

The Effects of Hydrothermal Aging on a Commercial Cu SCR Catalyst

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Directions in Engine-Efficiency and Emissions Research

Detroit, MI

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Motivation

- Selective Catalytic Reduction (SCR) proven effective over wide range of conditions, but improvement necessary for:
 - ✓ Increasingly stringent emission standards
 - ✓ Higher engine-out NO_x under high efficiency operating points
 - ✓ Cooler exhaust temperatures from advanced combustion regimes
 - ✓ Hotter exhaust temperatures from lean gasoline engines
- Model-based SCR system controls not sufficiently developed for adapting to catalyst aging/de-activation
 - ✓ Better understanding of catalyst aging required
 - ✓ Zeolite-based transition metal catalyst: Cu, Fe

Approach

- Investigate the nature of active sites using both model and commercial Cu SCR catalysts
- Conduct detailed laboratory reactor evaluation using both model and commercial Cu SCR catalysts
- Develop a Cu SCR catalyst model to extract kinetic parameters

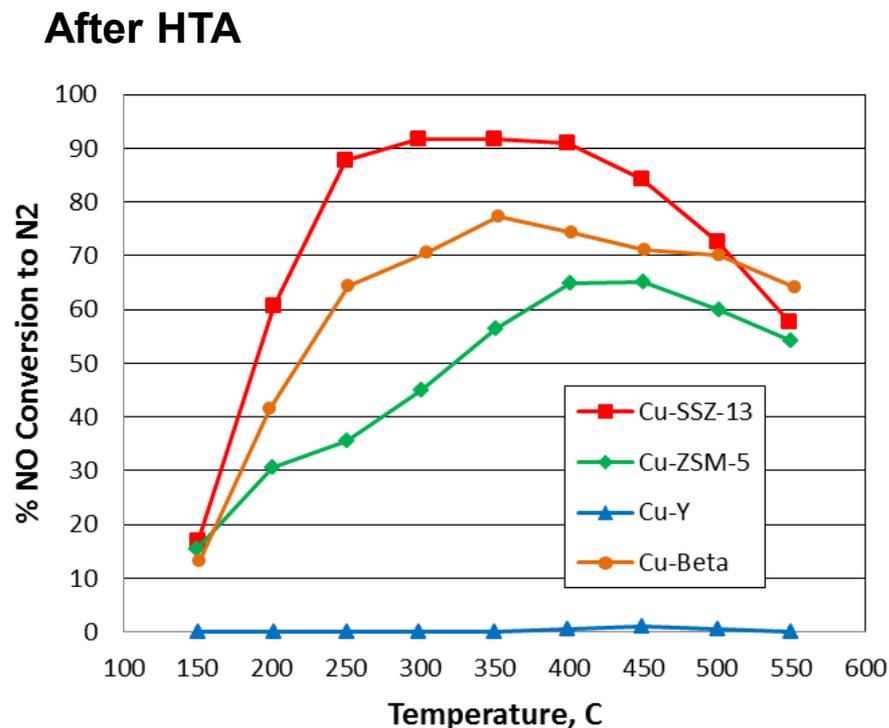
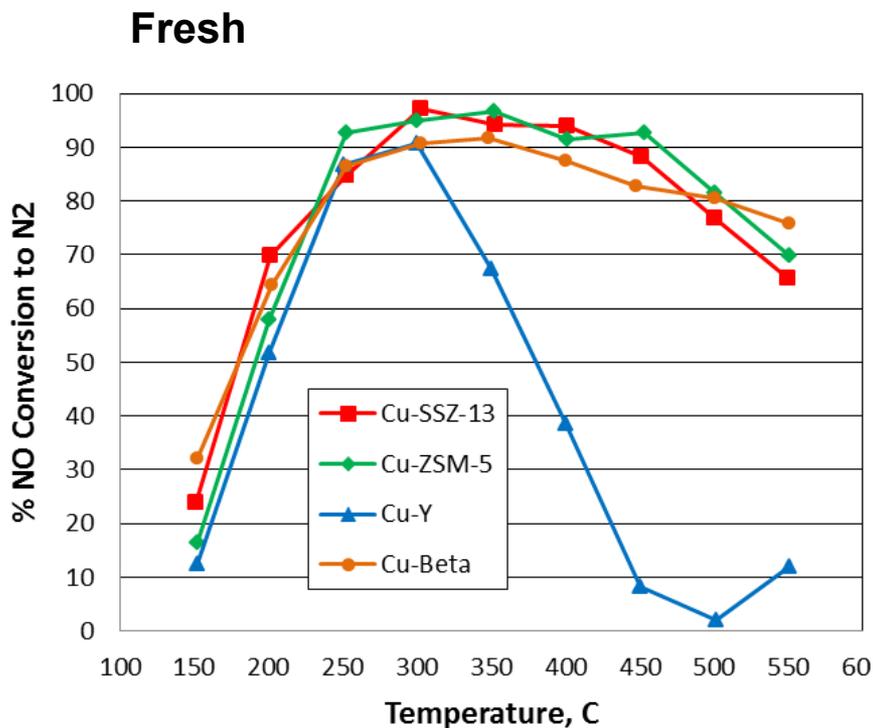
Presentation Outline

- Model Cu-Zeolite Catalyst
 - ✓ SCR activity
 - ✓ Characterization: XRD, H₂-TPR, Al NMR
- Commercial Cu-Zeolite Catalyst
 - ✓ SCR activity
 - ✓ Characterization
 - ✓ Cu SCR catalyst model
- Conclusions

Model Cu SCR Catalyst Study

- Model Cu-Zeolite SCR Catalyst
 - ✓ Cu-SSZ-13 (Si/Al₂ ~12), Cu-ZSM-5 (Si/Al₂ ~30)
Cu-beta (Si/Al₂ ~38), Cu-Y(Si/Al₂ ~5.2)
- Hydrothermal Aging
 - ✓ 10% H₂O in air, 800°C, 16 h
- Lab Reactor Evaluation
 - ✓ 350 ppm NO_x, 350 ppm NH₃, 14% O₂, 10% H₂O in balance N₂
 - ✓ GHSV = 30K h⁻¹
 - ✓ FT-IR (NO, NO₂, NH₃, N₂O)
- Catalyst Characterization
 - ✓ XRD, H₂-TPR, ²⁷Al NMR

