

# Improved Methods for Making Intermetallic Anodes

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Project ID #: ES022

# Objectives

- Make electrodes based on intermetallic alloys such as  $\text{Cu}_6\text{Sn}_5$  using a wide selection of binders with a particular emphasis on binders that are able to accommodate relatively large volume expansions.
- Develop methods to determine and control the optimum particle size, composition, and morphology of  $\text{Cu}_6\text{Sn}_5$  based intermetallic alloys.

# Overview

## Timeline

- Start: October 2008
- Finish: September 2014
- ~25% Complete

## Budget

- Total project funding
  - 100% DOE
- \$300K FY09 (ABR)
- \$300K FY10 (ABR)

## Barriers

- Development of a safe cost-effective PHEV battery with a 40 mile all electric range that meets or exceeds all performance goals
  - Intermetallic alloys have the potential to be high capacity anode materials, but the their large volume expansion must be addressed

## Partners

- Dileep Singh (ANL-NE)
- Wildcat Discovery Technologies
- Binder vendors



# Milestones

|                                                                               |                 |
|-------------------------------------------------------------------------------|-----------------|
| Determine influence of binder on $\text{Cu}_6\text{Sn}_5$ cycle life          | March, 2009     |
| Explore methods of controlling particle size and morphology                   | May, 2009       |
| Produce an intermetallic electrode with 200 cycles and 80% capacity retention | September, 2009 |

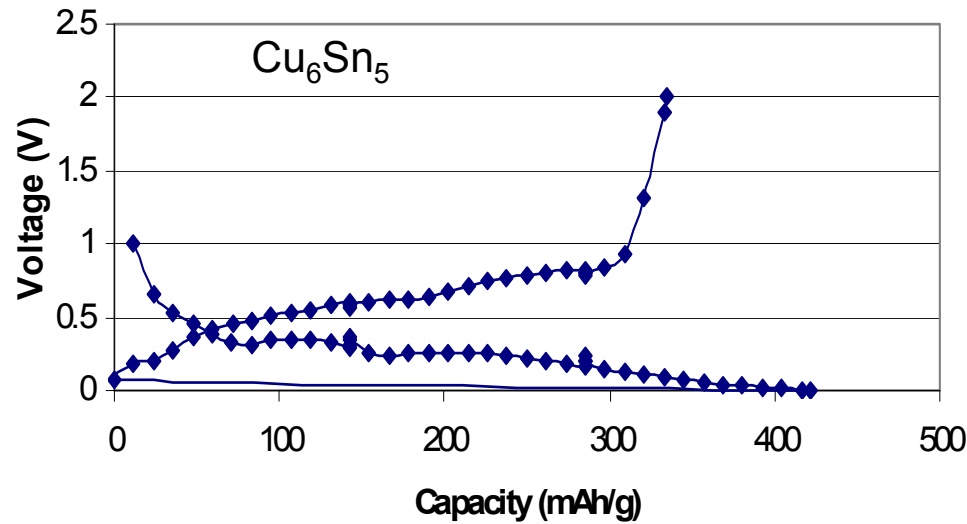


# Approach

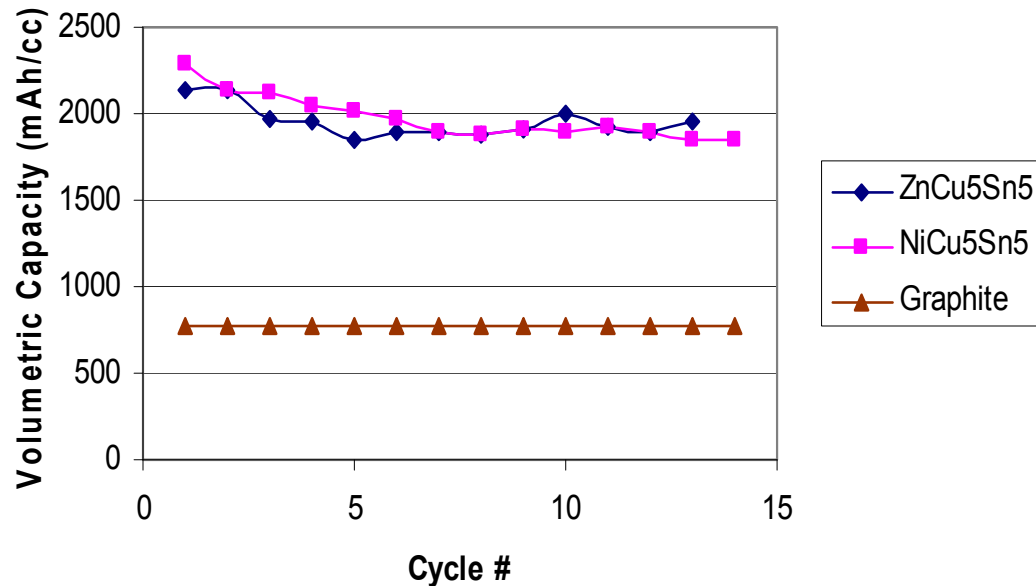
- The general approach in this subtask will be to explore alternative methods of making electrodes based on intermetallic alloys such as  $\text{Cu}_6\text{Sn}_5$ . The goal is not to create new classes of active materials but rather, to employ materials already being developed in the BATT Program.
- Success will be achieved upon development of an electrode that can accommodate the large volume expansion and contraction during deep discharge cycling, and can prevent the excluded metal (such as copper) from agglomerating into an inert mass during cycling.
- Likely solutions to these problems will involve the proper choice of binders and methods of controlling the particle size and morphology during production, and during repeated cycling.



