

Improving Efficiency and Load Range of Boosted HCCI using Partial Fuel Stratification with Conventional Gasoline

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Motivation



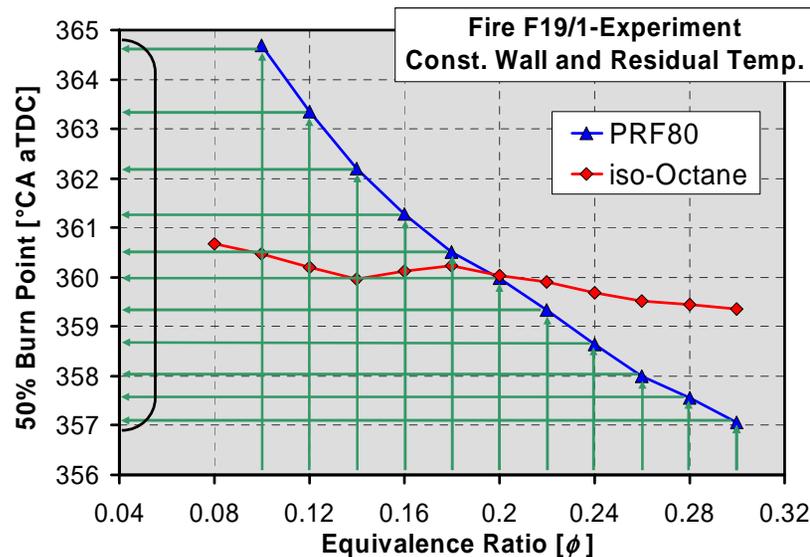
- Advanced engines using HCCI or HCCI-like combustion can provide both high efficiencies and very low emissions of NO_x and PM.
 - Limited max. power is a significant limitation to implementation of HCCI.
 - Recent results (SAE 2010-01-1086) show that intake boosting is a viable approach for extending the high-load limit of gasoline-fueled HCCI.
 - Achieved loads up to 16.3 bar IMEP_g without engine knock & ultra-low NO_x .
 - Knock controlled by retarding combustion phasing.
 - **Improvements are desirable in two key areas:**
 1. Reducing PRR with less combustion retard would allow higher loads with less boost.
 - > Greater operational flexibility and reduce pumping work for higher net eff.
 - > Increase exhaust enthalpy for a given boost, easing turbo-charger design.
 2. Even higher efficiencies could be achieved if less timing retard was required to control knock.
- Significant potential advantages to reducing PRR without timing retard.

Partial Fuel Stratification (PFS)



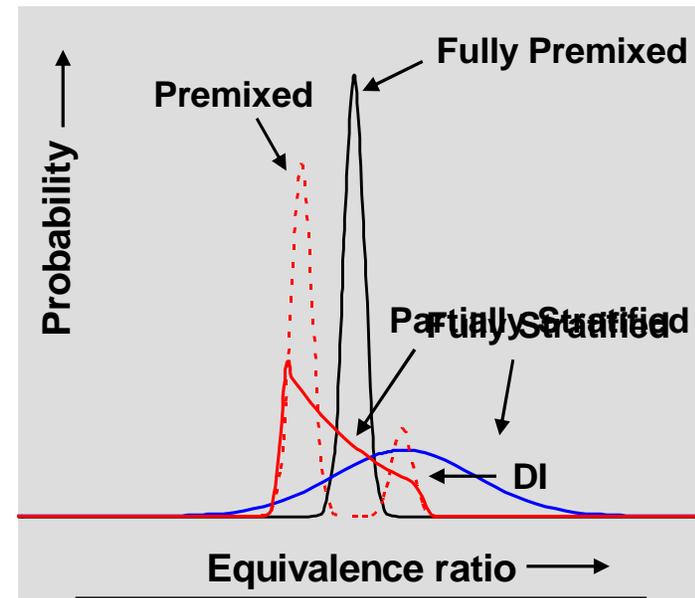
- One promising technique for reducing PRR is partial fuel stratification.
- Effective for controlling HRR (and PRR), but has two requirements:

1) Fuel autoig. must be ϕ -sensitive



Dec and Sjöberg, SAE 2004-01-0557

2) Appropriate ϕ -distribution



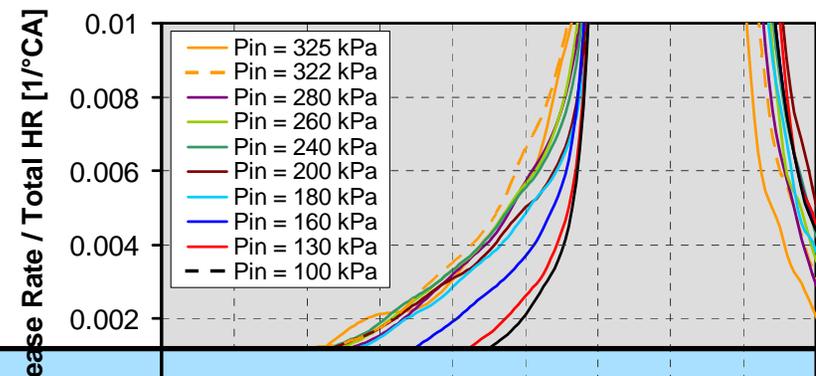
Sjöberg and Dec, SAE 2006-01-0629

- PRF80 is strongly ϕ -sensitive (2-stage ig.), iso-octane is not (1-stage-ig.)
- Partial fuel stratification (PFS) \Rightarrow most fuel premixed, up to 20% late DI.
 1. Good air utilization with leanest regions burning hot enough for good comb.
 2. Provides sufficient stratification.