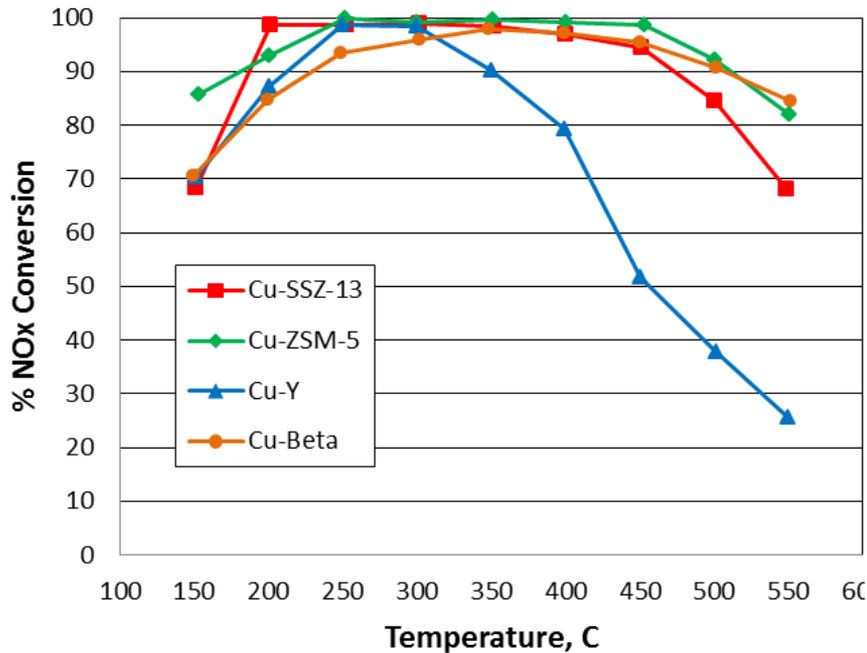
NO SCR over Model Cu Zeolite Catalysts



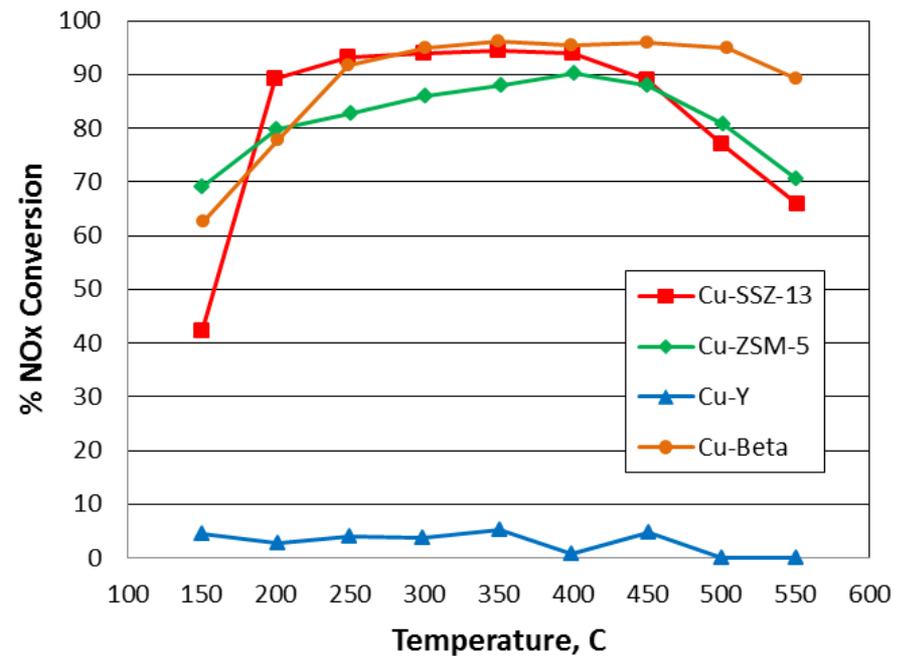
- High NO SCR activity for Cu-SSZ-13 even after HTA
- Significant loss of activity for Cu-ZSM-5, Cu-beta, Cu-Y

Fast SCR ($\text{NO}/\text{NO}_2 = 1$)

Fresh



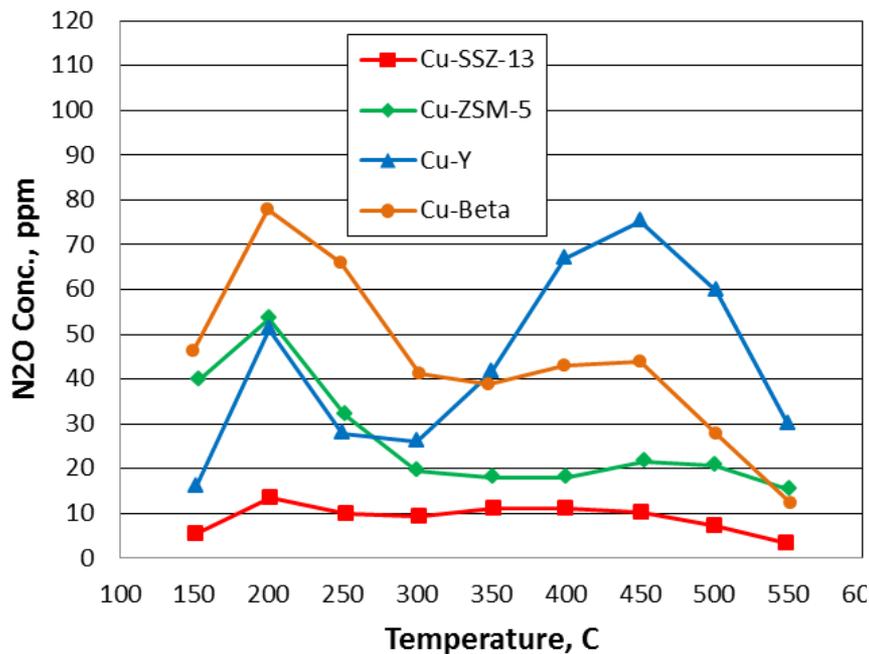
After HTA



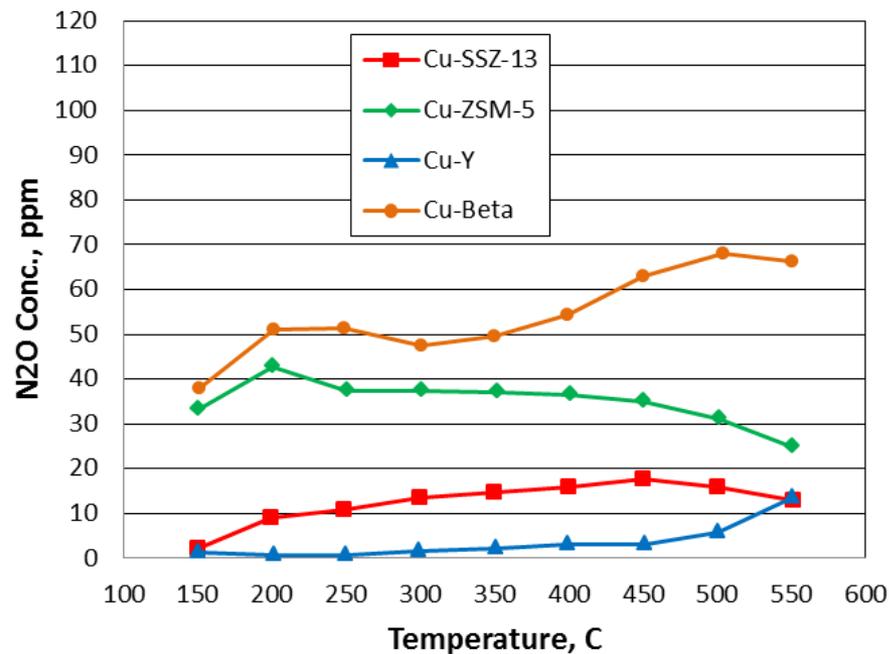
- Significant loss of activity for Cu-Y
- High SCR activity maintained for Cu-ZSM-5, Cu-beta, Cu-SSZ-13

