# **T**hermo**E**lectric **P**ower **S**ystem **S**imulator **(TEPSS)**

**Sponsored by NYSERDA's Industrial Research and Development Program**

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**2011 DOE Thermoelectrics Applications Workshop January 3 - 6, 2011 San Diego, CA** 





## RIT Sustainable Energy Lab

**Overall Goal:** To model, test, and design thermoelectric modules and systems for current and future power generation applications.





**Material Science & Engineering (nano vs. bulk)**











### **Overview**

- Motivation
- TEPSS Overview/Architecture
- Component and Node Modeling
- Optimization Shell
- Thermoelectric Power Unit Component
- Proof of Concept
- Conclusion/Remarks





## Motivation

### Benefits

- Modular, scalable (mW  $\rightarrow$  kW...)
- Solid-state, no moving parts
- Operate over a range of temperatures
- Transient thermal sources
- Minimal maintenance
- No noise, vibration

### Niche Applications

- Car exhaust
- Woodstoves, cookstoves
- Remote power
- Sensors
- Radioisotope thermoelectric generator



greencar.com



TEGPower.com

globalte.com







[micropelt.](http://www.micropelt.com/applications/te_power_one.php)com





## Motivation

- Over 50 quadrillion BTUs of waste heat generated each year.
- Recovering just 1% would power New York indefinitely.
- Improved TE materials, increased efficiency  $\rightarrow$  smaller heat sinks.
- Trade-offs:
	- high ZT vs. cost
	- high ∆T vs. ∆P, weight, volume, cost
- Currently specific device and system models exist.
- Need to integrate material properties, engineering thermal modeling, and economics.







## TEPSS Project Goal

*Create a versatile tool to evaluate whether or not thermoelectrics are currently or will soon become technically and economically viable for a specific application and if so determine what the optimal system might look like.*

- The tool should help quickly assess a range of potential applications for waste heat recovery using emerging thermoelectric materials.
- Most current thermoelectric modeling is geared towards very specific applications and may not consider system trade-offs.
- Historically module and system design have been loosely coupled.



### TEPSS Overview

Requirements

- Solve system of equations for the system steady operating state
- Unlimited system concepts defined by user
- Objective function is defined by the user
- Optimizes system configuration with respect to user defined design variables
- Open source and expandable
- Easy to use, modify, and reuse

### Challenges

- Energy components are a combination of empirical, analytical or FE/FD models
- Often highly nonlinear system of component models
- System of equations changes for each user defined concept



### TEPSS Architecture

- What are energy systems?
	- Independent (modular) components
		- Components contain models and independent of rest of system
	- Interconnected by nodes



### TEPSS Architecture





- Object oriented programming (Matlab)
- Components contain engineering models
	- Mass, energy conservation, performance data
- Components are linked together by nodes
	- Nodes provide component boundary conditions.
	- Nodes belong to a specific *domain* (fluid, mechanical rotation, electrical, etc.).



### Component Equations and Errors

Conservation of mass

Conservation of energy

$$
\dot{m}_{in} - \dot{m}_{out} = 0
$$
\n
$$
\dot{m}_{in} - \dot{m}_{out} = e(1)
$$
\n
$$
Q_{in} - \dot{m}Cp\Delta T = 0
$$
\n
$$
Q_{in} - \dot{m}Cp\Delta T = e(2)
$$
\n
$$
\Delta P + k\dot{m}^2 = 0
$$
\n
$$
\Delta P + k\dot{m}^2 = e(3)
$$

Viscous dissipation

Collect errors, use root finding<br>algorithm to set = 0.<br> $e = [e(1), e(2), e(3), ..., e(n)]$ 



algorithm to set  $= 0$ .