PFS - Fuel Effects (ϕ -Sensitivity)



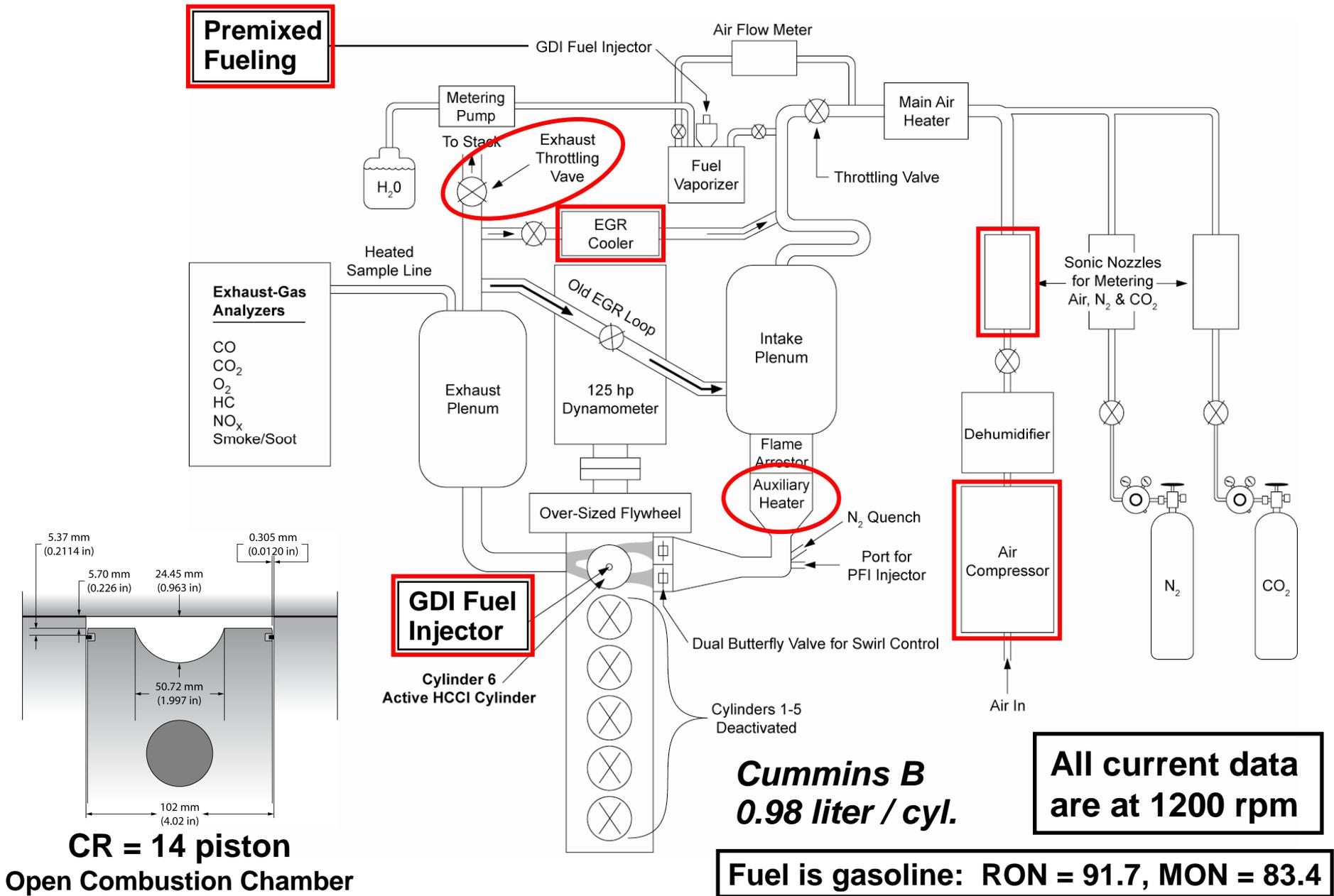
- Previous studies (naturally aspirated) have shown that PFS:
 - Reduces HRR for fuels with 2-stage ignition \Rightarrow high reactivity (ϕ -sensitive).
 - Ineffective for fuels with 1-stage ignition \Rightarrow low reactivity (not ϕ -sensitive).
- Our boosted HCCI results show intake boosting increased autoignition reactivity of conventional gasoline, but still single-stage ignition.
 - Enhances ITHR not LTHR.
- Increased reactivity suggests fuel may become ϕ -sensitive, \Rightarrow may be effective for PFS.



● Objectives:

1. Examine ϕ -sensitivity of gasoline \Rightarrow Naturally aspirated and Boosted.
2. Investigate effects of PFS on HRR and PRR.
 - > Vary amount of stratification \Rightarrow Sweep: 1) DI timing and 2) DI fraction.
3. Investigate potential of PFS for: 1) extending high-load limit, 2) improving efficiency of boosted HCCI.

HCCI All-Metal Engine and Subsystems



Operation and Terminology



- For boosted operation, increasing P_{in} enhances autoignition \Rightarrow overly advanced combustion, high PRR and knock.
 - Control by reducing intake temperature (T_{in}) and adding cooled EGR.
 - Minimum $T_{in} = 60^{\circ}\text{C}$ to prevent condensation of EGR-water or premixed fuel.
- For convenient comparison of data with the same charge dilution, but different EGR levels, we define:

$$\text{Equivalence ratio based on total charge mass} = \phi_m = \frac{(F / C)}{(F / A)_{stoich}}$$

- Acceptable maximum PRR varies with boost \Rightarrow use ringing intensity.

$$\text{Ringing Intensity} = \frac{1}{2\gamma} \cdot \frac{\left(0.05 \cdot \left(\frac{dP}{dt}\right)_{\max}\right)^2}{P_{\max}} \cdot \sqrt{\gamma R T_{\max}}$$

Eng, SAE 2002-01-2859

- Knock limit taken as Ringing = 5 MW/m².
 - \Rightarrow Corresponds to 8 bar/ $^{\circ}\text{CA}$ at 1200 rpm, $P_{in} = 1$ bar.