N₂O Formation during Fast SCR

Fresh

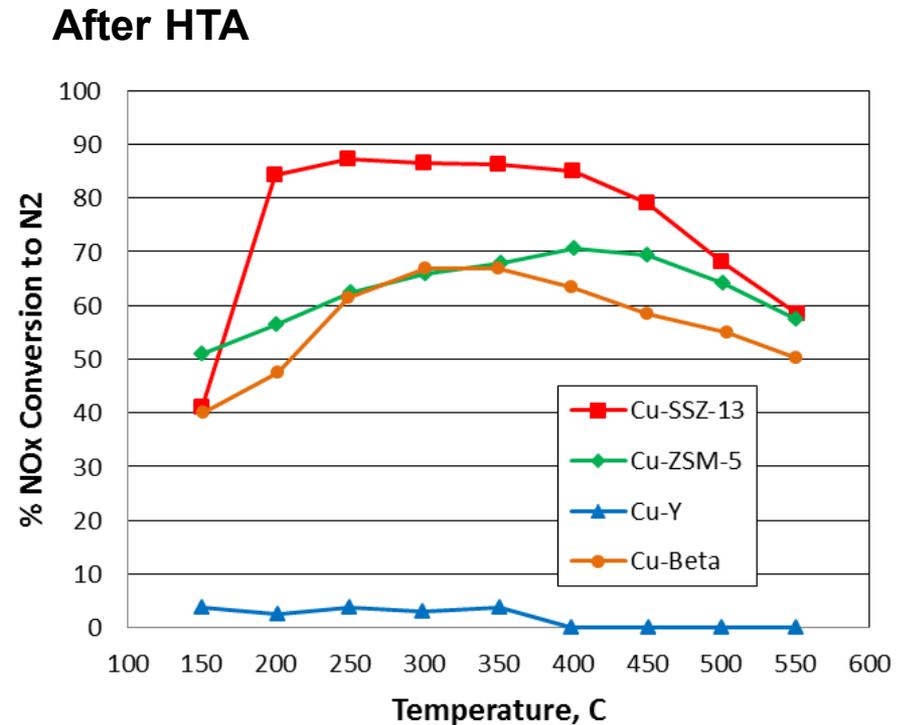
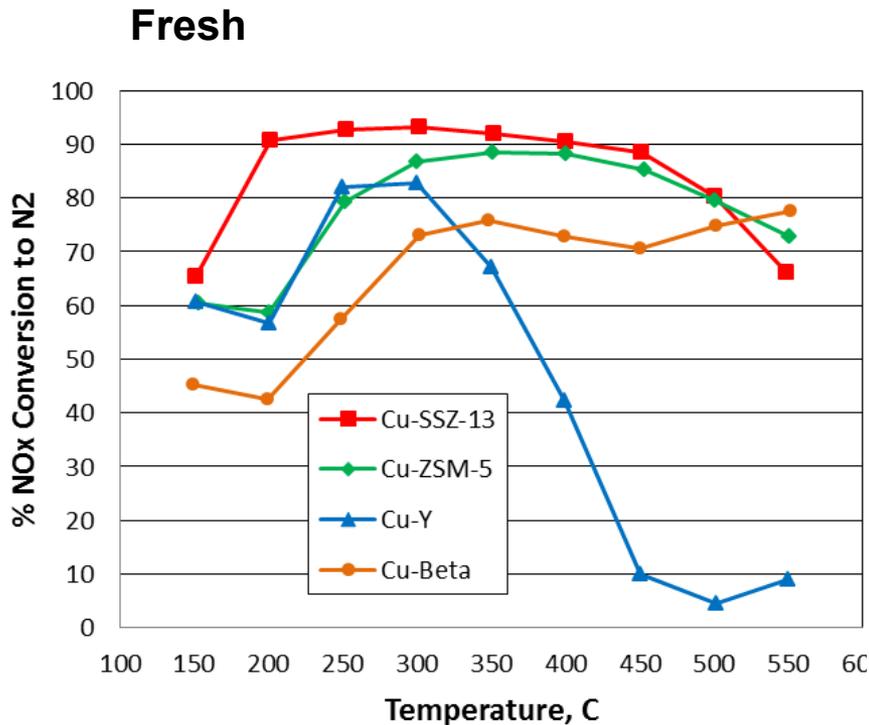


After HTA



- Significant N₂O formation during “fast” SCR
- Little N₂O formation on Cu-SSZ-13

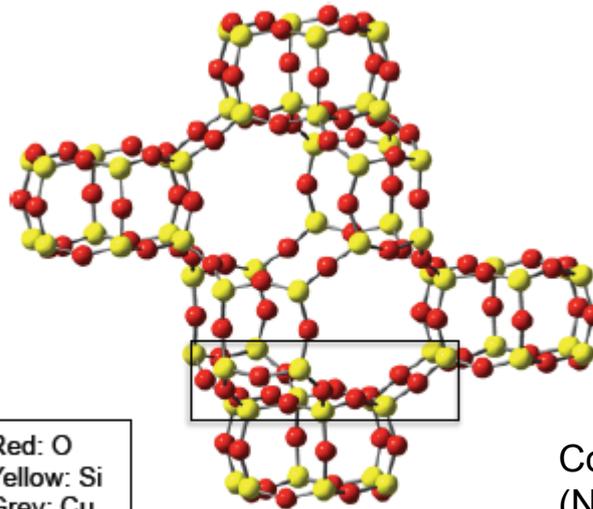
Fast SCR ($\text{NO}/\text{NO}_2 = 1$)



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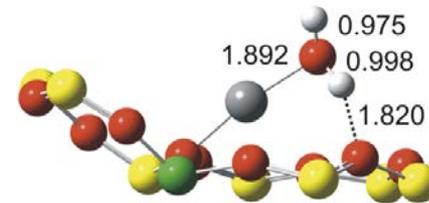
Effects of Hydrothermal Aging

1. Zeolite structure change
2. Dealumination of zeolite structure
3. Formation of different Cu species (e.g. CuO)



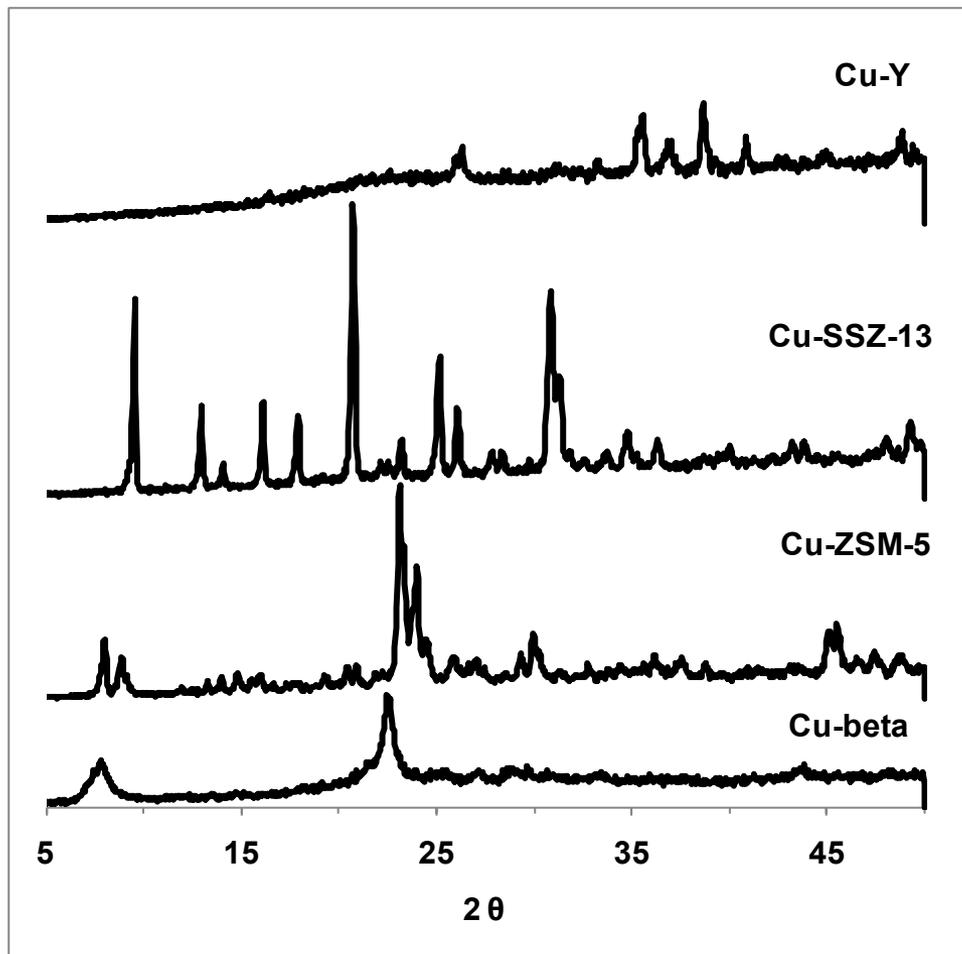
Red: O
Yellow: Si
Grey: Cu
Green: Al
White: H