### Node Domains

- Through and Across variables
- Fluid domain (fluidprop.tudelft.nl/)









### Steady State Simulation

Systems of nonlinear equations solved iteratively with Newton's Method:

$$
\Delta x_{i} = -[J(x_{i})]^{-1} \times f(x_{i})
$$
\n
$$
x_{i+1} = x_{i} + \Delta x_{i}
$$
\n
$$
[J(x_{i})] = \begin{bmatrix} \frac{\partial f_{1}}{\partial x_{1}} & \cdots & \frac{\partial f_{1}}{\partial x_{m}} \\ \vdots & \ddots & \vdots \\ \frac{\partial f_{n}}{\partial x_{1}} & \cdots & \frac{\partial f_{n}}{\partial x_{m}} \end{bmatrix}
$$

*i* is iteration number, *x* and *f* are vectors,  $[J(x_i)]$  is Jacobian Matrix at *xi*





### TEPSS Architecture



 $\frac{\Delta V}{\Delta}$ 



### General Cost Function

- Common cost metrics
	- Simple payback (added cost/net savings per year)
	- Cost per unit energy output
	- Emissions per unit energy output

$$
\text{cost} = \frac{\sum_{i=1}^{n} A_i + t \sum_{i=1}^{n} B_i + t \sum_{i=1}^{n} ([C_i][U])}{\sum_{i=1}^{n} D_i + t \sum_{i=1}^{n} E_i + t \sum_{i=1}^{n} ([F_i][V])} + \sum_{i=1}^{n} \Phi
$$

 $n =$  number of components *A-F*, *U*, *V* and  $t =$  user inputs  $\Phi$  = user defined penalty function



# User Inputs

- Solver inputs
	- components and nodes
	- interconnections (system concept)
	- initial guesses
	- boundary conditions
	- convergence criteria
- Component parameters
- Optimization inputs
	- design variables
	- upper and lower bounds
	- convergence criteria
- Cost function

```
solver inputs.fstr = '{compressor(parameters.compressor), tepowerun
 %create the nodes by assigning a cell in cell array n to the class
 %definition of the node domain.
\exists for i=1:6
     solver inputs.n{i} = fluid('N2, 02, CH4', [.7466, .1985, .0549], 'Gas
 end
 solver inputs. n\{7\} = mechrot;
 solver inputs.n\{8\} = mechrot;
```
#### %p Leg

```
parameters.tepowerunit.module.rho p=8e-6; %ohm*m
parameters.tepowerunit.module.alpha p=2e-4; %V/K
parameters.tepowerunit.module.k p=1.5;%w/(m*k)
parameters.tepowerunit.module.1 p=.005; %m
parameters.tepowerunit.module.area p=(1.397e-3)^2;% for 1 leg
```


# Thermoelectric Power Unit Component





- Counter and parallel flow using any combination of fluids as well as isothermal or constant heat flux configurations.
- Independently specified heat sink type and geometry (aligned and staggered plates, pin fins), material, fin pitch, and contact resistances.
- Pressure drop models for all configurations
- Thermal coupling with surrounding environment.
- Module layout in zones, series, and parallel.
- Heat spreading accounted for using modified model developed by Ellison. (G.N.Ellison, *IEEE Trans. on Comp. & Packaging Tech.,* 2003)





### Thermoelectric Power Unit Zone

- 12 equations for each zone represent various energy balances and the standard TEM models
- Set of equations are nonlinear and solved internally using numerical techniques to obtain heat flows and temperatures throughout the system and final power recovered by each zone.

$$
q_{ins(j)} = \frac{T_{H(j)} - T_{C(j)}}{R_{ins}}
$$
  
\n
$$
q_{comb,H(j)} = \frac{\Delta T_{lm,H(j)}}{R_{cond,H}}
$$
  
\n
$$
q_{H(j)} = \frac{T_{H(j)} - T_{C(j)}}{R_{ih}} - \frac{1}{2} I_{(j)}^2 R_e + \alpha T_{H(j)} I_{(j)}
$$
  
\n
$$
q_{C(j)} = \frac{T_{H(j)} - T_{C(j)}}{R_{ih}} + \frac{1}{2} I_{(j)}^2 R_e + \alpha T_{H(j)} I_{(j)}
$$
  
\n
$$
I_{(j)} = \frac{\alpha (T_{H(j)} - T_{C(j)})}{R_e + R_{load}}
$$

 $R_{comb} = f$ f(fin type & material, geometry, flow rate, fluid type, heat spreading)