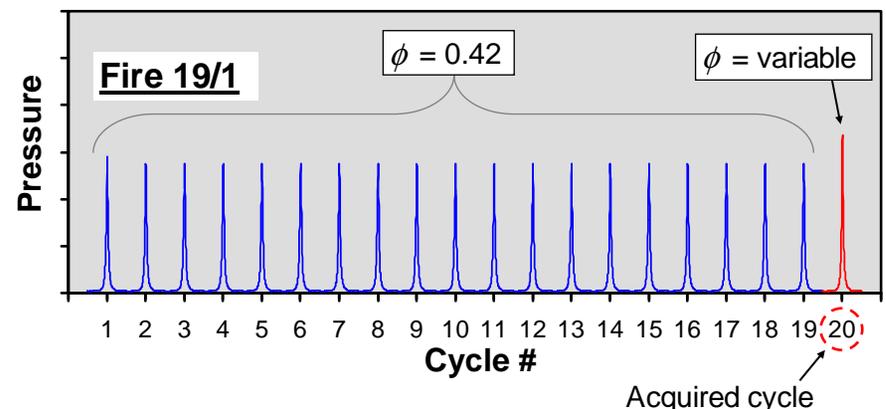
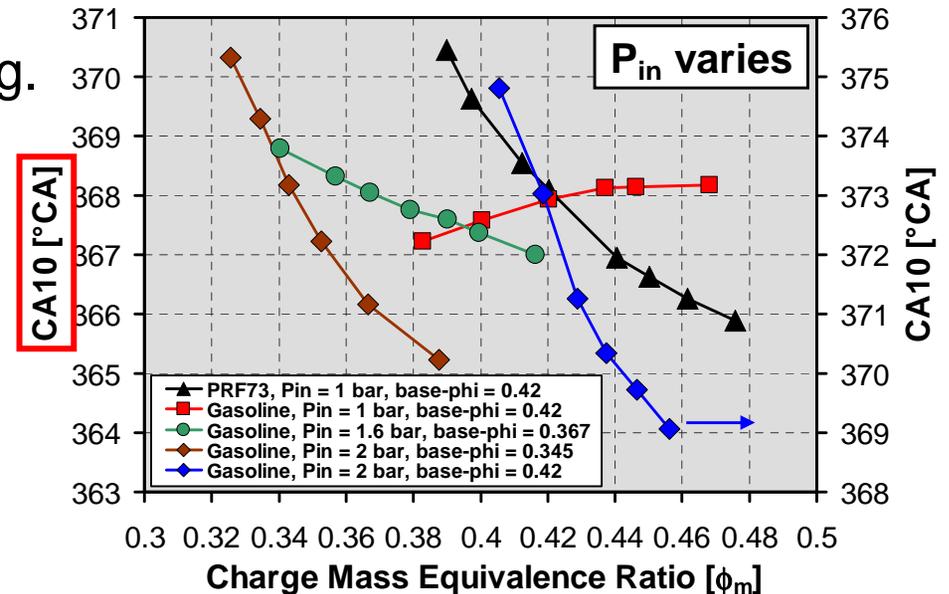


Φ -Sensitivity of Gasoline

- Use Fire19/1 technique to isolate fuel-chemistry effects from thermal effects.
 - Dec & Sjöberg *SAE 2004-01-0557*.
- Sweep ϕ above & below base fueling.
- PRF73 \Rightarrow 2-stage fuel with strong ϕ -sensitivity
(Yang *et al.*, *Proc. Combust. Inst.* 2011)

Gasoline:

- $P_{in} = 1$ bar \Rightarrow chemistry not ϕ -sensitive, γ effect dominates.
- $P_{in} = 2$ bar \Rightarrow strong ϕ -sensitivity, more than PRF73.
- $P_{in} = 1.6$ bar \Rightarrow intermediate ϕ -sensitivity.



- Gasoline autoignition strongly ϕ -sensitive w/ boost. Not for $P_{in} = 1$ bar.

Increase Stratification for $P_{in} = 1$ bar

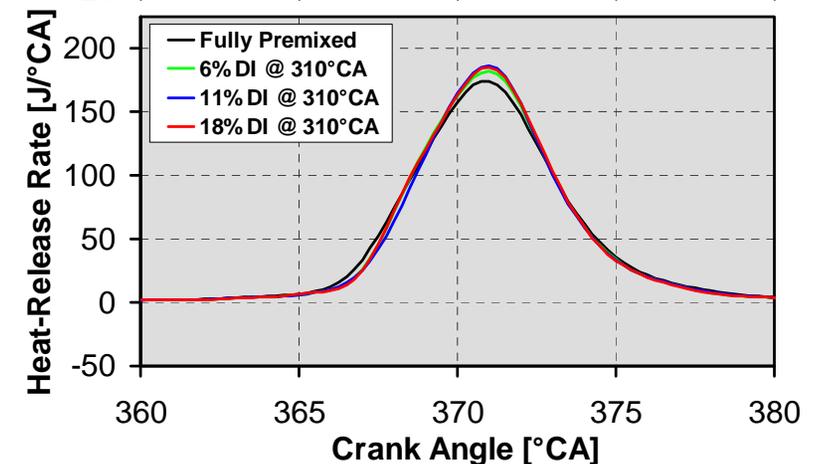
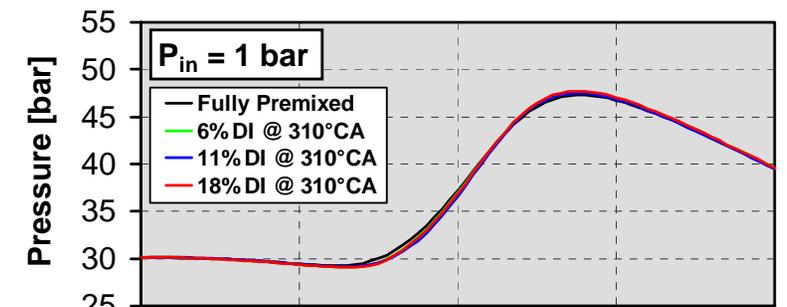
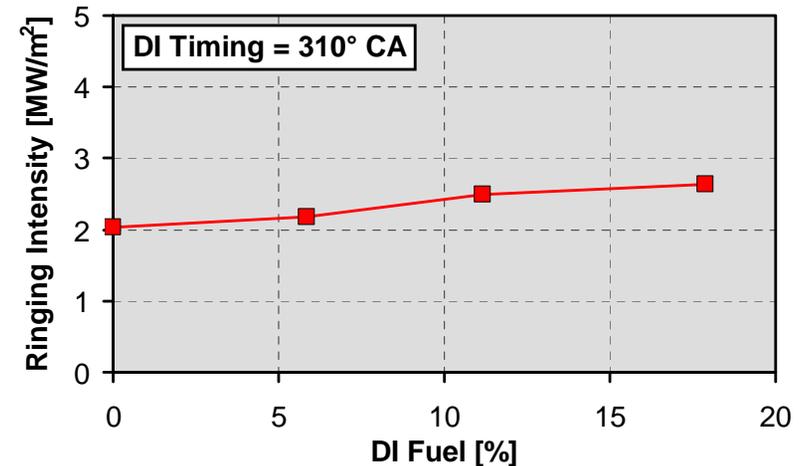
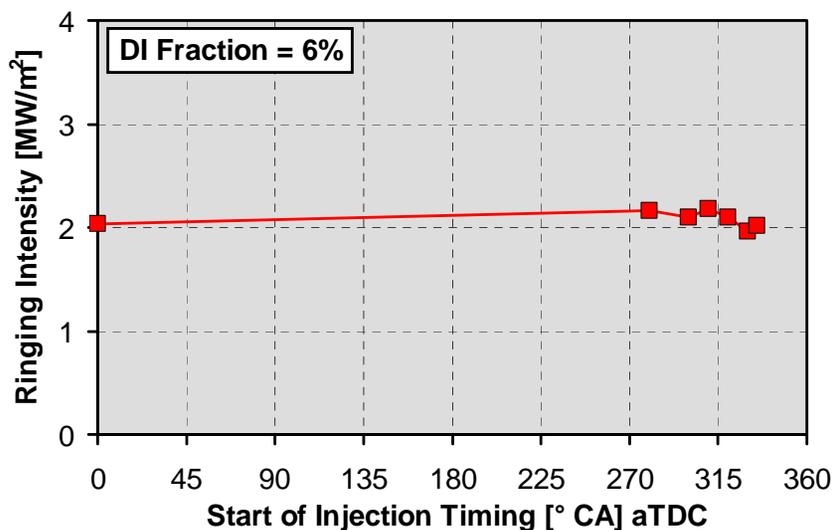