periodic DFT



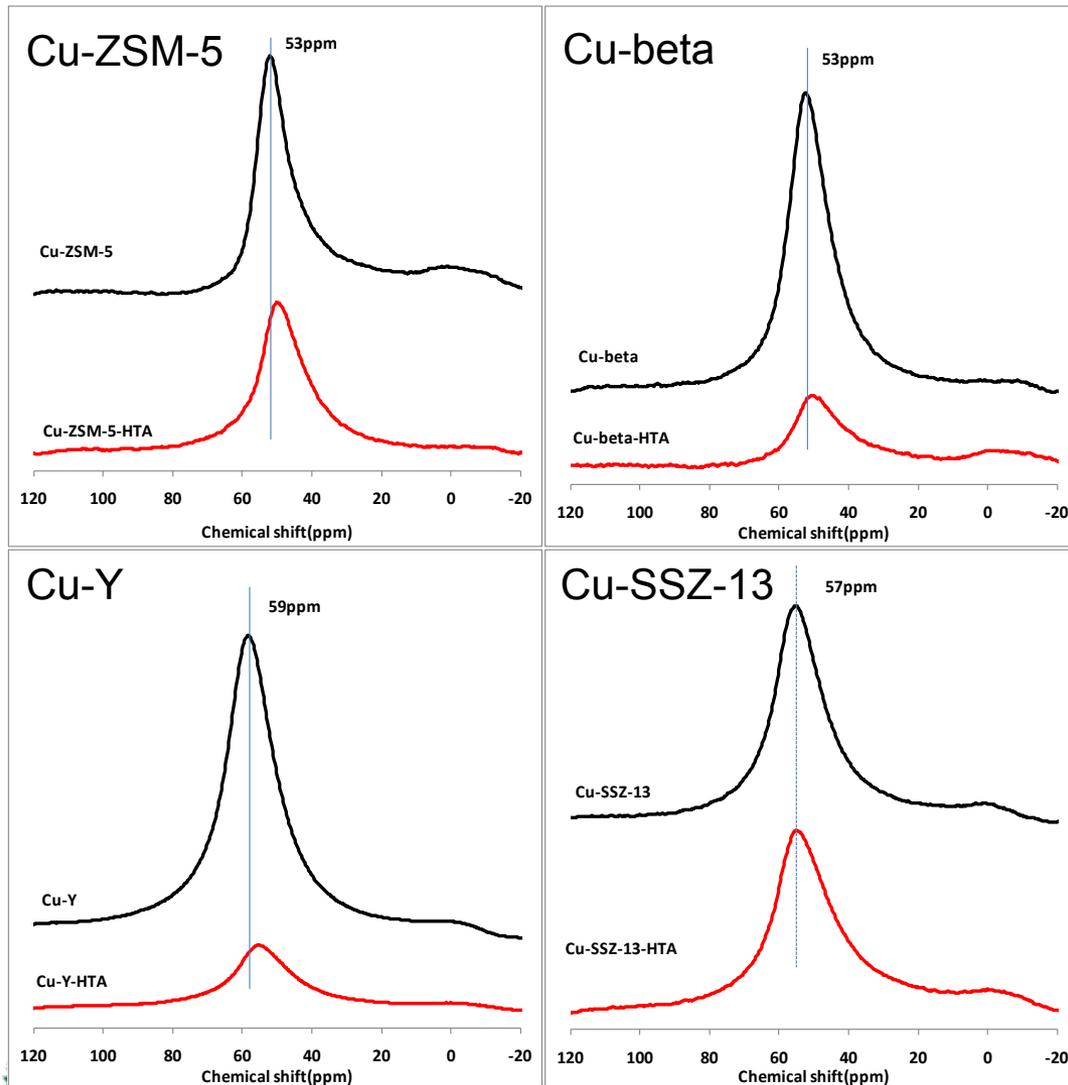
Courtesy of Prof. Bill Schneider
(Notre Dame)

Structural Integrity by XRD



- Total collapse of zeolite structure for Cu-Y
 - Little changes noticed for Cu-SSZ-13, Cu-ZSM-5, Cu-beta
- Structure mostly intact after 800C for 16 h

