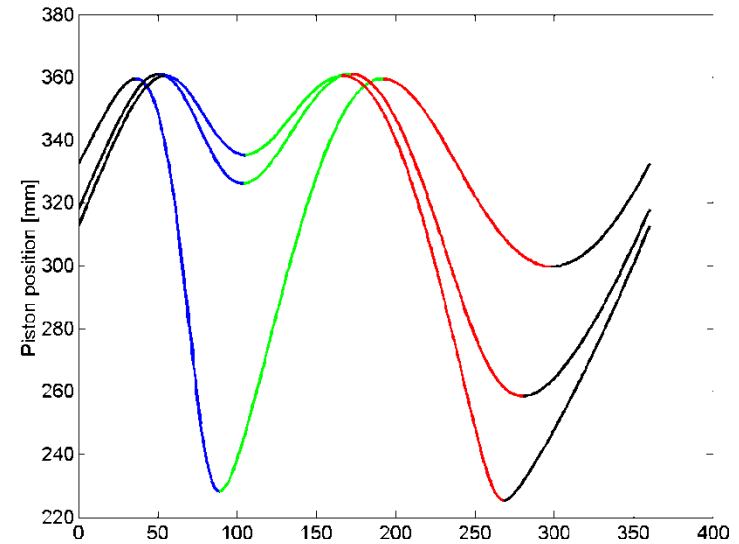
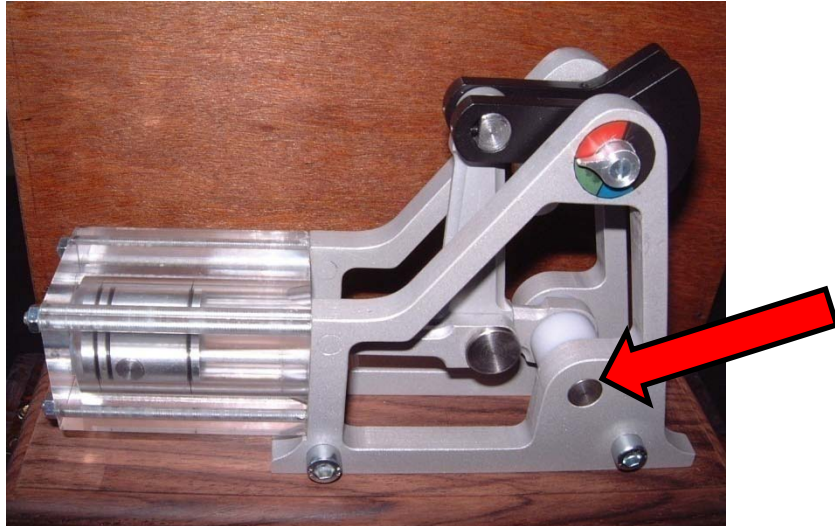
Time: 0.0002