- Vary DI timing for const. 6% DI fueling.
 - Ringing ~ constant.
- Increase DI fraction; SOI = 310°CA.
 - Ringing increases slightly.

● Gasoline at $P_{in} = 1$ bar \Rightarrow PFS has no benefit for reducing max. PRR.

- Agrees with low ϕ -sensitivity.

Hold: $\phi_m = 0.44$, $T_{in} = 143^\circ\text{C}$, $CA50 = 371^\circ\text{CA}$

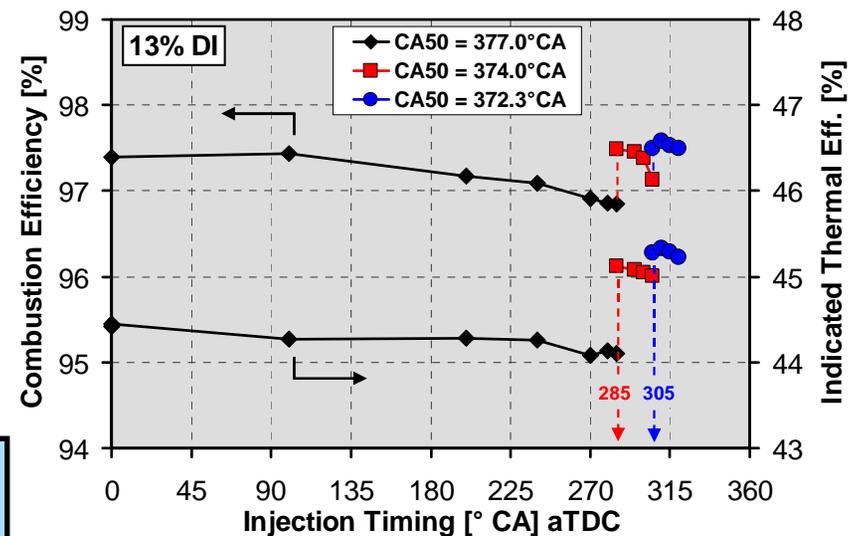
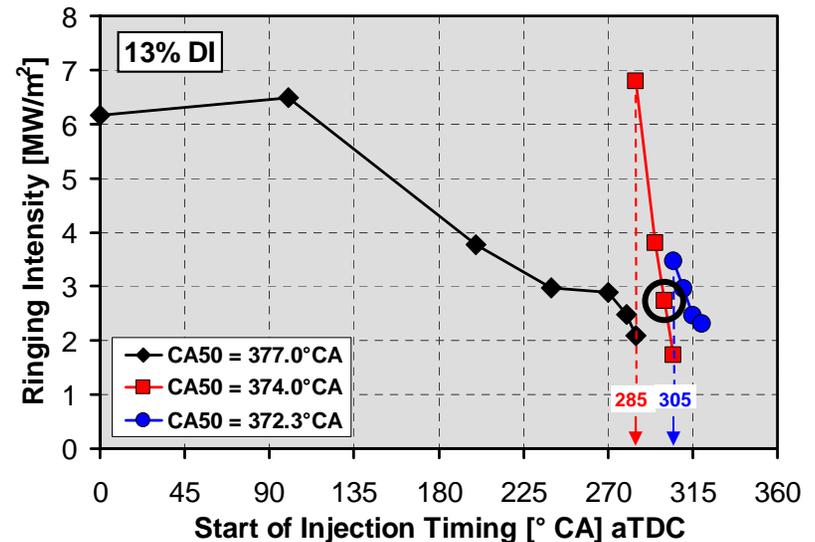


$P_{in} = 2$ bar: DI Timing Sweep with 13% DI



- High ϕ -sensitivity suggests PFS benefit.
- Retard DI timing to increase stratification.
 - Hold CA50 constant by varying EGR \Rightarrow piecewise ($15.4\% \leq O_2 \leq 14.0\%$).
- Dramatic reduction in ringing.
 - Initial **CA50 = 377°CA** for premixed, ringing ≈ 6 MW/m².
 - By SOI = 285°CA, $R \approx 2 \Rightarrow$ stability limit.
 - Advance to **CA50 = 374°CA** and further increase stratification with later SOI.
 - Advance to **372.3°CA** at SOI = 305°CA.
- Advancing CA50 improves combustion and thermal efficiencies.
- NOx and soot well below US-2010.