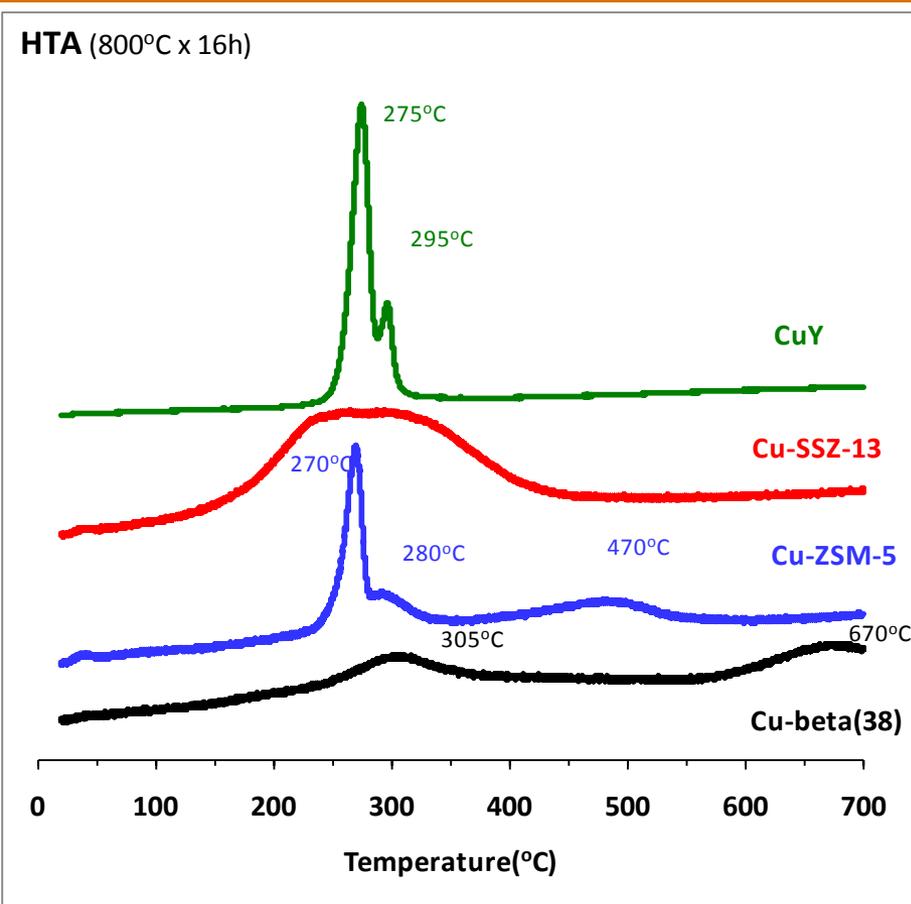
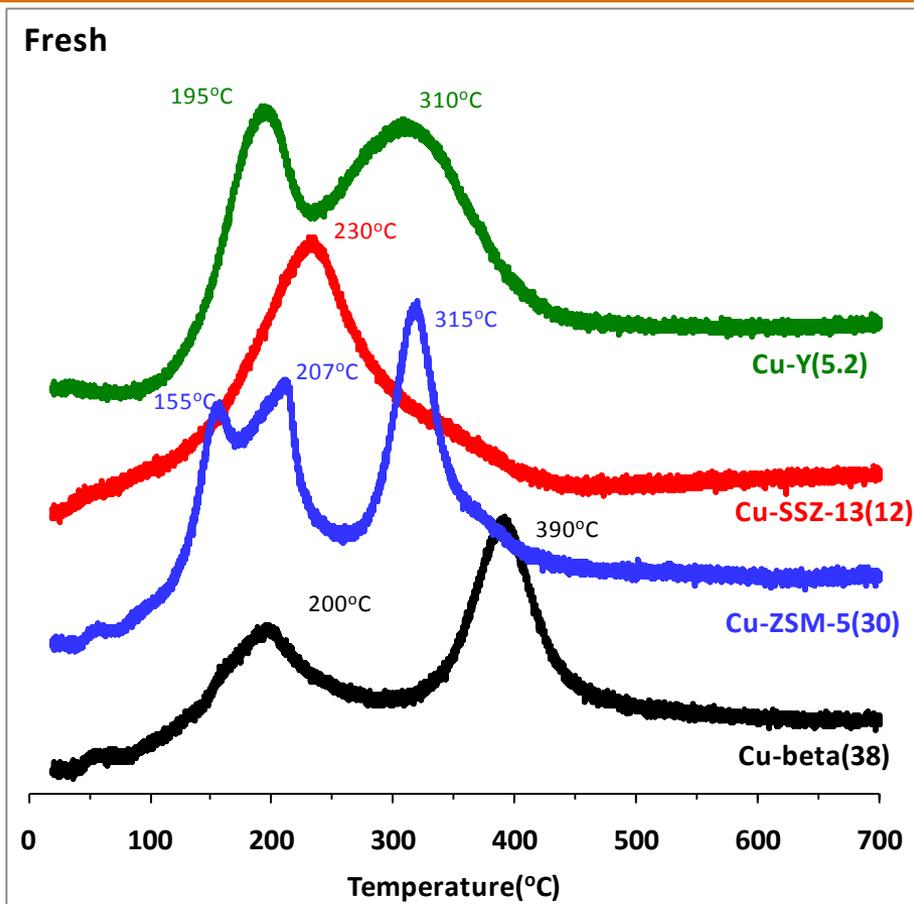
Dealumination by Solid State ^{27}Al NMR



- With dealumination, tetrahedral Al becomes octahedral
- Cu-SSZ-13: no change
- Cu-ZSM-5, Cu-beta, Cu-Y: loss of tetrahedral Al, but no octahedral Al

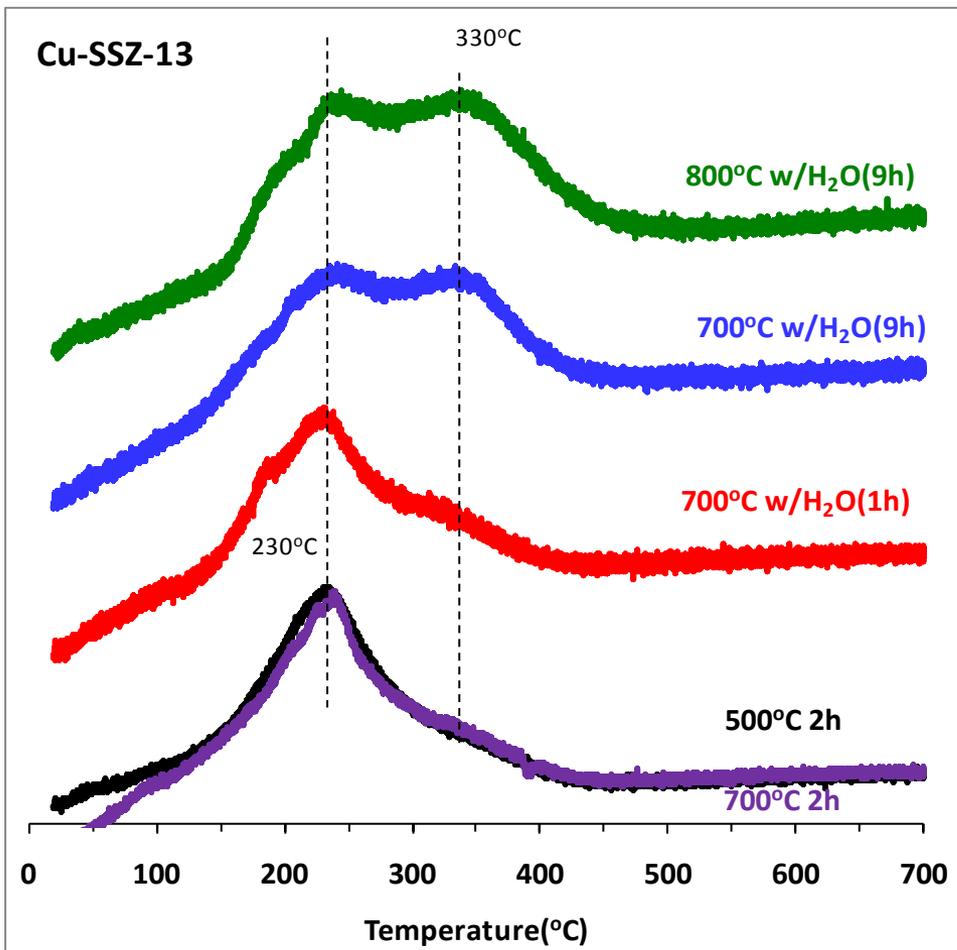
→ Isolated Cu species in strong contact with alumina in Cu-ZSM-5, Cu-beta

Cu Reducibility by H₂-TPR

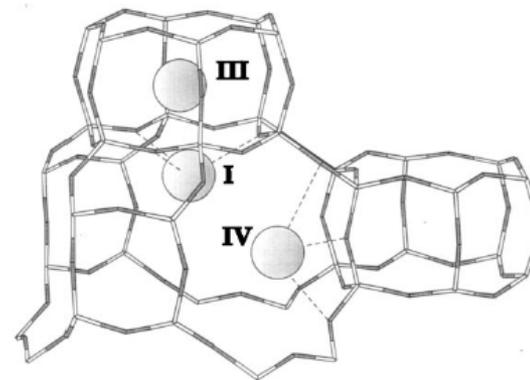


- Reduced amount of “zeolytic” Cu over aged Cu-ZSM-5, Cu-beta
- Same amount, but different ratios of two peaks over Cu-SSZ-13