# Why the Interest in Intermetallic Alloys



- Previous work from the BATT program has shown that doped- $\text{Cu}_6\text{Sn}_5$  materials have reversible capacities similar to graphite
- When their high density is taken into account the volumetric capacities are nearly 3X that of an optimized graphite based electrode.



# Metal Alloys Provide an Advantage in Calculated PHEV Battery Designs

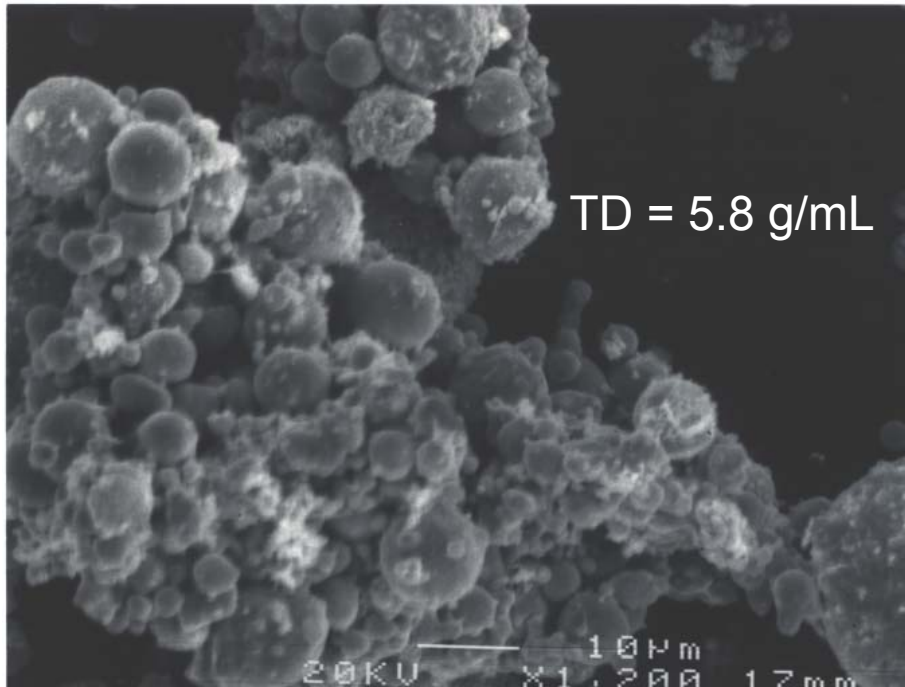
| Cell Couple                               | Graphite<br>vs.<br>NCM  | Cu <sub>6</sub> Sn <sub>5</sub><br>vs.<br>NCM |
|-------------------------------------------|-------------------------|-----------------------------------------------|
| <b>Positive Electrode (32 % porosity)</b> |                         |                                               |
| Material Capacity                         | 200 mAh/g               | 200 mAh/g                                     |
| Active Loading                            | 84 %                    | 84 %                                          |
| Coating Thickness                         | 72 μm                   | 100 μm                                        |
| Coating Loading                           | 18.4 mg/cm <sup>2</sup> | 28.4 mg/cm <sup>2</sup>                       |
| <b>Negative Electrode (34 % porosity)</b> |                         |                                               |
| Material Capacity                         | 290 mAh/g               | 400 mAh/g                                     |
| Active Loading                            | 92 %                    | 84 %                                          |
| Coating Thickness                         | 100 μm                  | 67 μm                                         |
| Coating Loading                           | 14.9 mg/cm <sup>2</sup> | 18.3 mg/cm <sup>2</sup>                       |

| Cell Couple       | Graphite<br>vs.<br>NCM | Cu <sub>6</sub> Sn <sub>5</sub> vs.<br>NCM |
|-------------------|------------------------|--------------------------------------------|
| Battery Power     | 45 kW                  | 45 kW                                      |
| Battery Weight    | 111 kg                 | 104 kg                                     |
| Battery Volume    | 69 L                   | 54 L                                       |
| Battery Energy    | 15.5 kWh               | 15.5 kWh                                   |
| C/3 Capacity      | 46.8 Ah                | 53.5 Ah                                    |
| Number of Modules | 8                      | 8                                          |
| Cells per Battery | 96                     | 96                                         |
| Battery Voltage   | 336 V                  | 298 V                                      |
| Vehicle Range     | 40 miles               | 40 miles                                   |