Hold: $\phi_m = 0.44$, $T_{in} = 60^\circ\text{C}$

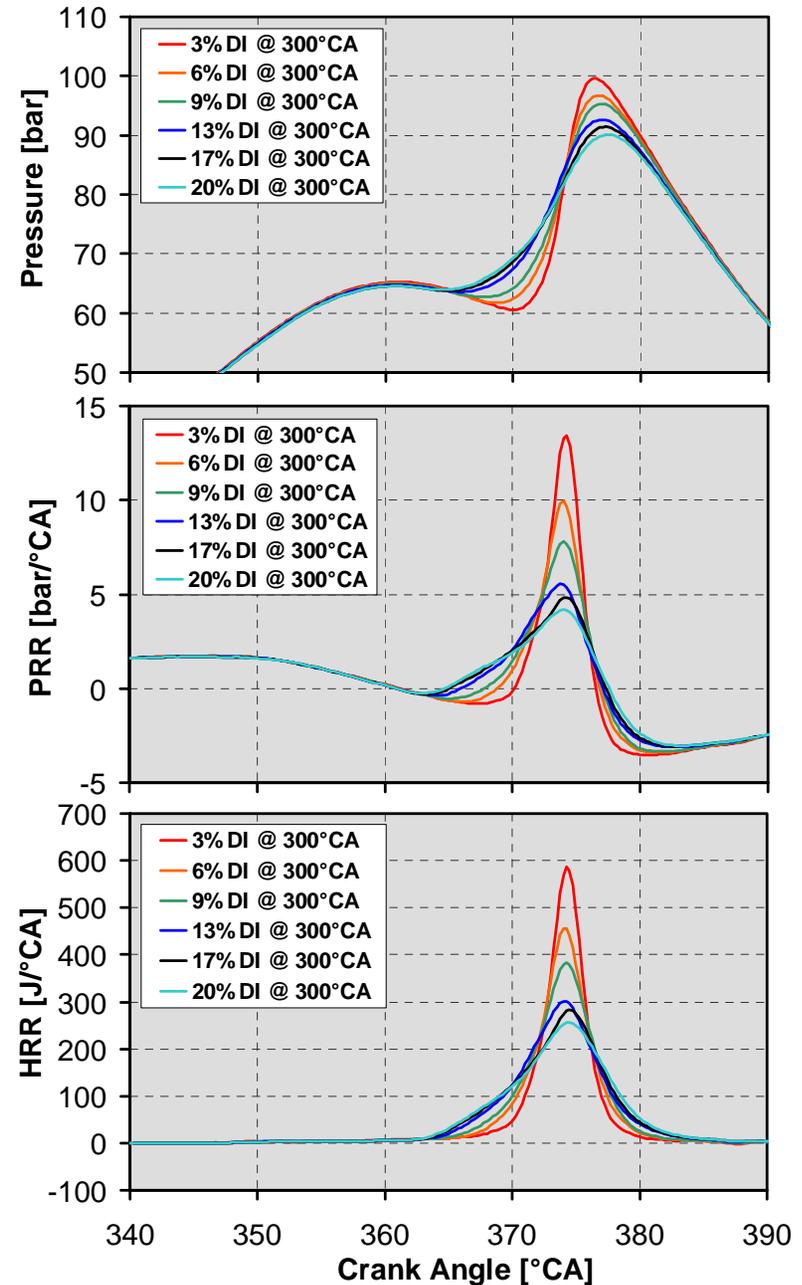
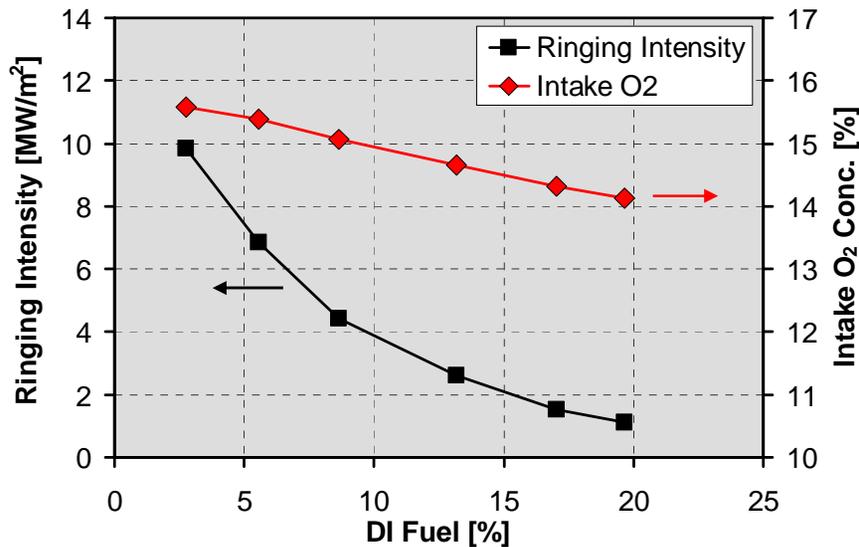


● PFS greatly reduces PRR_{max} (ringing) for gasoline boosted to $P_{in} = 2$ bar.

$P_{in} = 2$ bar: DI Fraction Sweep, SOI = 300°CA

- Large drop in ringing with increased DI%.
- Increased DI% \Rightarrow increased regions of higher $\phi_m \Rightarrow$ autoignite faster \Rightarrow advances hot ignition for same CA50.
 - Increases burn duration.
 - Reduces peak HRR, PRR_{max} , and P_{max} .
- Therm. Eff. \sim const., ultra-low NOx and soot, and COV of IMEP_g < 1.5%.