Cu Species in Cu-SSZ-13



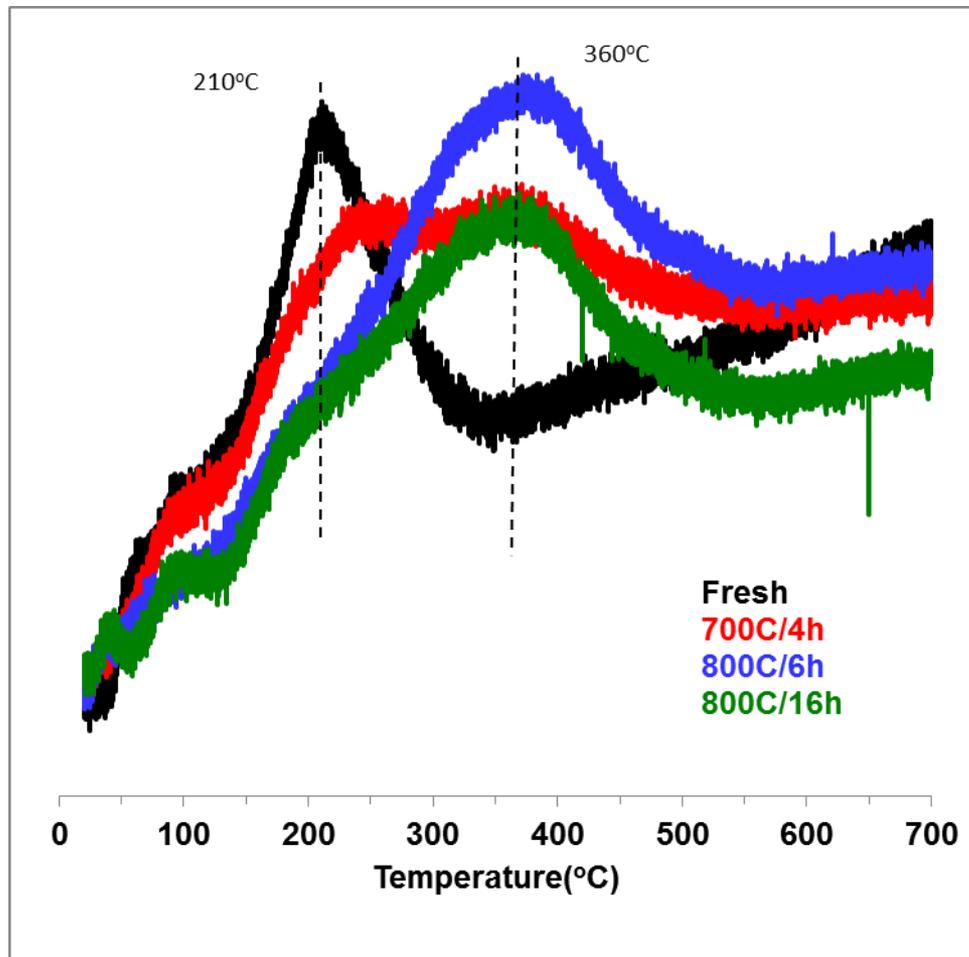
Cationic sites in dehydrated CHA



J. Dědeček et al. / Microporous and Mesoporous Materials 32 (1999) 63–74

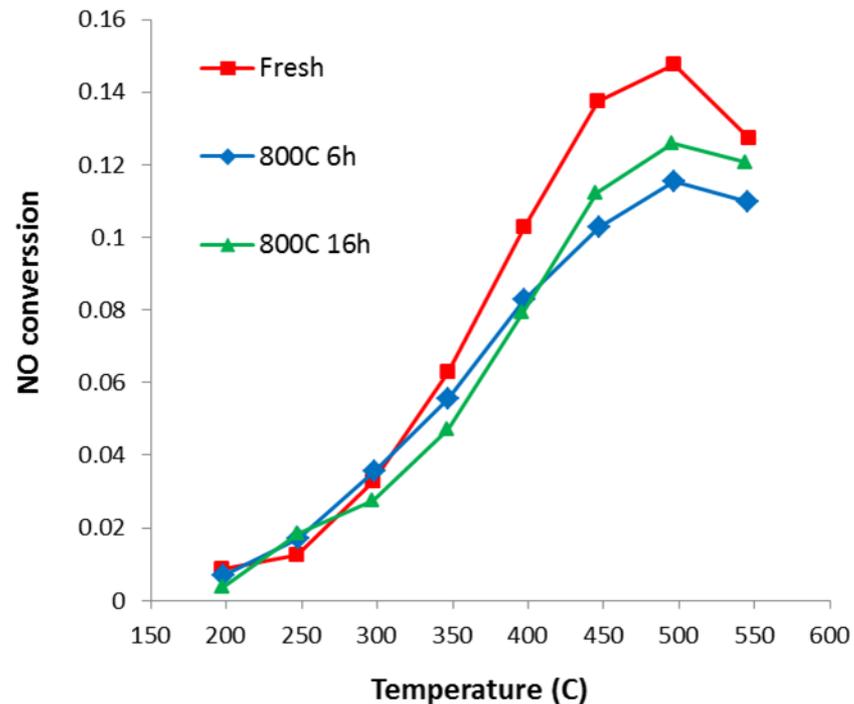
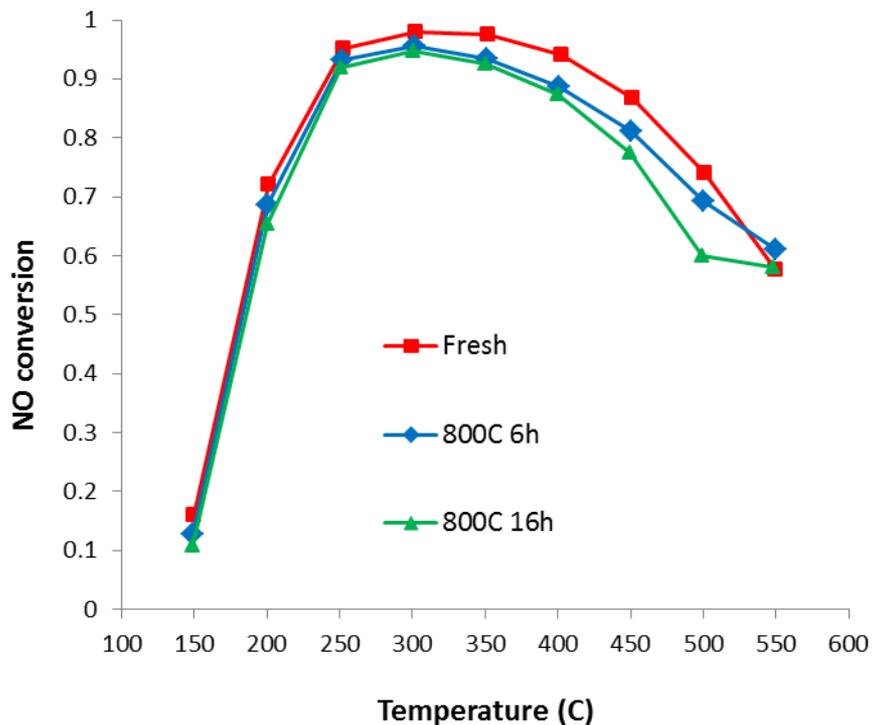
Change in distribution of Cu species after HTA!