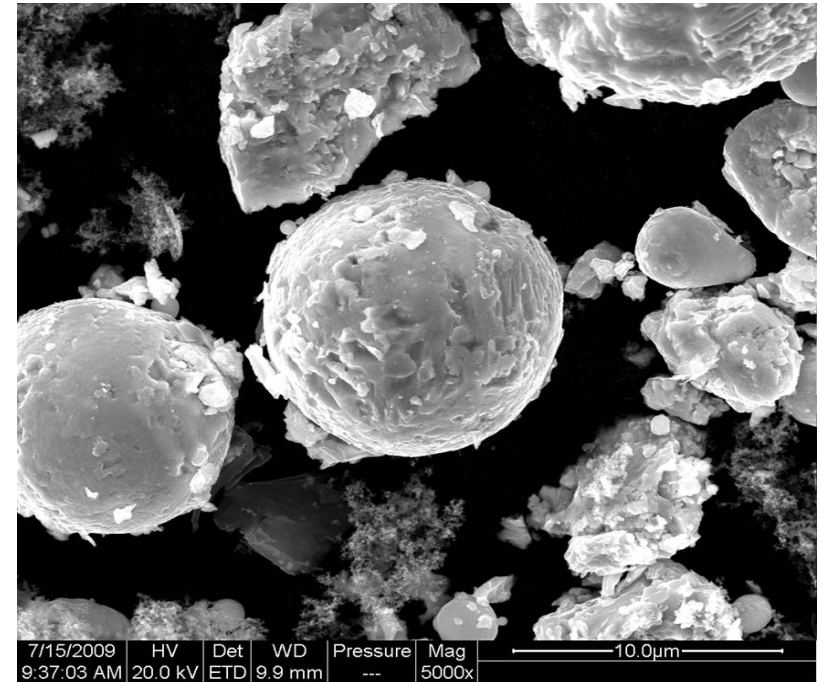
- Calculations based on Paul Nelson's Battery Design Model (Argonne)
- No 30% power margin was used in these predictions



# Obtained $\text{Cu}_6\text{Sn}_5$ Sample from Vendor



SEM photo of  $\text{Cu}_6\text{Sn}_5$  powder as received.

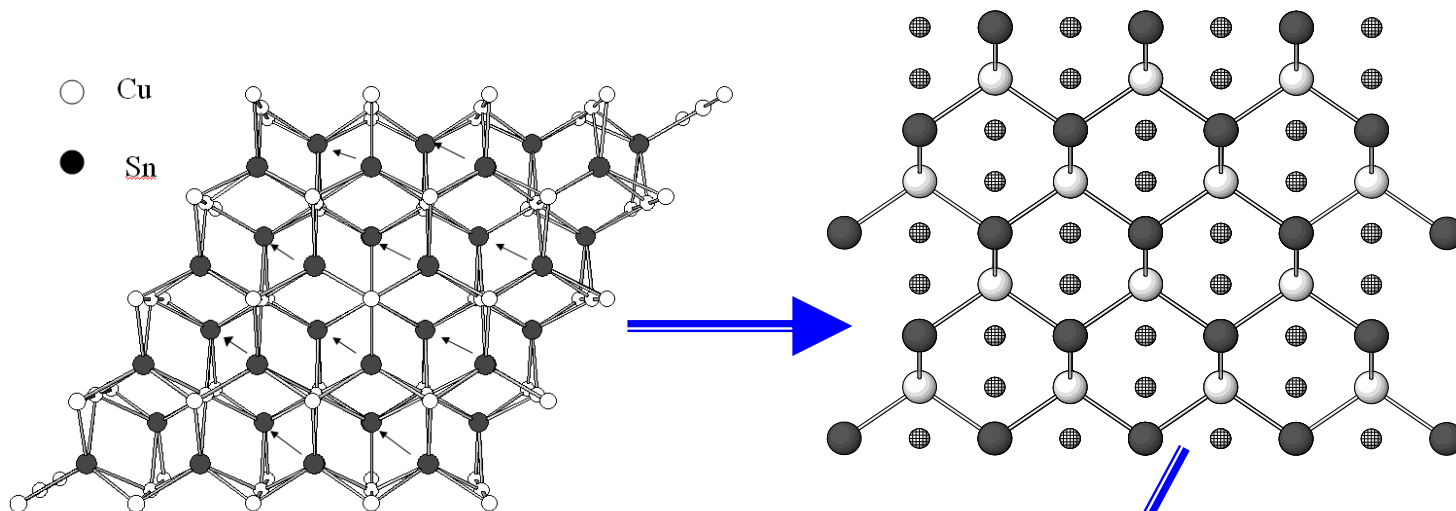


SEM photo of  $\text{Cu}_6\text{Sn}_5$  powder blended on roller mill with acetylene black carbon and SFG-6 graphite.

- Study was initiated with this sample due to its high tap density.



# Significant Lattice Changes Occur Upon Lithiation

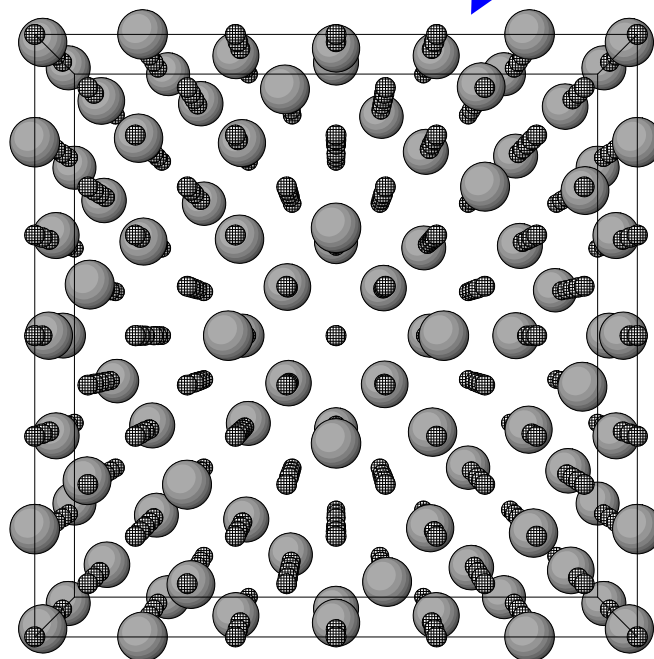


$\text{Cu}_6\text{Sn}_5$

| Atoms | Length |
|-------|--------|
| Sn-Sn | 5.12 Å |
| Cu-Cu | 2.52 Å |
| Cu-Sn | 2.82 Å |