Hold: $\phi_m = 0.44$, $T_{in} = 60^\circ\text{C}$, CA50 = 374°CA

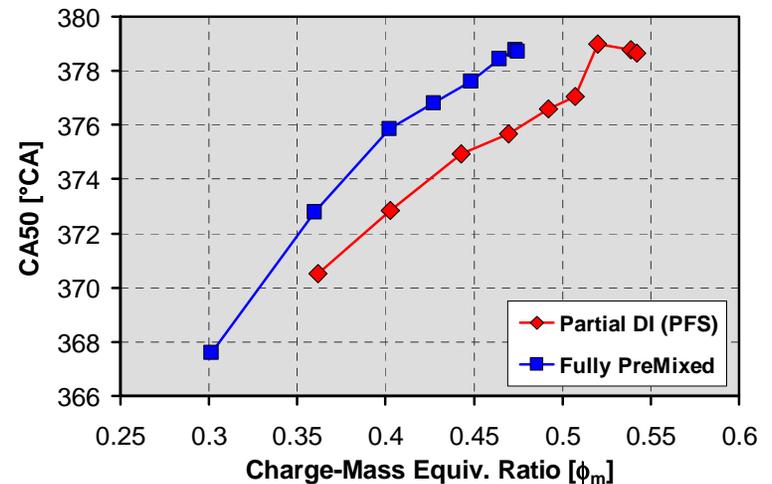
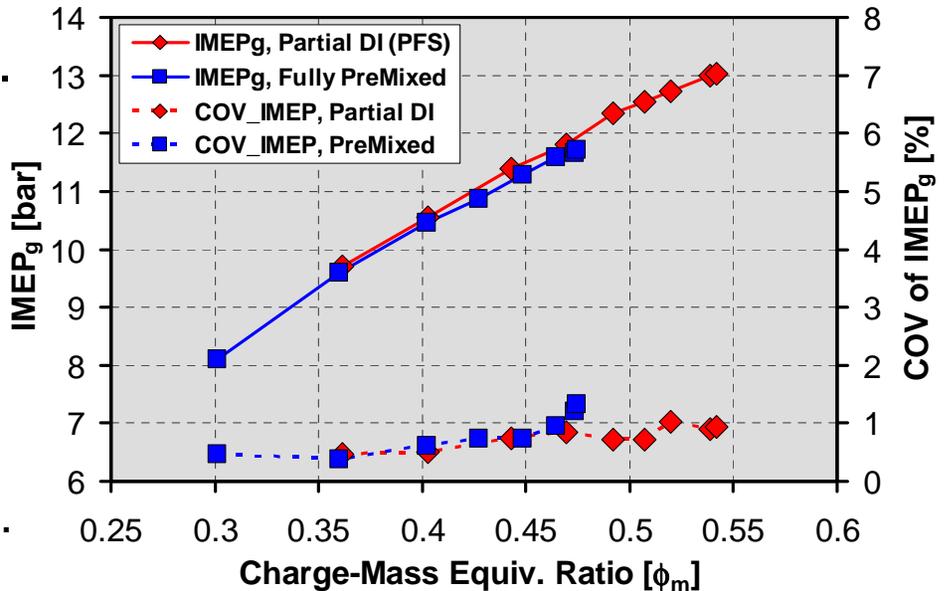


Extend High-Load Limit with PFS, $P_{in} = 2$ bar

- Premixed fueling \Rightarrow increase load from $\phi_m = 0.3$ to knock/stability limit.
 - Retard CA50 so Ringing ≤ 5 MW/m² \Rightarrow Limit: IMEP_g = 11.7 bar at $\phi_m = 0.47$.

- PFS allows significantly higher loads.
 - Limit: IMEP_g = 13.0 bar, $\phi_m = 0.54$.
 - Approaching oxygen availability limit \Rightarrow 0.9% O₂ in exhaust.

- Large reduction of HRR (PRR) allows:
 - CA50 more advanced than premixed.
 - > Higher thermal efficiency.
 - Even with ringing of 2 to 3 MW/m² vs. 5 MW/m² for premixed.
 - > PFS more stable with lower ringing.
 - > Lower ringing \Rightarrow quieter.