Cu Species in Commercial Catalyst



- Hydrothermal aging of Commercial Cu SCR: 700C/4h, 800C/6, 800C/16
 - 210°C and 360°C peaks
- Change in distribution of Cu species after HTA?
- Formation of different Cu species?

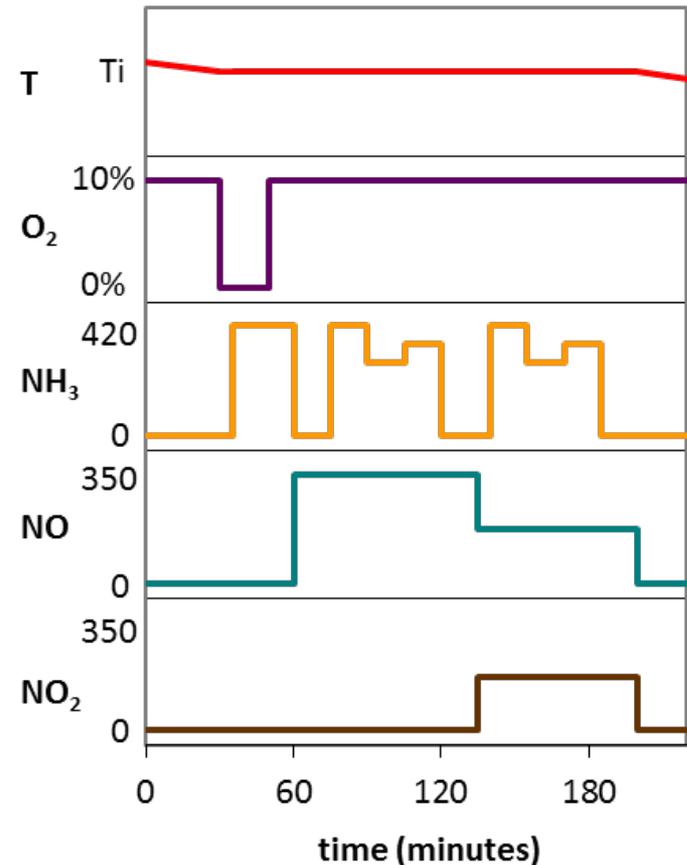
NO SCR over Commercial Catalyst



- Progressive deterioration of SCR activity at high temperatures
- Changes in Cu location/species? Changes in kinetics?

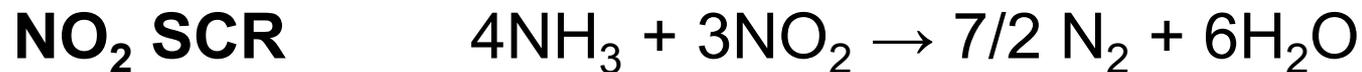
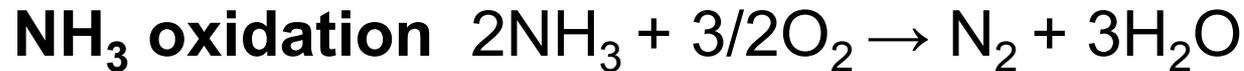
Commercial Cu SCR Catalyst Evaluation

- CLEERS SCR Transient Reactor Protocol designed to generate data needed for model calibration and performance evaluation
 - ✓ Steady state & transient points
 - ✓ SCR conditions:
 - $\text{NH}_3/\text{NO}_x = 0.8, 1.0, 1.2$
 - $\text{NO}_2/\text{NO}_x = 0.0, 0.5$
 - O_2 oxidation of NH_3 & NO
- Experiments conducted on commercial core samples
 - ✓ 150-550°C
 - ✓ 30k, 60k, 90k h^{-1}
 - ✓ 350 ppm NO_x



Cu SCR Model Development

In addition to NH_3 adsorption and desorption on SCR catalyst surface, the following reactions have been incorporated in this version of Cu-Z SCR model



Cu SCR Model Development

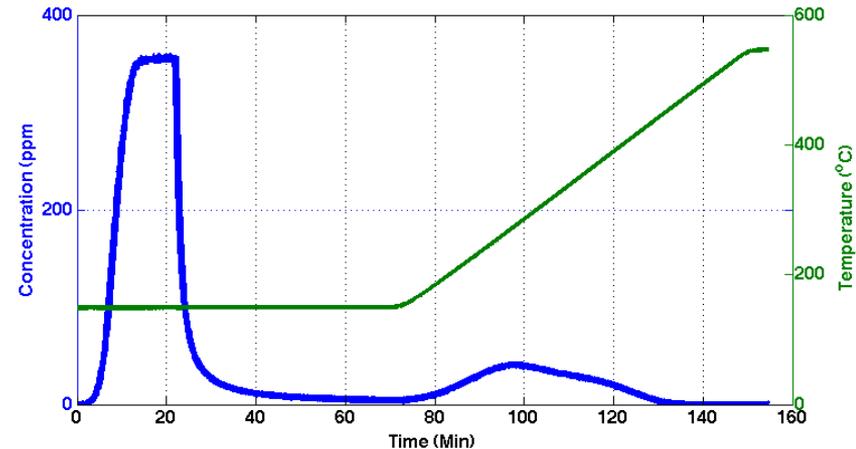
- All SCR models developed in Matlab/Simulink using a variable step solver (ode23tb)
- First order Euler integration in space – 100 elements (cells) along the axis
- Nonlinear constrained minimization (fmincon) used to identify rate parameters using Matlab's Optimization toolbox

$$\frac{\partial c_{g,NH_3}}{\partial t} = -\frac{u}{\varepsilon} \frac{\partial c_{g,NH_3}}{\partial x} + \frac{\Omega}{\varepsilon} (r_{des} - r_{ads})$$
$$\frac{d\theta_{NH_3}}{dt} = r_{ads} - r_{des}$$

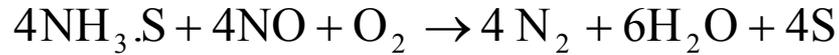
NH₃ adsorption and desorption

$$r_{ads} = A_{ads} c_{g,NH_3} (1 - \theta_{NH_3})$$

$$r_{des} = A_{des} e^{\frac{-E_{des}(1-\gamma\theta_{NH_3})}{RT}} \theta_{NH_3}$$