$\text{Li}_2\text{CuSn}$   
+ 1 Cu for every 5 Sn

| Atoms | Length |
|-------|--------|
| Sn-Sn | 4.44 Å |
| Cu-Cu | 4.44 Å |
| Cu-Sn | 2.72 Å |



$\text{Li}_{17}\text{Sn}_4$   
+ 6 Cu for every 5 Sn

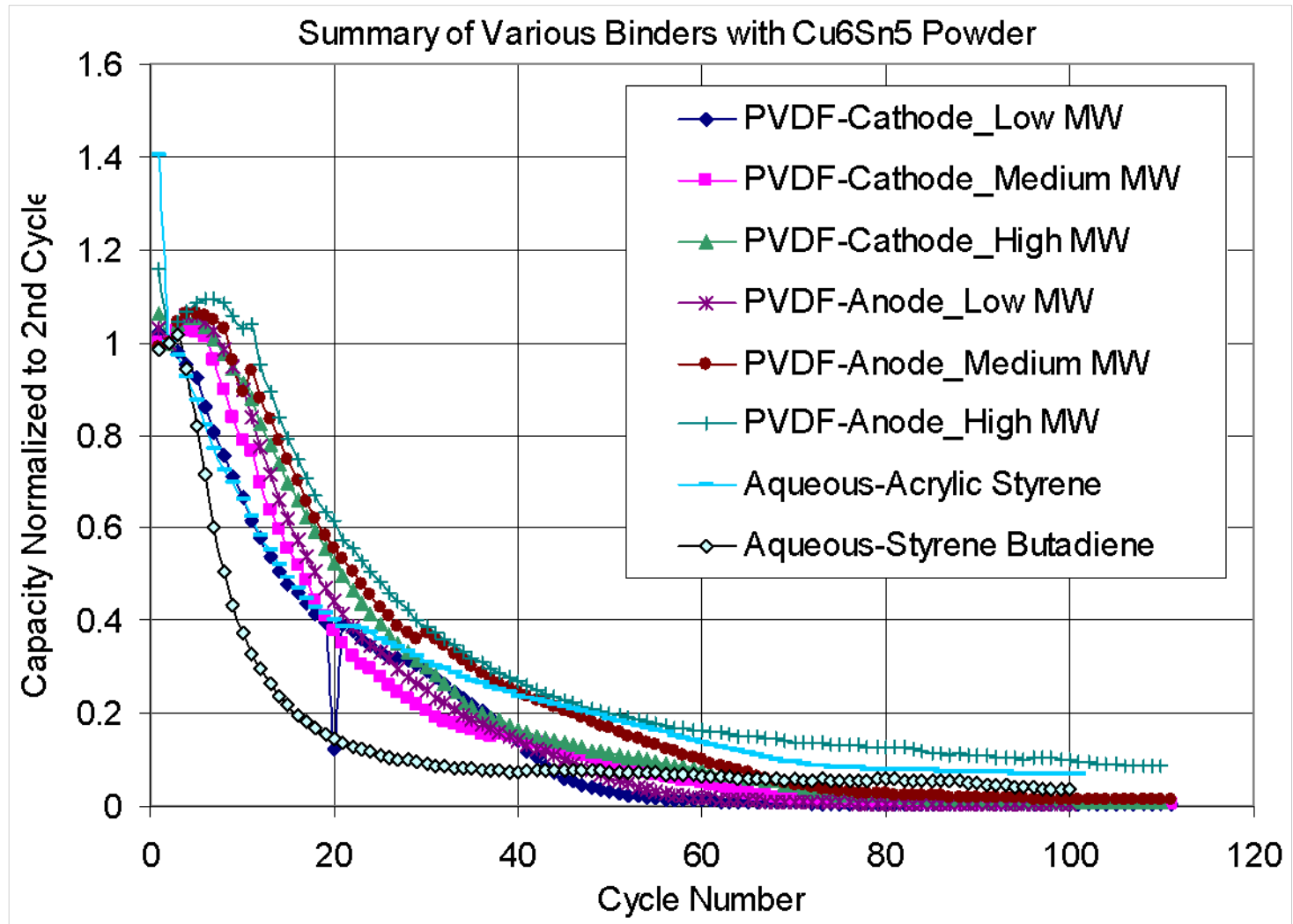
| Atoms | Length |
|-------|--------|
| Sn-Sn | 5.0 Å  |