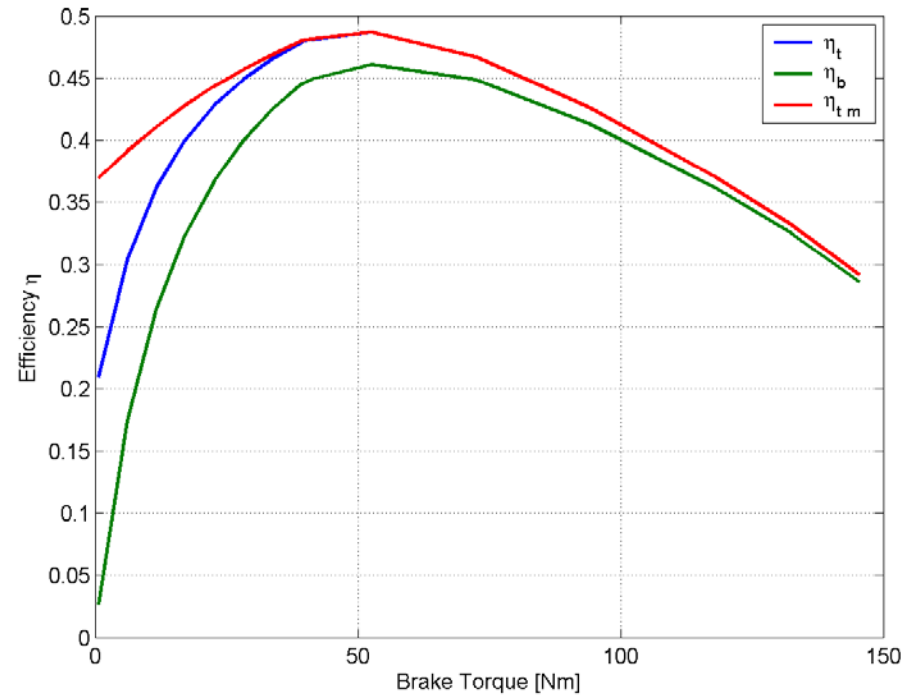
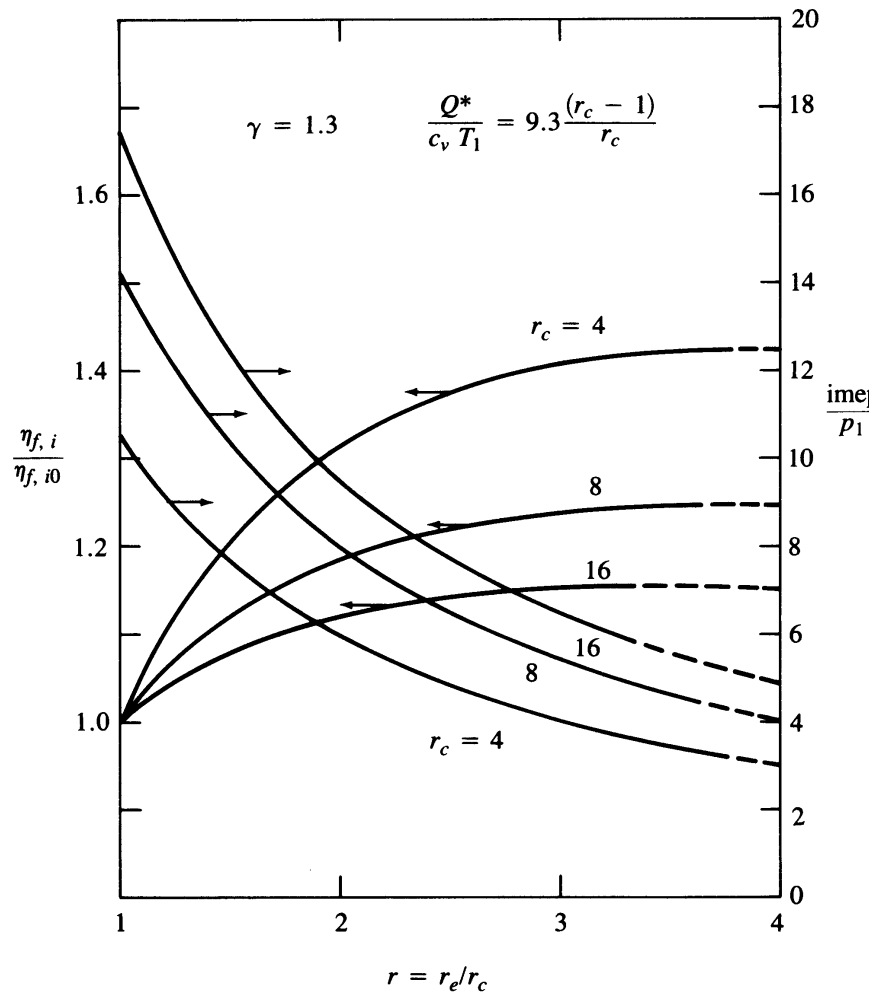
Displacement from 0.15 to 0.85 l per cylinder gives 0.6 to 3.4 l four cylinder engine at full load (@max BMEP)