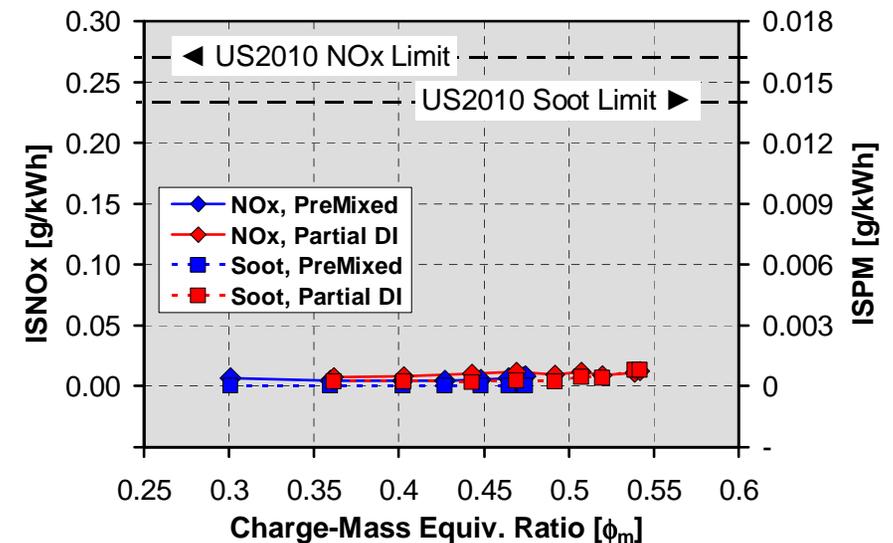
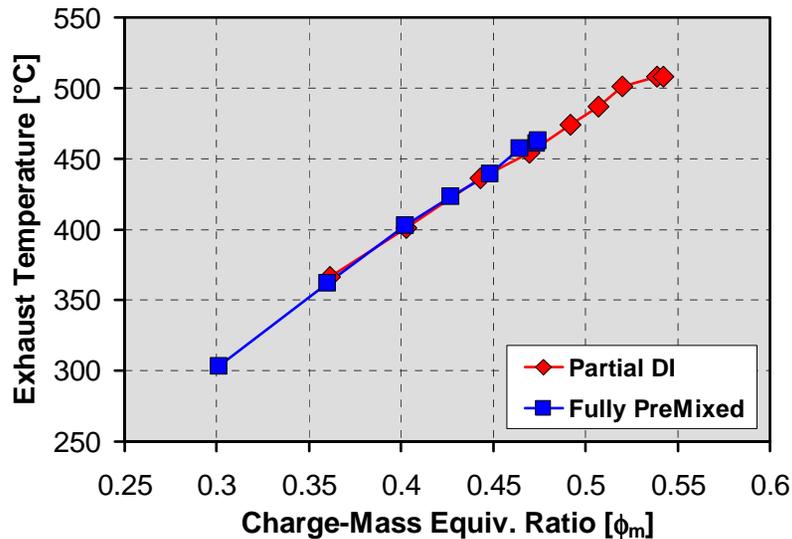
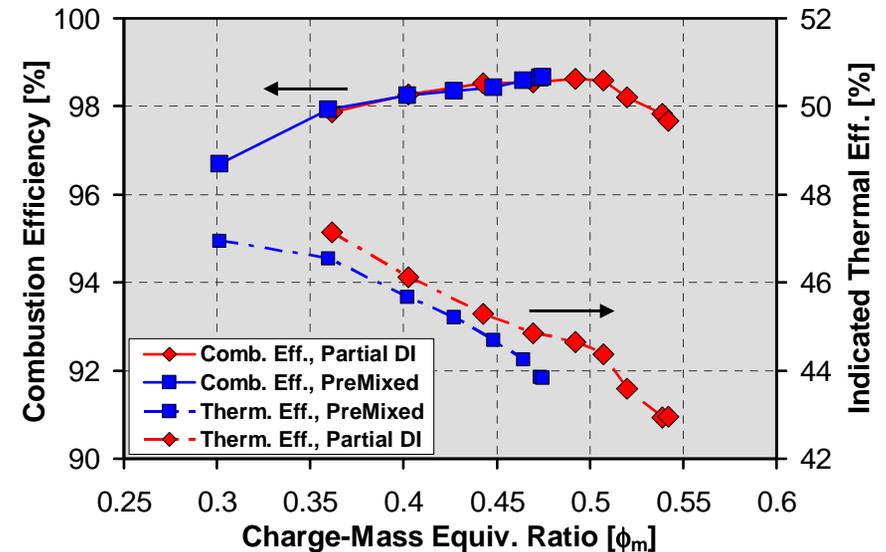


- PFS allows a large increase in load for gasoline boosted to $P_{in} = 2$ bar.

High-Load Limit with PFS, $P_{in} = 2$ bar



- Combust. Eff. mostly $> 98\%$, similar to premixed.
 - Small drop at highest loads due to increased CO as O_2 becomes limited.
- Therm. Eff is higher with PFS than premixed \Rightarrow CA50 is less retarded.
- NO_x and soot near detectability limit.
- Exhaust reaches higher temperature \Rightarrow Benefits for turbo-charging.

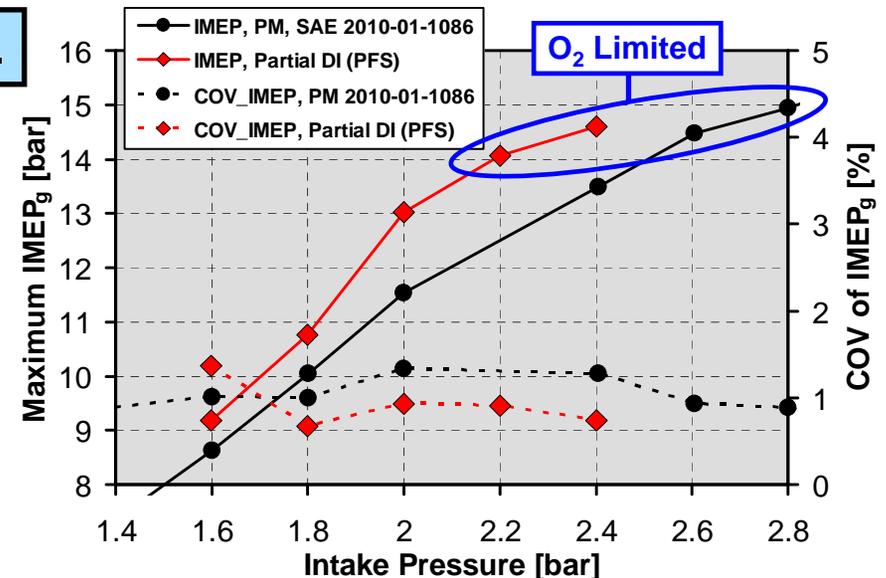
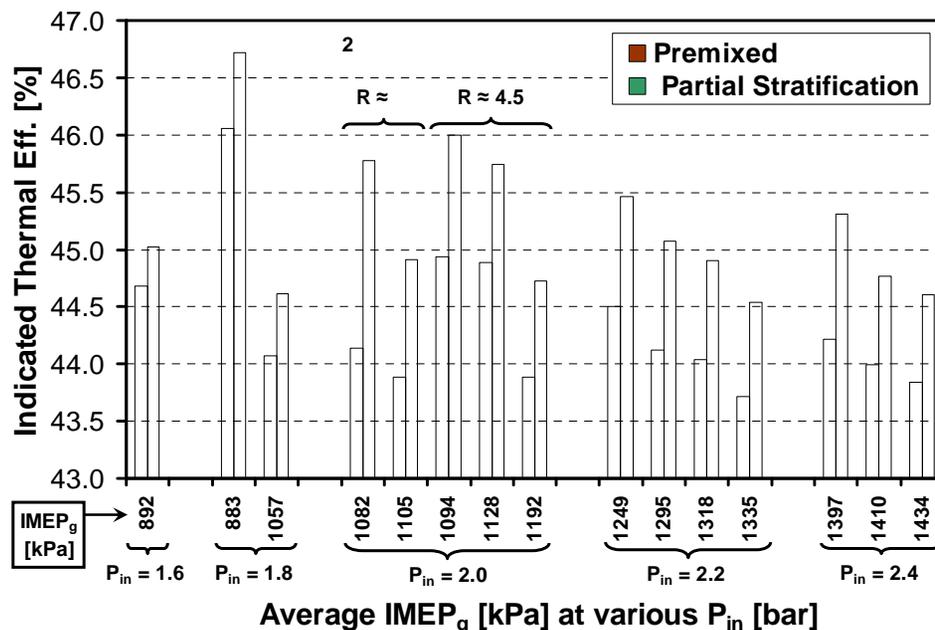