# Elastic Binders Are Needed

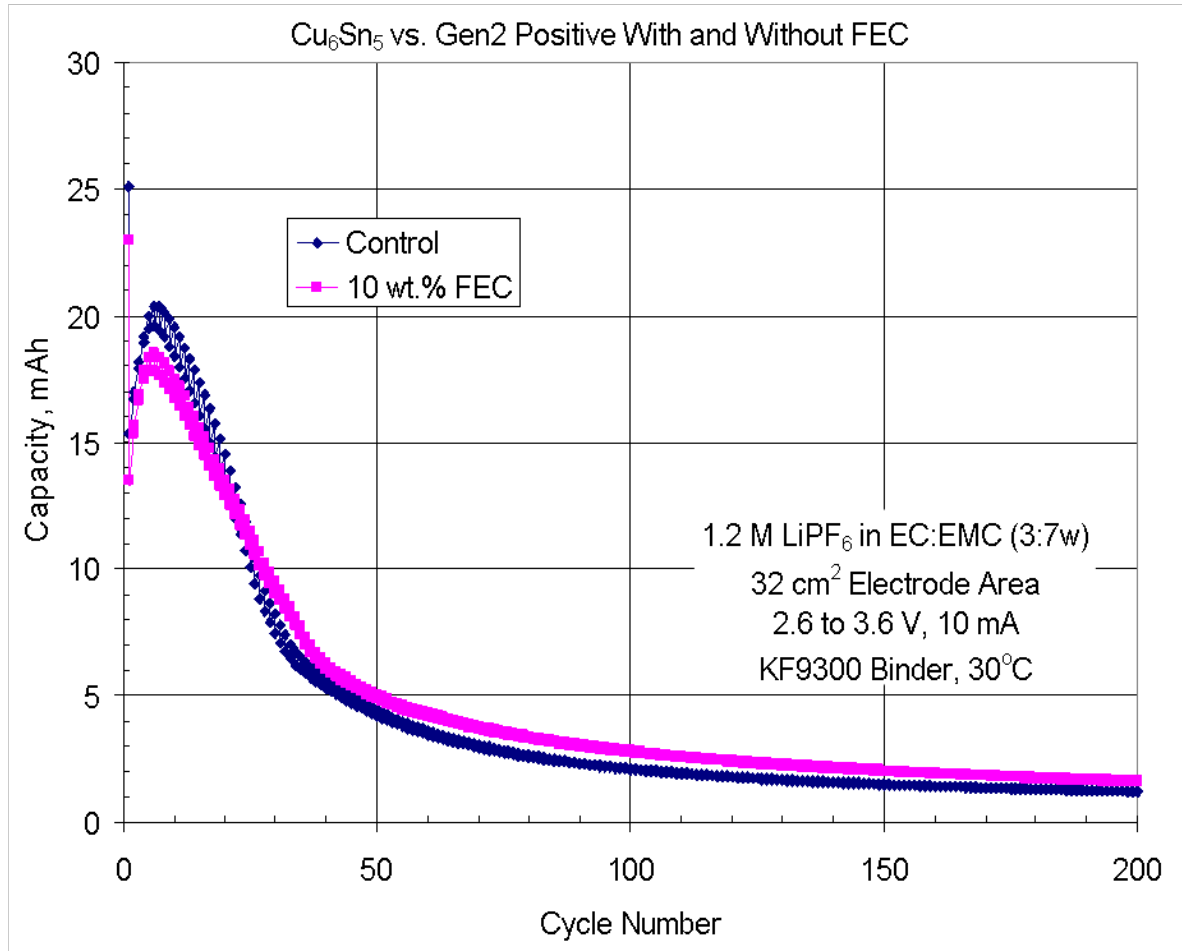
- Binder and electrode recipes have been optimized for graphite, which has ~10% volume expansion upon lithiation
- Little effort has been applied to the intermetallic anode materials where the volume fluctuates by nearly 200%
- Several classes of commercial binders were identified and evaluated with the sourced  $\text{Cu}_6\text{Sn}_5$  powder
- Solid anode additives (alumina, magnesia, and graphite) were also explored to see if they impeded the agglomeration of displaced copper



## Choice of Binders Did Not Enhance Capacity Retention (for this powder sample)



# Electrolyte Additive (FEC) Not Enough in This Case



- FEC was shown to be effective in other intermetallic efforts at Argonne
- This particular  $\text{Cu}_6\text{Sn}_5$  morphology or size may not be suitable for battery electrodes



# Volume Expansion Is a Concern

- Full lithiation of  $\text{Cu}_6\text{Sn}_5$  may not be practical due to the large volume change.
  - Can this volume fluctuation be designed into the particle and/or electrode?