### Standard 1D Thermoelectric Model

 $q_H$ 

ЧС

 $x = 0$ 

 $T_H$ 

 $\overline{\boldsymbol{I}}_C$ 

 $\bm{P}_{TEM}$ 

• Multiple module model options:

$$
q_{H} = I \alpha_{p,n} T_{H} + K(T_{H} - T_{C}) - \frac{I^{2} R_{e}}{2}
$$

- experimentally measured values
- manufacturer specifications
- build from selected TE material properties, leg geometries, and contact resistances.

$$
K = n \left( \frac{A_p}{2R^{\prime \prime}_{c} + {}^{l}p} \bigg|_{\lambda_p} + \frac{A_n}{2R^{\prime \prime}_{c} + {}^{l}n} \bigg|_{\lambda_n} \right) \qquad R_e = n \left( \frac{\rho_p l_p + 2r^{\prime \prime}}{A_p} + \frac{\rho_n l_n + 2r^{\prime \prime}}{A_n} \right)
$$
\n
$$
\alpha_{p,n} = n(\overline{\alpha_p} - \overline{\alpha_n})
$$
\n
$$
R \cdot I \cdot J
$$

### Proof of Concept



- Power Unit Design Parameters:
	- 1.0 mm aligned plate fins, counter flow configuration
	- 10 zones, 12,500 4cm x 4cm modules (127 couples)
	- TE Properties: <sup>α</sup>*<sup>p</sup>* = -<sup>α</sup>*<sup>p</sup>* = 200 µV/K, λ*<sup>p</sup>* = λ*<sup>p</sup>* = 1.5 W/m∙K, <sup>ρ</sup>*<sup>p</sup>* = <sup>ρ</sup>*<sup>p</sup>* = 8e-6 Ω ∙m  $ZT \sim 2.5 \omega$ , 750K
	- Base area to module ratio of 9
	- Design parameters: channel height (3-12 cm) and fin density (4-24/module)
- Costs (materials, per leg pair, per module, fuel cost, 20 year  $\omega$  100% capacity)
- Cost function = additional cost per generated  $kWh_e$  above base system





### Proof of Concept







**Optimal Case:** *l = 6.03* **cm** *n = 13.9* **fins/module**  $W_{net} = 10.11 \text{ MW}$  $W_{TEG} = 121 \text{ kW}$  $Cost = 4.03$   $\ell$ /kWh *Cost function* =  $-14.12\%$ 



### Proof of Concept



# Closing Remarks

- TEPSS environment has been developed for simulating and optimizing thermoelectric power generation systems.
- TEPSS is expandable with reusable and customizable components.
- New node domains and components can be added to increase potential system concepts.
- TEPSS will allow for the exploration of suitable applications for emerging TE materials while coupling module level design with system level performance and economics.
- Working on more robust steady state solver and optimization options and developing more advanced component models.
- Interest in using/testing contact  $r$  iseme $\omega$ rit.edu





## Acknowledgements

- John Kreuder
- Andy Freedman
- NYSERDA (Contract #11135)

NYSERDA has not reviewed the information contained herein, and the opinions expressed in this presentation do not necessarily reflect those of NYSERDA or the State of New York.





### Sample Component Class

**classdef pump < handle** 

#### **properties (SetAccess=private)**

design variables component operating parameters end

# **Blower Nodes**

#### **methods**

**function obj = pump(parameters)**  component setup end

**function e = compute(obj, node1, node2, onoff)** engineering models end

#### **function component**  $\text{cost} = \text{cost}(\text{obj})$

component costing models end

#### **function y = paramcheck(obj)**

constraint and physical check models end





## Optimization in TEPSS

- **MATLAB** *fmincon* optimization algorithm *Constrained nonlinear optimization*
	- User supplies cost function
	- Simulation determines steady state
	- Cost function is evaluated at steady state
	- New parameters are chosen by *fmincon*
	- Repeat until cost function is minimized