Load-Limit & Efficiency Improvements at Various P_{in}

- Our initial investigation of boosted HCCI in SAE 2010-01-1086 showed \Rightarrow maximum load attainable for well premixed HCCI at various boost levels.

• PFS allows higher loads for all P_{in} tested.

- PFS quite stable $P_{in} \geq 2.0$ bar \Rightarrow largest gain.
- O_2 limited for $P_{in} \geq 2.2$ bar.
- PFS less stable for $P_{in} = 1.6$ & 1.8 bar. $>$ Lower ϕ -sensitivity.



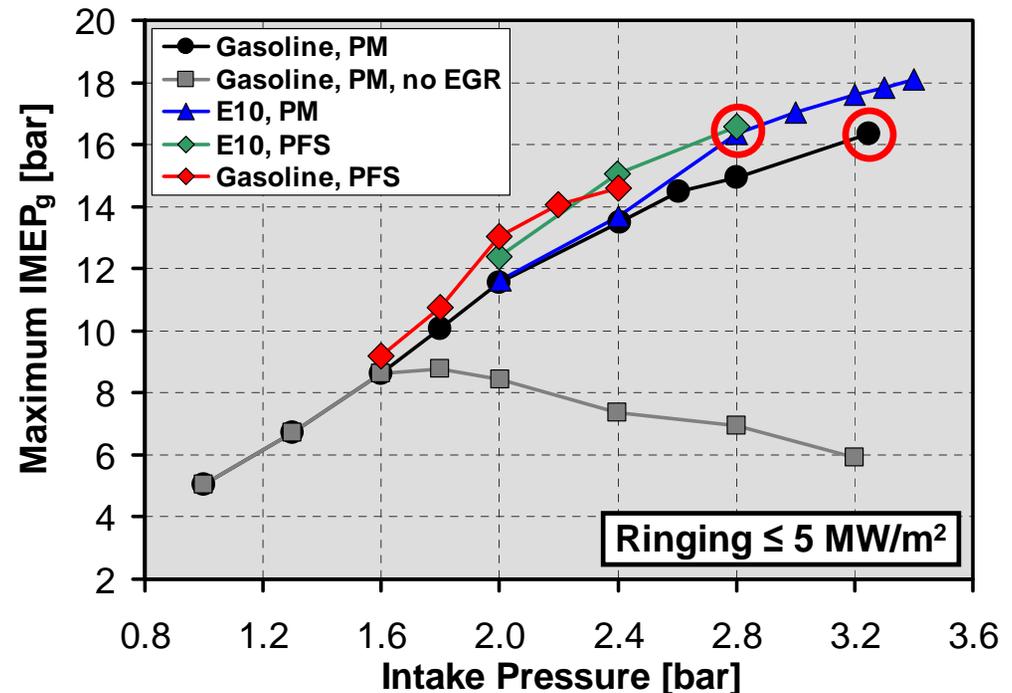
- Alternatively, for the same load, PFS allows CA50 to be advanced.
- T-E increases 0.3 to 1.6 T-E units \Rightarrow fuel economy gain of 0.7 – 3.6%.

• PFS gives typical fuel economy improvement of 2 – 2.5%.

Can E10 Increase the Oxygen-Availability Limit?



- High-load limit of ON=87 gasoline, $IMEP_g = 16.34$ bar at $P_{in} = 3.25$ bar.
 - Oxygen limited $P_{in} \geq 2.6$ bar.
- E10 \Rightarrow Add 10% ethanol to ON=87 gasoline, $ON \approx 89.6$
 \approx **mid-grade pump gasoline.**
- E10 significantly reduces EGR requirement with boost.
 - More air \Rightarrow higher fueling
- Remains stable with timing retard \Rightarrow ITHR still high.



- High-load limit for E10, $IMEP_g = 18.1$ bar at $P_{in} = 3.4$ bar.
 - Ringing ≤ 5 , ultra-low NO_x & soot

- PFS works well with E10 \Rightarrow increase load if not O_2 limited ($P_{in} \leq 2.8$ bar).
 - Obtain $IMEP_g = 16.6$ bar with less boost $\Rightarrow P_{in} = 2.8$ bar vs. 3.25 bar for gasoline.

Conclusions



- The ϕ -sensitivity of gasoline varies substantially with intake pressure.
 - $P_{in} = 1$ bar \Rightarrow not ϕ sensitive, and PFS is not effective for reducing the PRR.
 - $P_{in} = 2$ bar \Rightarrow strongly ϕ sensitive, and PFS is highly effective at reducing PRR.
- For $P_{in} = 2$ bar, PFS extends the high-load limit to $IMEP_g = 13.0$ bar compared to $IMEP_g = 11.7$ bar for fully premixed fueling.
- For higher boost, $P_{in} = 2.2$ and 2.4 bar, PFS allows fueling to be increased to the oxygen-availability limit (EGR \sim 48-50%).
- PFS is effective for increasing thermal efficiencies of boosted, gasoline-fueled HCCI for $P_{in} = 1.6 - 2.4$ bar over a wide range of fueling rates.
 - Typically, by an amount to give fuel economy improvements of 2 – 2.5%.
- PFS also works well for E10 \Rightarrow Effective range shifts to $P_{in} = 2.0 - 2.8$ bar.
- All PFS points examined showed extremely low NO_x and soot emissions.