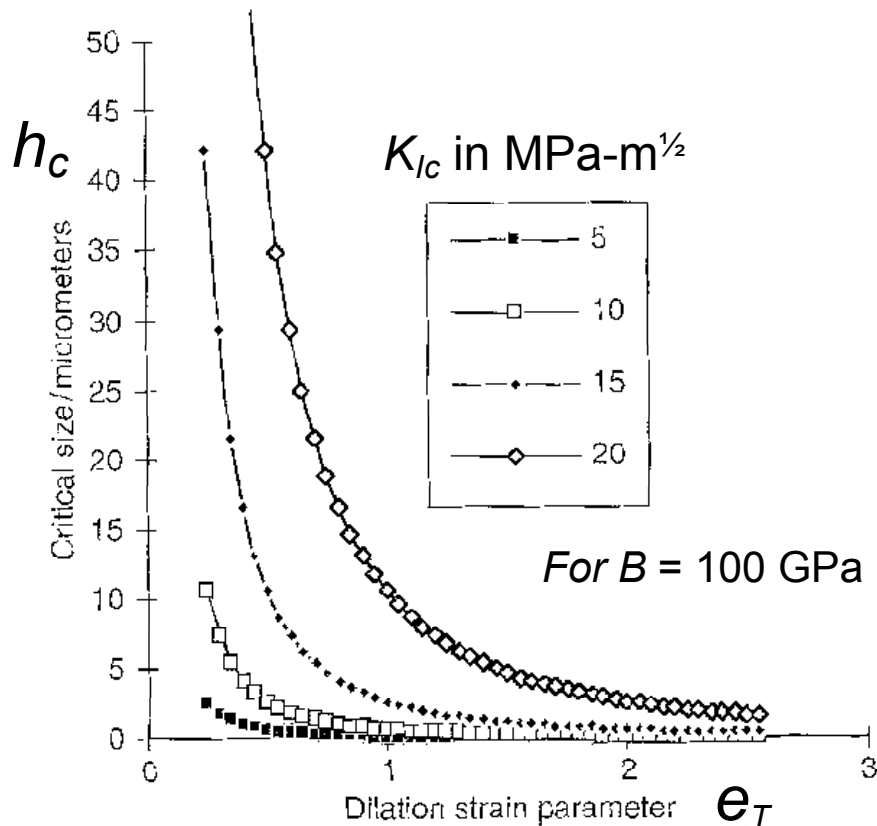
| Phase*                           | Volume per Sn Atom, Å <sup>3</sup> |
|----------------------------------|------------------------------------|
| Sn                               | 34.2                               |
| LiSn                             | 41.1                               |
| Li <sub>7</sub> Sn <sub>3</sub>  | 61.2                               |
| Li <sub>5</sub> Sn <sub>2</sub>  | 64.3                               |
| Li <sub>13</sub> Sn <sub>5</sub> | 65.5                               |
| Li <sub>7</sub> Sn <sub>2</sub>  | 80.3                               |
| Li <sub>17</sub> Sn <sub>4</sub> | 95.4                               |

| Phase                                    | Unit Cell(s)                                               | Volume of Unit Cell, Å <sup>3</sup> | Volume per Sn Atom, Å <sup>3</sup> |
|------------------------------------------|------------------------------------------------------------|-------------------------------------|------------------------------------|
| $\text{Cu}_6\text{Sn}_5$                 | $\text{Cu}_{24}\text{Sn}_{20}$                             | 782                                 | 39.1                               |
| Li <sub>2</sub> CuSn<br>+ Cu             | Li <sub>8</sub> Cu <sub>4</sub> Sn <sub>4</sub><br>+ 0.8Cu | 245<br>+0.8(11.75)                  | 63.6                               |
| Li <sub>17</sub> Sn <sub>4</sub><br>+ Cu | Li <sub>340</sub> Sn <sub>80</sub><br>+ 96Cu               | 7634<br>+96(11.75)                  | 109.5                              |

\*Adapted from R.A. Huggins and W.D. Nix, *Ionics* **6** (2000) p. 57-63.



# Huggins' Critical Particle Size Model



R.A. Huggins and W.D. Nix, "Decrepitation Model For Capacity Loss During Cycling of Alloys in Rechargeable Electrochemical Systems", *Ionics* **6** (2000) p. 57-63.

- The model work of Huggins suggests a particle size of 0.2  $\mu\text{m}$  is preferred for pure Sn as a starting material.
- Intermetallic alloys provide an opportunity to increase the fracture toughness and decrease the elastic modulus of metal anodes through alloying with additional metals and phases.

$$h_c \approx \frac{23}{\pi} \left( \frac{3K_{Ic}}{Be_T} \right)^2$$

$h_c$  is critical size in  $\mu\text{m}$

$K_{Ic}$  is fracture toughness in MPa-m<sup>1/2</sup>

$B$  is elastic modulus in GPa

$e_T$  is strain dilation ( $\Delta V/V$ )



# Determine Mechanical Properties of Intermetallic Alloys

## Elastic modulus (Universal Materials Testing Machine (Instron))

- Measurements were made from stress strain plots obtained during four-point-bend tests using rectangular bars of the test material
- Outer fiber stress and associated strain were obtained from standard elastic beam theory
- Slope of the stress vs. strain plot gave the elastic modulus of the material

## Fracture toughness (Single Edged Notched Bend (SENB))

- Single-edged notched beam test was used for fracture toughness evaluations
- Thin wafering blade was used to notch the samples such that the notch depth to sample thickness was  $\sim 0.5$
- Samples were tested in three-point bend loading configuration at a constant displacement rate
- Fracture toughness was determined from the peak load at failure, sample dimensions, and a standard fracture mechanics relationship



# Results of Mechanical Testing on Cast Bars

| Alloy                             | Strength (MPa) | Modulus (GPa) | Fracture Toughness (MPa m <sup>0.5</sup> ) |
|-----------------------------------|----------------|---------------|--------------------------------------------|
| Cu <sub>6</sub> Sn <sub>5</sub>   | 79±14          | 41.1±4.4      | 2.19±0.54                                  |
| NiCu <sub>5</sub> Sn <sub>5</sub> | 41.0±7.5       | 65.9±8.5      | 1.32±0.13                                  |
| ZnCu <sub>5</sub> Sn <sub>5</sub> | 93.0±8.9       | 46.0±6.2      | 2.56±0.23                                  |
| FeCu <sub>5</sub> Sn <sub>5</sub> | 78.9±7.0       | 52.19±0.89    | 2.38±0.15                                  |
| Cu <sub>6</sub> Sn <sub>6</sub>   |                |               |                                            |
| Li <sub>2</sub> CuSn              |                |               |                                            |