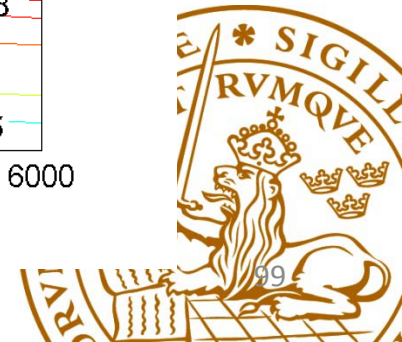
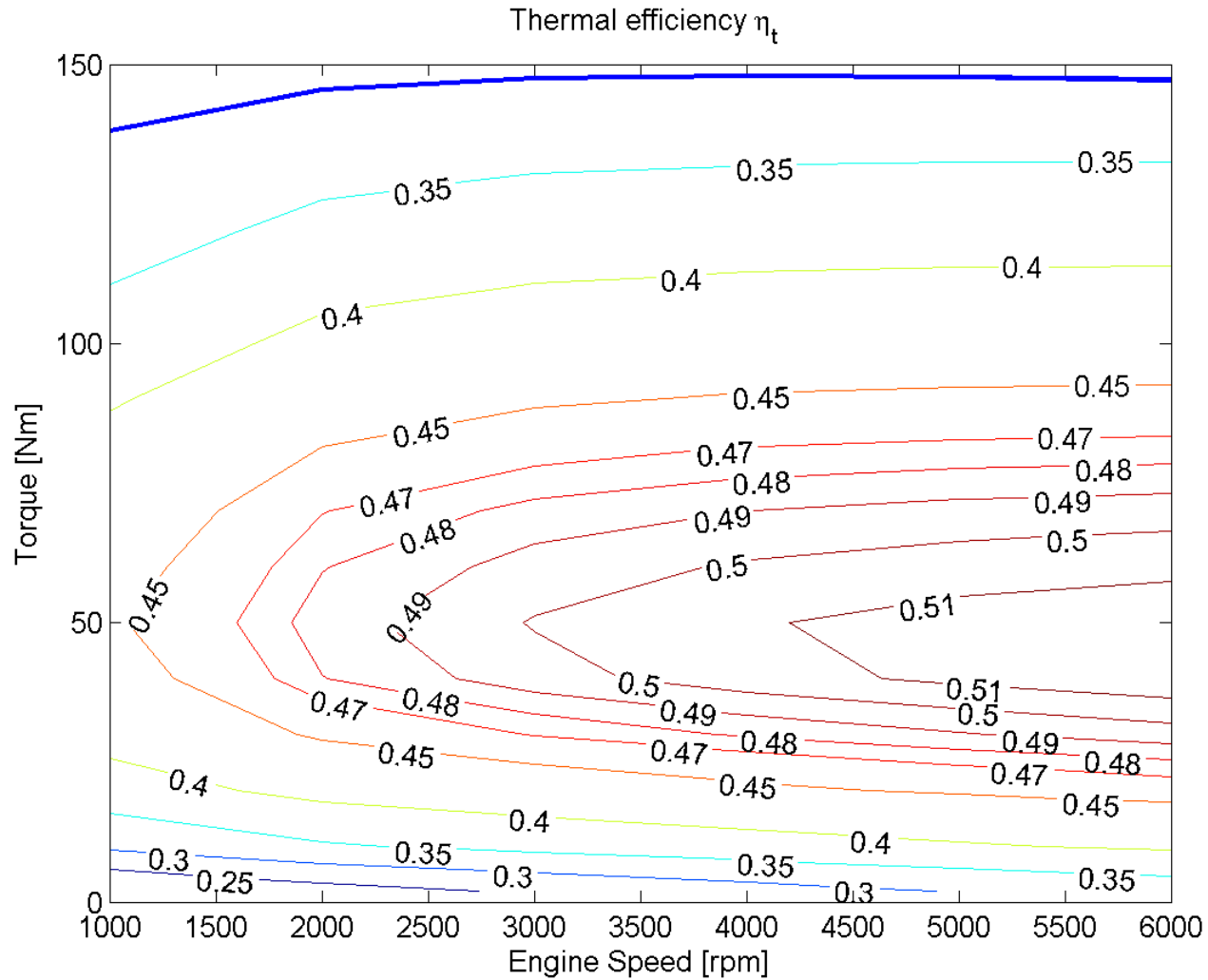
Atkinson engine with variable displacement



Atkinson engine efficiency



Atkinson engine thermal efficiency



A-B-C of Fuel Consumption

- A. Car size
- B. Engine size
- C. Engine efficiency in right operating conditions
(Maximum engine efficiency)



Summary /ABC of fuel consumption

- A. Correct car size gives factor of 6 in fuel consumption
- B. Correct load point gives factor 2 in fuel consumption (21%-42% or 400-200 g/kWh)
- C. Partially Premixed Combustion have the potential to extend brake efficiency to 50% with US10/Euro emissions. With further optimization 55% could be reached
- D. With waste heat recovery 60% should be possible giving a factor of 3 from today.

A total reduction potential of factor 18!



Cars and traffic situation