SCR Reactions



$$r_{std-scr} = A_{std-scr} e^{\frac{-E_{std-scr}}{RT}} c_{g,NO} \theta_{\text{NH}_3}$$

$$\frac{\partial c_{g,NO}}{\partial t} = -\frac{u}{\varepsilon} \frac{\partial c_{g,NO}}{\partial x} - \frac{1}{\varepsilon} (r_{\text{NO},oxi} + \Omega r_{std-scr})$$

$$\frac{\partial c_{g,NO_2}}{\partial t} = -\frac{u}{\varepsilon} \frac{\partial c_{g,NO_2}}{\partial x} + \frac{1}{\varepsilon} (r_{\text{NO},oxi})$$

$$\frac{\partial c_{g,NH_3}}{\partial t} = -\frac{u}{\varepsilon} \frac{\partial c_{g,NH_3}}{\partial x} + \frac{\Omega}{\varepsilon} (r_{des} - r_{ads})$$

$$\frac{d\theta_{\text{NH}_3}}{dt} = r_{ads} - r_{des} - r_{\text{NH}_3,oxi} - r_{std-scr}$$

$$\frac{\partial c_{g,O_2}}{\partial t} = -\frac{u}{\varepsilon} \frac{\partial c_{g,O_2}}{\partial x} - \frac{\Omega}{\varepsilon} \left(\frac{3}{4} r_{\text{NH}_3,oxi} + \frac{1}{4} r_{std-scr} \right)$$



$$r_{fast-scr} = A_{fast-scr} e^{\frac{-E_{fast-scr}}{RT}} c_{g,NO} c_{g,NO_2} \theta_{\text{NH}_3}$$

$$\frac{\partial c_{g,NO}}{\partial t} = -\frac{u}{\varepsilon} \frac{\partial c_{g,NO}}{\partial x} - \frac{1}{\varepsilon} (r_{\text{NO},oxi} + \Omega (r_{std-scr} + 0.5 r_{fast-scr}))$$

$$\frac{\partial c_{g,NO_2}}{\partial t} = -\frac{u}{\varepsilon} \frac{\partial c_{g,NO_2}}{\partial x} + \frac{1}{\varepsilon} (r_{\text{NO},oxi} - \Omega (r_{\text{NO}_2-scr} + 0.5 r_{fast-scr}))$$

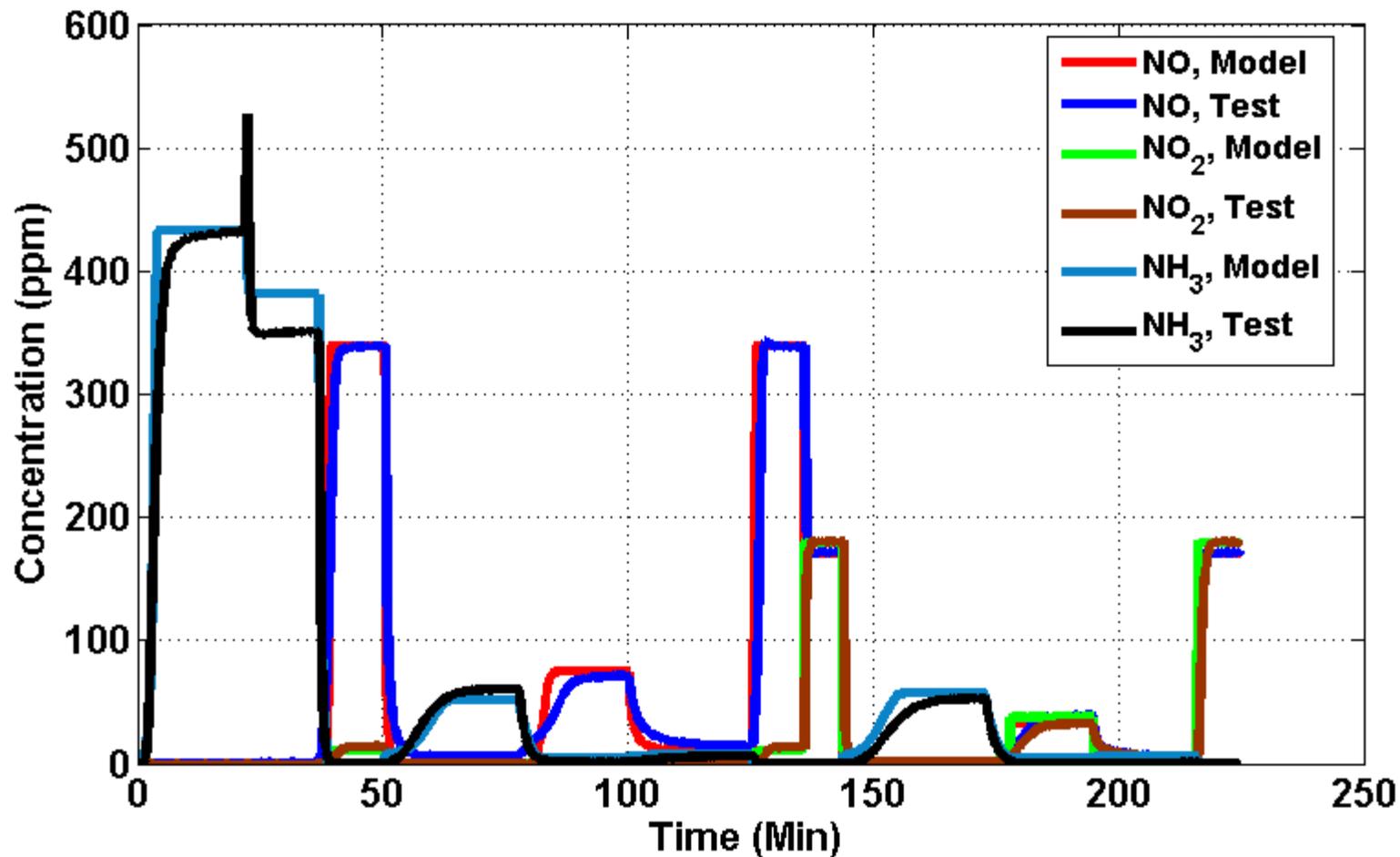
$$\frac{\partial c_{g,NH_3}}{\partial t} = -\frac{u}{\varepsilon} \frac{\partial c_{g,NH_3}}{\partial x} + \frac{\Omega}{\varepsilon} (r_{des} - r_{ads})$$

$$\frac{d\theta_{\text{NH}_3}}{dt} = r_{ads} - r_{des} - r_{\text{NH}_3,oxi} - r_{std-scr} - r_{\text{NO}_2-scr} - r_{fast-scr}$$

$$\frac{\partial c_{g,O_2}}{\partial t} = -\frac{u}{\varepsilon} \frac{\partial c_{g,O_2}}{\partial x} - \frac{\Omega}{\varepsilon} \left(\frac{3}{4} r_{\text{NH}_3,oxi} + \frac{1}{4} r_{std-scr} \right)$$

- Cost function to be minimized is defined as the average sum of absolute error between the test and simulated concentrations.

Model Validation



Rate Parameters

Reaction	E (kJ/mol)	E (kJ/mol) from Published Literature	Reference
NH₃ Desorption	180.2	181.5	Olsson, 2008
NH₃ Oxidation	74	68.7 6.3	Kamasamudram, 2010
NO Oxidation	39	43	Chakravarthy, 2007
Standard SCR	84.9	84.9	Olsson, 2008
Fast SCR	85.1	85.1	Olsson, 2008

- Changes in rate parameters induced by hydrothermal aging to be monitored with respect to changes in Cu species, etc.

Conclusions

- Investigated the effects of hydrothermal aging on the activity and physicochemical properties of model and commercial Cu SCR catalysts.
- Small pore zeolite-based commercial Cu and model Cu-SSZ-13 are highly active, selective, and durable.
 - ✓ Little changes in zeolite structure after 800°C/16h
 - ✓ Isolated Cu ion species (not Cu-aluminate-like species)
- Developed Cu SCR catalyst model to monitor the changes in kinetic parameters induced by catalyst aging.

Acknowledgments

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- CLEERS Team
- Sanath Kumar, Pat Burks (BASF)
- Giovanni Cavataio (Ford)