Strength: four-point bend test

Elastic modulus: four-point bend test

Fracture toughness: notched samples tested in 3-point bend





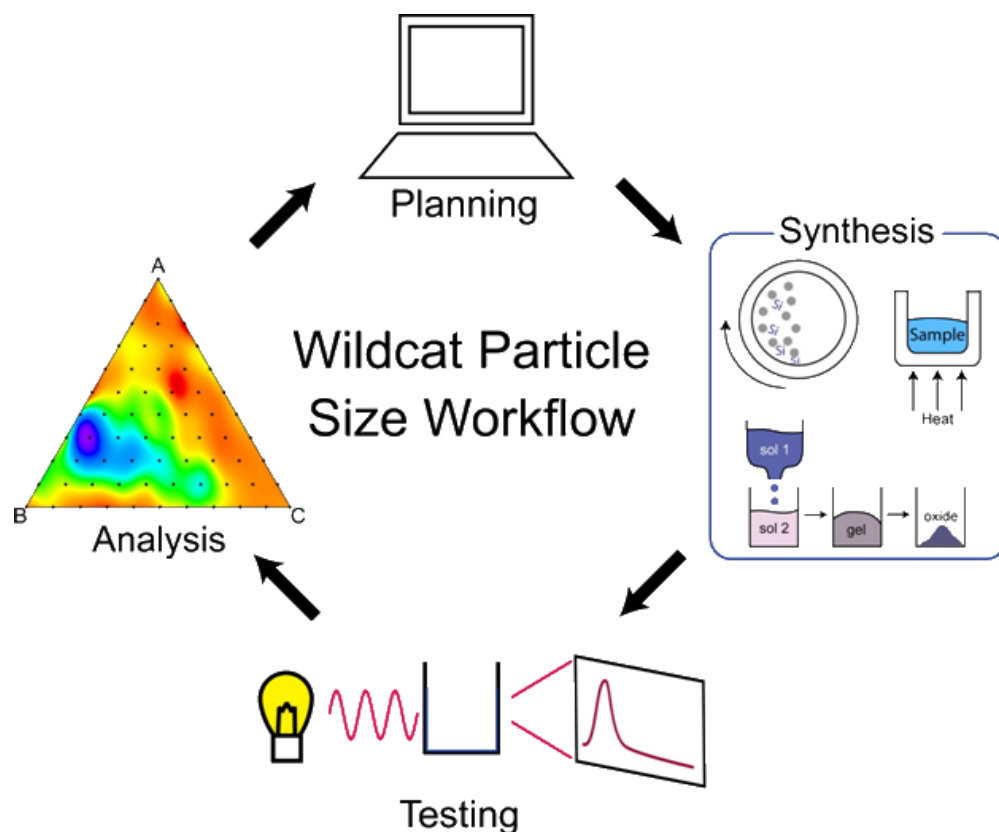
# Intermetallic Particles Must Be Sub-micron in Size

| Intermetallic Alloy        | $10\text{Li} + \text{MCu}_5\text{Sn}_5 \leftrightarrow 5\text{Li}_2\text{CuSn} + \text{M}$ |                             | $85\text{Li} + 4\text{MCu}_5\text{Sn}_5 \leftrightarrow 5\text{Li}_{17}\text{Sn}_4 + 20\text{Cu} + 4\text{M}$ |                             |
|----------------------------|--------------------------------------------------------------------------------------------|-----------------------------|---------------------------------------------------------------------------------------------------------------|-----------------------------|
|                            | Critical Particle Size, $\mu\text{m}$<br>( $eT = 0.63$ )                                   | Theoretical Capacity, mAh/g | Critical Particle Size, $\mu\text{m}$<br>( $eT = 1.8$ )                                                       | Theoretical Capacity, mAh/g |
| $\text{Cu}_6\text{Sn}_5$   | 0.47                                                                                       | 257                         | 0.058                                                                                                         | 507                         |
| $\text{NiCu}_5\text{Sn}_5$ | 0.067                                                                                      | 258                         | 0.0082                                                                                                        | 510                         |
| $\text{ZnCu}_5\text{Sn}_5$ | 0.51                                                                                       | 256                         | 0.063                                                                                                         | 507                         |
| $\text{FeCu}_5\text{Sn}_5$ | 0.35                                                                                       | 259                         | 0.042                                                                                                         | 511                         |
| $\text{Cu}_6\text{Sn}_6$   |                                                                                            |                             |                                                                                                               |                             |
| $\text{Li}_2\text{CuSn}$   |                                                                                            |                             |                                                                                                               |                             |



# High Throughput Particle Size Control

- Contracted Wildcat Discovery Technologies to synthesize  $\text{MCu}_5\text{Sn}_5$  samples (100 g) with controlled particle size
  - High throughput materials discovery company
  - Specialty synthesis
- Wildcat performed a high throughput screen to identify reaction conditions for target particle size
- In 2 weeks, ran ~150 reactions
- Tested
  - Milling conditions
  - Process control agents
  - Reagents



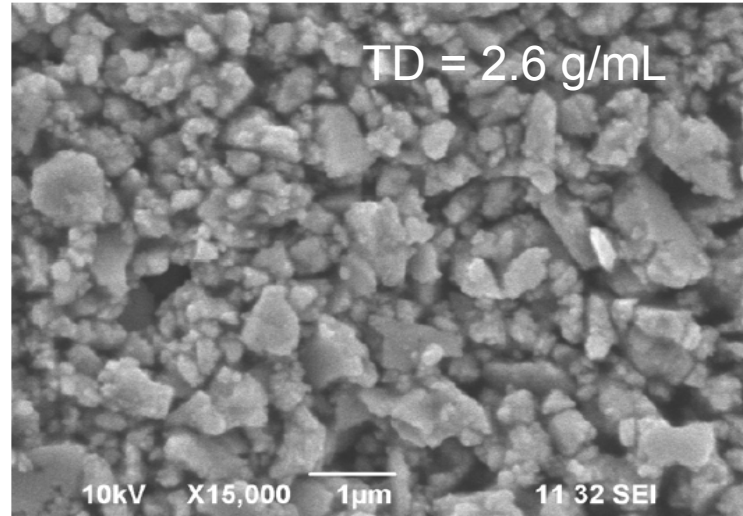
# Materials Successfully Synthesized by Wildcat Discovery Technologies



*Sample 4*

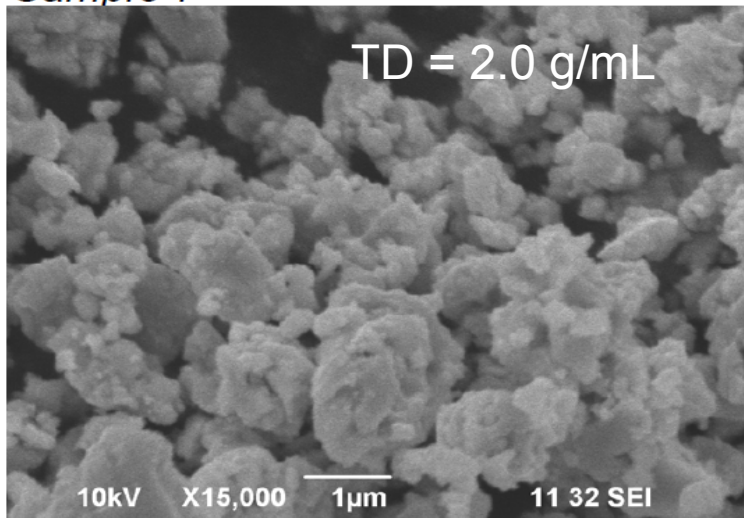
Variety of morphologies induced

- Primary particle size (<100 nm to micron)
- Porous and dense structures

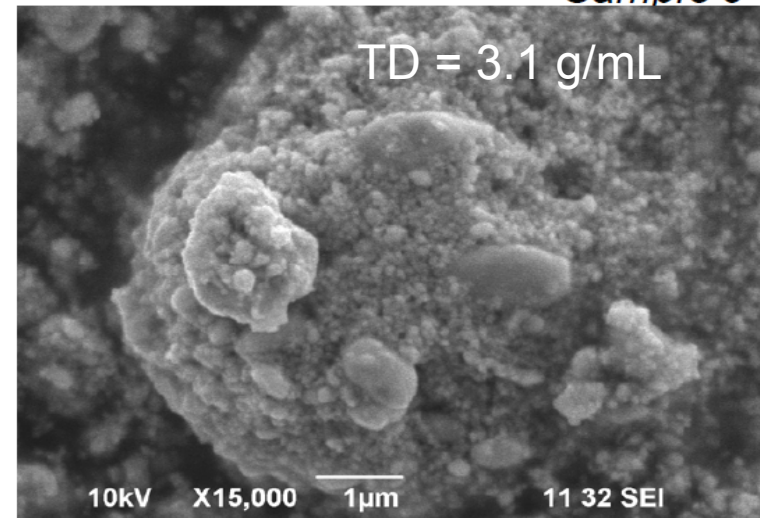


Selected Method #4 for its primary particle size and separation

*Sample 1*



*Sample 6*



# Future Work

- Now in the process of testing  $M_yCu_5Sn_5$  alloys with 0.5  $\mu m$  particle size from Wildcat Discovery Technologies for  $M = Cu, Ni, Zn, Fe,$  and  $Sn$
- Revisit the influence of elastic binders with new smaller intermetallic alloys
- Explore the subject of critical particle size based on Huggins work by making alloy casts of lithiated intermetallic alloys and evaluating their mechanical properties
- Continue search for additives that promote copper retention at the particle level and electrode level
  - Influence of grain size
- Revisit electrolyte additive study to enhance SEI formation on new smaller intermetallic electrodes
- Monitor energy density of final electrode design to compare against graphite/carbon electrodes



# Summary

- Explored the subject of critical particle size based on Huggins work by making alloy casts of intermetallic alloys and evaluating their mechanical properties
- Developed coating process to make electrodes with varying thickness of  $\text{Cu}_6\text{Sn}_5$  to establish baseline
- Identified metals supplier to help in development of intermetallic alloys of varying particle size and morphology
- Evaluated the influence of conductive and resistive additives to electrode powder mix in an attempt to minimize copper migration
- Expanded Argonne's Battery Design Model to assess the benefit of using intermetallic alloys in PHEV batteries
- Obtained numerous samples of electrode binders for binder optimization study



# Contributors and Acknowledgments

- Jack Vaughey (Argonne)
- Dileep Singh (Argonne-NE)
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